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TRACE-D USERS' MANUAL

JULY 1969

S. G. Santarelli

Prepared for

DIRECTORATE OF PLANNING AND TECHNOLOGY

ELECTRONIC SYSTEMS DIVISION

AIR FORCE SYSTEMS COMMAND

UNITED STATES AIR FORCE

L. G. Hanscom Field, Bedford, Massachusetts



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Project 7070

Prepared by

THE MITRE CORPORATION

Bedford, Massachusetts

Contract F19628-68-C-0365

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FOREWORD

This report was prepared by The MITRE Corporation for the Directorate of Planning and Technology, Electronic Systems Division, Air Force Systems Command, L.G. Hanscom Field, Bedford, Massachusetts, under Contract F19628-68-C-0365.

REVIEW AND APPROVAL

Publication of this technical report does not constitute Air Force approval of the report's findings or conclusions. It is published only for the exchange and stimulation of ideas.

ANTHONY P. TRUNFIO
Technical Advisor
Development Engineering Division
Directorate of Planning and Technology

ABSTRACT

This report describes the MITRE version of the TRACE-D program now in operation. While the primary function of TRACE-D is orbit determination, options are also available in the program for trajectory prediction and observational data generation. A functional description of these features is contained in this report along with a complete user's manual and a brief program description.

PREFACE

The program described herein is a modified version of the TRACE-D program originally developed by the Aerospace Corporation in Los Angeles. Although the modifications made were many and included conversion of the program to FORTRAN IV and STRAP, restructuring of the program logic, and the addition of minor options and features, the basic functions (i.e., orbit determination, trajectory prediction, and observational data generation) remain intact.

The people involved in various aspects of the effort, in addition to the author, were Dr. K. K. Maitra, G. M. Hyder, P. E. Shifres, and S. Schwartz. A great deal of appreciation is due to K. W. Hubbard, C. C. Tonies, and other members of the Flight Mechanic's Department of the Aerospace Corporation whose cooperation in obtaining the program and unlimited assistance throughout the task were invaluable.

This report is intended solely as a user's guide to the TRACE-D program, and therefore contains only a brief functional description of the analytics. For the reader seeking the mathematical details and arguments the ideal reference is the original document¹ issued by the Aerospace Corporation (see [1]).

¹ Material from this Aerospace document has been freely incorporated into this report wherever pertinent and is not to be taken as original.

TABLE OF CONTENTS

		<u>Page</u>
LIST OF ILLUSTRATIONS		viii
LIST OF TABLES		x
SECTION 1	BASIC INFORMATION	1
	1.1 INTRODUCTION	1
	1.2 PROGRAM HISTORY	1
	1.3 MODIFICATION PROCESS	2
SECTION 2	MAJOR PROGRAM FUNCTIONS	3
	2.1 TRAJECTORY PREDICTION	3
	2.2 OBSERVATION GENERATION	4
	2.3 ORBIT DETERMINATION	5
SECTION 3	USAGE	13
	3.1 PRELIMINARY FACTS	13
	3.2 BASIC DATA	16
	3.2.1 Constants	16
	3.2.1.1 Integration Constants	17
	3.2.1.2 Physical Constants	18
	3.2.2 Functions to be Performed	21
	3.2.3 Trajectory Specifications	21
	3.2.3.1 Epoch	21
	3.2.3.2 Initial Conditions	22
	3.2.4 Force Model Inputs	23
	3.2.4.1 Drag and T Matrix	23
	3.2.4.2 Other Body Perturbations	25
	3.2.4.3 Exponential Thrust	26
	3.2.4.4 Gravity Perturbations	26
	3.2.5 Miscellaneous Inputs	28
	3.2.5.1 Orbit Adjusts	28
	3.2.5.2 Extra Kicks	29
	3.2.5.3 Print Code	29
	3.2.5.4 Equinox Precession Corrections	30
	3.2.5.5 Direction of Integration	30
	3.2.5.6 Primary Scratch Tape	31
	3.3 TRAJECTORY-ONLY DATA	32
	3.3.1 Print Time Vector	32
	3.3.2 Variational Equation Partial Derivatives	32
	3.3.3 Trajectory Comparison Options	34
	3.3.4 Revolution Number	35
	3.3.5 Trajectory Tape Generation	35
	3.3.6 Latitude and/or Longitude Prints	36

TABLE OF CONTENTS (continued)

	<u>Page</u>
3.4 OBSERVATION GENERATION DATA	37
3.4.1 Special Output Options	37
3.4.2 Vehicle Attitude Specifications	38
3.4.3 Data Error Inputs	39
3.4.4 Orbit Covariance Matrix	43
3.4.5 Station Cards	43
3.4.6 Data Limit Specification Cards	44
3.4.7 Data Type Specification Cards	45
3.5 Orbit Determination Data	56
3.5.1 Multiple Satellite Option	56
3.5.2 Parameter Specification	57
3.5.2.1 Differential Equation Parameters	57
3.5.2.2 Radar Parameters	59
3.5.3 Parameter Bounds	62
3.5.4 Observation Sigmas	63
3.5.5 Maximum Iterations	63
3.5.6 Residual Editing	63
3.5.7 Data Correction Factors	64
3.5.7.1 Elevation Angle Refraction	64
3.5.7.2 Range Refraction Correction	65
3.5.7.3 Propagation Time Correction	65
3.5.8 Data Tape Options	65
3.5.9 True Equinox Correction	66
3.5.10 Proximity Indicators	66
3.5.11 Constraint Matrix	66
3.5.11.1 General Constraint Matrix	66
3.5.11.2 Specific Application	69
3.5.12 Station Cards	72
3.5.13 Observation Cards	73
3.6 Input Deck Arrangements	74
3.6.1 Trajectory Prediction Deck Arrangement	76
3.6.2 Observation Generation Deck Arrangement	76
3.6.3 Orbit Determination Deck Arrangement	80
3.6.4 Sample Input Decks	84
SECTION 4	
SAMPLE OUTPUT	105
4.1 TRAJECTORY ONLY SAMPLE OUTPUT	105
4.2 OBSERVATION GENERATION SAMPLE OUTPUT	109
4.3 ORBIT DETERMINATION SAMPLE OUTPUT	112

TABLE OF CONTENTS (concluded)

	<u>Page</u>
SECTION 5	
PROGRAMMING INFORMATION	147
5.1 STRUCTURE AND FLOW CHARTS	147
5.2 TAPE USAGE	147
5.3 SUBROUTINES	150
5.4 VARIABLE LISTS	173
REFERENCES	191

LIST OF ILLUSTRATIONS

<u>Figure Number</u>		<u>Page</u>
1	Station Card Format	47
2	Data Generation Limits Card Format	48
3	Date Type Card Format	49
4	Observation Card Format	50
5	Trajectory Prediction Deck Arrangement	74
6	Multiple Case Trajectory Prediction Deck Arrangement	75
7	Deck Arrangement for Observation Generation Single Case	76
8	Deck Arrangement for Two Cases of Observation Generation	77
9	Deck Arrangement for Orbit Determination with Input Tape	78
10	Deck Arrangement for Single Orbit Determina- tion Run with all Data on Cards	79
11	Deck Arrangement for Two Orbit Determination Cases all Data on Cards	80
12	Deck Arrangement for Multiple Satellite Orbit Determination Run (Three Satellites)	81
13	Listing of a Sample Data Deck for a Trajectory Prediction Run	83
14	Listing of a Sample Data Deck for an Observation Generation Run	85
15	Listing of a Sample Data Deck for an Orbit Determination Run	87
16	Trajectory Prediction Output Listing of Input	116-18

LIST OF ILLUSTRATION

<u>Figure Number</u>		<u>Page</u>
17	Header Page	119
18	Initial Information	120-21
19	Ephemeris Output	122
20	Observation Generation Output Listing of Input	123-24
21	Header Page	125
22	Initial Information	126-27
23	Data Specifications	128
24	Generated Data	129-30
25	Orbit Determination Output Listing of Input	131-33
26	Header and Observations	134-36
27	Initial Information	137-38
28	Computed Values	139
29	Residual Output	140
30	RMS Summary	141
31	Results of Iteration	142-44
32	General TRACE-D Program Flow Chart	145
33	Segmentation Flow Chart	146

LIST OF TABLES

<u>Table Number</u>		<u>Page</u>
1	Input Output Quantities Associated with TRACE-D Trajectory Mode	6
2	Input Output Quantities Associated with TRACE-D Observation Generation	9
3	Input Output Quantities Associated with TRACE-D Orbit Determination	11
4	Parameter List	
5	INTEG and C Constants Lists	19
6	YAW(811) Table Format	39
7	Data Types for ISIG Entries	42
8	Output Quantities Corresponding to Columns 7 through 33 of Data-Generation Type Card	53
9	Available Radar Parameters	61
10	Observation Types and Indicators	75
11	Basic Set of Tapes	148
12	Trajectory Prediction Tapes	148
13	Observation Generation Tapes	149
14	Orbit Determination Tapes	149
15	Subroutine Listing	151
16	NUMB Array	175
17	IFLAG Array	177
18	CNDT Array	179

LIST OF TABLES (contd.)

<u>Table Number</u>		<u>Page</u>
19	KIND Array	181
20	TREG Array	183
21	TEMP Array	185
22	STAT Array	187
23	Common Layout	189

Section 1.

BASIC INFORMATION

1.1 Introduction

This document is intended as a user's manual and therefore does not discuss the theory and mathematical details of TRACE-D except in a functional context. Section 1 of this report presents some program history, a brief summary of the modification process, and a statement of the program's present status. Section 2 specifies the functional capabilities of TRACE-D while Sections 3 and 4 describe input and output (patterned after the original TRACE-D document) and Section 5 contains programming information. Wherever pertinent, throughout the report, material from the Aerospace documentation has been freely incorporated.

1.2 Program History

The TRACE-D orbit determination program was developed by the Aerospace Corporation as a multipurpose, flexible computational tool for application to problems in orbit analysis. A major design objective was that the program be able to provide answers to a wide range of problems relating to orbit and system design, space vehicle performance, and force model analysis. It was not and is not a "real time" program and therefore it is most effective for post-flight analysis and also for research and investigative purposes. The program has been used extensively and successfully by the staff at Aerospace in just such an environment.

TRACE-D was originally written in FORTRAN II and FAP for use on the IBM 7094 computer in the "CHAIN" multi-coreload mode of operation. About thirty-percent of the program consisted of machine language (FAP) subroutines including the numerical integration package. The status of the program at the time of its release to us was reported to be operational for all functions.

1.3 Modification Process

The primary objective of this effort was to produce a version of TRACE-D operable on the IBM 7030 computer here at MITRE. To accomplish this, two separate yet simultaneous endeavors were carried out; one being to get the original TRACE-D program to run successfully on a nearby 7094 installation, and the other the actual conversion of routines to FORTRAN IV and STRAP and the reconstruction of the program. Upon completion of this phase, the next step was the checkout and "debugging" of the 7030 version of the program. This task was greatly facilitated and accelerated by running test cases for all options with both versions (7094 and 7030) of TRACE-D and checking all results.

Having accomplished the primary objective satisfactorily, work began on minor adjustments and additions to the program. Such features as observation residual plotting, an expanded earth geopotential capability, and a dynamic constraint matrix capability for site location adjustments were implemented. At the present time the program is operational on the 7030 computer and has produced meaningful and significant results for many MITRE orbit-related problems.

Section 2.

MAJOR PROGRAM FUNCTIONS

2.1 Trajectory Prediction

Basic to all the functions of the TRACE-D program is the generation of a time history (either in a forward or backward direction; see Section 3) of the position and velocity of a space vehicle in an inertial frame of reference. However, this inertial ephemeris as well as its associated ground track and altitude history are, in many instances, of interest in themselves. Thus, these computations are performed and printed out in the trajectory prediction mode of TRACE-D.

The motion of a space vehicle is generated by numerical integration of the appropriate differential equations of motion. Using a Cowell formulation (i.e., expressing the total acceleration vector as three components in a cartesian system $[\ddot{x}, \ddot{y}, \ddot{z}]$) three non-linear second-order differential equations are derived. A predictor-corrector numerical integration procedure based on "eighth-order differences" is used to obtain position (x, y, z) and velocity $(\dot{x}, \dot{y}, \dot{z})$ at any time t based on the known position and velocity at some initial time t_0 .

The total acceleration vector, mentioned above, is actually a sum of the effects of the perturbing forces that comprise the TRACE-D dynamic model. The earth geopotential effects (gravity) are included in the form of a spherical harmonic expansion with provision for zonal harmonics J_2 through J_{15} and all tesseral and sectorial terms through $J_{15, 15}$. Effects due to other bodies in the solar system (Sun, Moon, Venus, Mars, Jupiter) are computed from inverse-square law formulas and positions of the other bodies are obtained from tabulated coordinates stored on magnetic tape (planetary tape). Acceleration due to atmospheric drag is assumed to be directly proportional to the square of the velocity of the vehicle relative to the air. The atmospheric density is obtained from one of two different

model atmospheres that are incorporated into the program according to the user's choice. Instantaneous changes in the inertial velocity vector may be applied at specific times to simulate maneuvers such as orbit adjust or vehicle separation. Also, an included low-thrust acceleration term may be used to simulate thrust tailoff in cases involving large engines, long-term constant thrust, or, in some instances, leaking tanks or valves.

Although all of the above effects are programmed into the TRACE-D equations of motion, the actual model that is employed may include some, all, or none of these perturbations. The user has the option to choose the model by setting a series of indicators. The comparative listing of associated input and output quantities given in Table 1 suggests the range of potential application. Complete instructions for preparation of trajectory mode input data and a sample of a typical trajectory mode output listing are given in Sections 3 and 4.

2.2 Observation Generation

The object of the data generation function is to generate various forms of simulated measurements from a given definition of the ephemeris of a vehicle and the location of observing stations on the earth's surface. These measurements may be any of twenty different types from up to one hundred different sites and may be generated at user-specified frequencies. Both "clean" and "noisy" data are available, the latter being generated by adding noise of specified variances and biases to the "clean" measurements. Upon user request, the visibility function (i.e., the rise and set times) of a vehicle with respect to one or more stations may be obtained without printout of any intermediate data. When data is generated, it may be written on magnetic tape or punched on cards and is formatted such that it is readily available as input to the orbit determination process.

This option lends itself well to many applications, two of which are the following: studies of the effects of specific data imperfections

on orbit determination convergence behavior and the fitting of data using a different force model than that used to generate the data giving insight into the real-world problem of fitting live data with programmed (and always less than perfect) dynamic models.

Since the calculations performed for this option encompass all the calculations of the trajectory prediction mode, the input quantities include all those listed in Table 1 plus the additional information in Table 2. Available output quantities are listed in Table 2 also, but a more specific list of available data types with definitions is included in Sections 3 and 4.

2.3 Orbit Determination

Orbit determination is the primary function of the TRACE-D program and encompasses both the trajectory prediction and observation generation modes. Stated in simplest form the orbit determination problem consists of extracting information from observations (possible 20 types) of a space vehicle. The data is generally collected by a network of tracking stations on the surface of the earth. Nearly always, the information to be extracted includes the orbital elements but may include many other parameters of the dynamic model and of the tracking system.

The process of extraction in TRACE-D takes the form of a generalized least-squares differential correction procedure. More specifically, the goal is to determine values for a set of parameters (from the dynamic and/or observational model) such that the differences between the actual input measurements and corresponding values computed from the model (usually termed observation residuals) will be minimized in a least-squares sense. The solution set may be comprised of not more than one hundred parameters, of which not more than sixty may be trajectory-related parameters (i.e., initial conditions, geopotential coefficients, etc.). The amount of data that may be fitted is restricted only by the nature of the problem and not by the program.

Table 1.
Input/Output Quantities Associated with TRACE-D Trajectory Mode

Input Data	Output Data
1. Earth-model constants 2. Atmosphere model constants 3. Solar system constants 4. Units conversion factors	1. Satellite inertial position and velocity in rectangular and spherical coordinates 2. Magnitudes of geocentric-radius and inertial-velocity vectors.
5. Numerical integration-control constants 6. Epoch time 7. Position and velocity or orbital elements at epoch time 8. Satellite ballistic coefficient	3. Latitude and longitude of sub-vehicle point 4. Altitude above earth 5.* Differences between two trajectories in rectangular, spherical, classical element, and orbit-plane coordinates 6.* Time difference between corresponding points of two trajectories
9. Time, magnitude, and direction of velocity increments	7.* Magnitudes of distance and velocity difference vectors for two trajectories
* Associated with a trajectory differencing	

Table 1 (cont.)

Input Data	Output Data
<p>10. Interval, amplitude, and decay rate of low thrust</p> <p>11. Table of time points where output is to occur</p> <p>12. Parameter selection indicators</p> <p>13. Tape-unit numbers for trajectory differencing</p> <p>14. Latitudes and longitudes where special printouts are to occur</p>	<p>8.** Partial derivatives of trajectory position with respect to differential-equation parameters</p> <p>9.** Differences between changes in position and velocity produced by perturbing parameters and changes predicted by corresponding calculated partial derivatives</p>
<p>Items Printed Out at Special Time Points</p>	<p>10. At time when vehicle crosses ascending node: Output Items 1 through 4 above Classical orbital elements Mean and true anomaly Nodal regression rate Rate of advance of the line of apsides Apogee and perigee radius and altitude Keplerian, anomalistic, and nodal periods</p>

** Refer to the partial derivatives of trajectory position with respect to selected parameters.

Table 1 (cont.)

Input Data		Output Data
<p>15. Minor option indicators</p>	<p>Items Printed Out at Special Time Points</p>	<p>10. (continued) Revolution number (this set obtained by simple differencing rather than by formula) Nodal period Nodal period decay Nodal regression Nodal regression (this set obtained by simple differencing rather than by formula)</p> <p>11. At time of the event Orbit adjust magnitude and direction Magnitude of low thrust at start and stop times and at ascending node times</p> <p>12. At the time when the flight path angle passes through ninety degrees (roughly at apogee and perigee): Output Items 1 through 4 above</p> <p>13. At the time when the vehicle reaches local maximum or minimum altitude (when $h = 0$): Output Items 1 through 4 above</p>

Table 2.
 Input/Output Quantities Associated with
 TRACE-D Observation Generation Mode

<u>INPUT DATA</u>	<u>OUTPUT DATA</u>
1. All input listed in Table 1.	1. Computed observations
2. Site location coordinates	2. Rise-set times (per station)
3. Visibility function indicator	*3. Observation uncertainties
4. Observation types	
5. Observation frequencies	
6. Noise information	
7. Output mode (card, tape)	
8. Refraction specifications	
9. Uncertainty matrix for adBARV at epoch	

* Is the propagation and effect of input 9 above.

In fact, TRACE-D is capable of fitting observational data from six vehicles in a single orbit determination procedure. It allows for estimation of the trajectory initial conditions and drag coefficients associated with five satellites in addition to the usual parameters in a single satellite run.

The list of all possible input for the orbit determination mode is quite extensive as can be seen from Table 3. This is, of course, due to the comprehensive model programmed into TRACE-D for the purpose of wider and more varied applications. However, flexibility has not been sacrificed for completeness, so that the program is easily adaptable to either a non-real or more-real environment by simple input adjustment. The input and output capabilities of orbit determination are listed in Table 3 and described in detail in Sections 3 and 4. Table 4, which follows, is a complete list of all possible parameters that may be differentially corrected in TRACE-D.

Table 3.
 Input/Output Associated with
 Orbit Determination Mode

<u>INPUT</u>	<u>OUTPUT</u>
1. All input in Table 1.	1. Chronological list of all observations by satellite
2. Parameters in solution set	2. Variational equation solutions
3. Initial conditions for satellites 2-6	3. Trajectory printouts
4. Bounds for parameter correction	4. Observation partial derivatives
5. Station locations	5. Residuals
6. Data errors and biases	6. Station and observation type RMS summary
7. Data editing criterion	7. Computed and predicted RMS
8. Refraction correction indicators	8. Corrections
9. Iteration count	9. Covariance matrix
10. Constraint matrix for parameters	10. Correlation matrix
11. Observations from all vehicles	11. Solution set
12. Tape specifications	12. Tape of residuals

Table 4.
Parameter List*

1. Initial position and velocity components in either spherical, rectangular, or classical element form for up to six independent space vehicles.
2. Reciprocal of ballistic coefficients for up to six different satellites.
3. Up to six velocity increments (KICKS) for one satellite.
4. Amplitude and time constant for an exponentially decaying low thrust.
5. Zonal harmonic coefficients J_2 through J_{10} and all tesseral harmonics $J_{2,1}$ through $J_{6,6}$.
6. Constant biases on all types of observations.
7. Scale factors for range and range-rate observations.
8. Time biases (i.e., biases in reported times at which observations were made).
9. Latitudes, longitudes and altitudes above sea level of observing stations.

* On any one run up to 100 of listed quantities may comprise the solution set with not more than 60 from types 1-5.

Section 3.

Usage

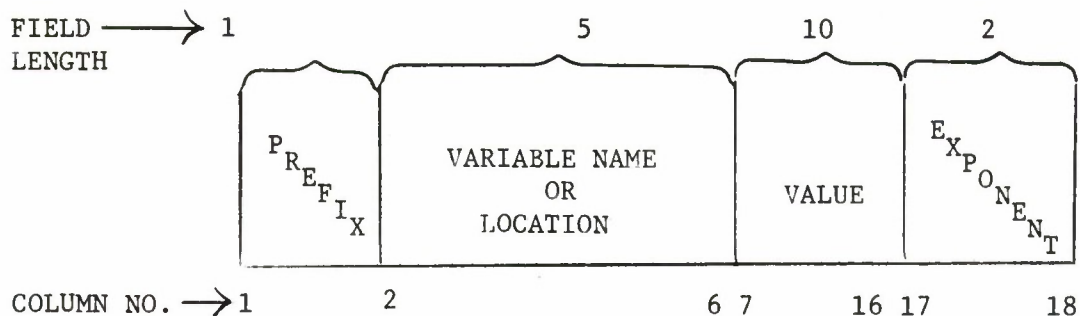
3.1 Preliminary Facts

In order to run the TRACE-D program the user need not concern himself with the internal elements of the program¹ nor worry about handling a cumbersome deck of cards. The entire program is stored on tape and can be used simply by attaching an appropriate data deck to the small basic running deck supplied by MITRE and submitting the job for execution. The basic running deck contains only tape usage information and the necessary instructions to trigger execution, therefore it is never necessary for the user to alter it in any way. Due to the varied tape requirements for each of the major functions, there are three versions of the basic running deck and the appropriate one must be used for each option exercised.

The input to the TRACE-D program falls into two categories: one which follows the normal FORTRAN IV rules of input and the other which is interpreted by a special routine in the program. The former method is used for all observing-station data (only a fraction of total input) and needs no description, while the latter method is used for all remaining input and requires a brief explanation.

The input routine accepts each piece of data from a data card in a field of eighteen columns in length with four distinct subfields as shown on the following page.

¹ The user who is curious or interested in the actual programming facts will find these concisely presented in Section 5.



1. Prefix Field - The prefix field is one column in length and can occupy columns 1, 19, 37, or 55. The mode of the input that follows is dictated by what is punched (or not punched) in the prefix field. The following are the permissible prefixes.

<u>Prefix</u>	<u>Data-Modes</u>
blank	Floating point number, number contains or implies a decimal point.
I	Fixed point number, no decimal point.
D	Hollerith information, data is not a number but a sequence of characters which can extend into the exponent field.
G	Used in connection with integration parameters, basic constants and the earth model. It indicates that card contains a symbolic name followed by a comment.
H	Followed by 1 or 2 in column 2. This is simply a header card to be printed at various places on the output. The number 1 indicates columns 1-80 and 2 indicates columns 81-132 on the printout.

2. Location Field - The location field is 5 columns in length and starts in columns 2, 20, 35 and 56. The information punched in the location field is either a symbolic name or a subscript. A symbolic

name defines a location in core where the data is stored. In the case of a subscript, it is used with respect to the immediately preceding symbolic name. Therefore, whenever a symbolic name is the name of a table, a subscript of 1 is attached to that name and those subscripts greater than 1 indicate storage relative to the start of the table. All names and subscripts should be left-adjusted within the field.

3. Value Field - The value field, 10 columns in length, starts in columns 7, 25, 43, or 61. This field together with the exponent field contains the numerical or hollerith data which is to be input. In the event the data is an integer (prefix = I) the exponent field is ignored. If the data is a floating point number (prefix column is blank, not punched) the decimal point, whenever it is not punched within the value field, is assumed to be after the last digit. Whenever hollerith data is input (prefix = D) the exponent field becomes an extension of the value field thus allowing for a total of twelve characters in the hollerith quantity. All data in the value field must be left-adjusted.
4. Exponent field - The exponent field, two columns in length, starts in columns 17, 35, 53, and 71. This field allows for a range of floating point numbers from 10^{-19} to 10^{-99} . An exponent of - 10 or smaller must start with the letter J (i.e., J0 = - 10, J5 = - 15, etc.). As in the value field the characters in the exponent field must be left-adjusted.

Although the input routine will accept four input fields per card, it is not necessary to use all four. One field used per card is just as correct since the rest of the card is ignored.

In addition to the precise field format there are a few other rules of input preparation.

1. The actual order of the data cards is almost immaterial, the only restriction being that all values with subscripts in the location field are placed in the input deck relative to the last previous symbolic name.
2. Any input which does not apply to the immediate run or is to have

a value of zero need not be specified.

3. In the case of two appearances of the same location symbol, the last one to appear defines the effective input.

4. The basic input units are feet, degrees, and seconds. Therefore, whenever the units are not stated then they are a combination of the basic set.

With the preceding basic description and the details on input preparation that follow, the user should have sufficient knowledge to use the TRACE-D program successfully.

3.2 Basic Data

The term "basic data" is defined as the data that is common to all the principal TRACE-D functions. This includes the constants for the integration procedure, the necessary physical constants, function indicator, trajectory specifications (like epoch time, initial conditions) and force model inputs.

3.2.1 Constants

The constants constitute two lengthy lists of input and involve quite a bit of keypunching. Because of this, there is available a standard set, in card deck form, which may be used as is, or altered for specific entries. This facility reduces the user's card preparation time and eliminates possibility of error.

In the event that the constants must be punched they must be formatted as shown on the following page.

3.2.1.1 Lines 1 - 19 Standard Set of Integration Constants¹

LINE #	PREFIX	NAME OR SUBSCRIPT	VALUE	EXPONENT
	Cols. 1,19,37,55	Cols. 2,20,38,56	Cols. 7,25,43,61	Cols. 17,35,53,71
1	G	INTEG		
2	I	1	1	
3	I	2	2	
2 4	I	4	1	
5	I	5	1	
6		11	1.00002516	
7		23	1.	JO
8		26	1.	
9		30	1.	
10		31	.015625	
11		32	64.	
12		33	1.	- 7
13	I	34	4	
14	I	35	1	
15	I	36	0	
16		37	.001	
17		38	0.	
18		40	2820.1763	
19	I	41	1	

¹ For definitions of the constants consult Table 5.

² Notice that there are entries missing in the INTEG list, like the 3rd one, for instance. This is because these entries are either not necessary for all options or are used by the program and not available to the user. This is true in both constants lists.

3.2.1.2 Lines 20 - 46 Standard Set Physical Constants¹

LINE #	PREFIX	NAME OR SUBSCRIPT	VALUE	EXPONENT
	Cols. 1,19,37,55	Cols. 2,20,38,56	Cols. 7,25,43,61	Cols. 17,35,53,71
20	G	C		
21		1	.43752691	- 2
22		2	.55303935	- 2
23		6	.5	
24		8	.43752691	- 2
25		9	1.	
26		13	3280.8399	
27		14	57.2957795	
28		15	20925738.	
29		16	332951.3	
30		17	.0122999	
31		18	.814979	
32		19	.107821	
33		20	317.887	
34		21	95.129	
35		22	23454.865	
36		23	3443.9336	
37		24	20925738.	
38		25	348762.3	
39		26	32.174	
40		30	348762.3	
41		31	1.5	
42		32	1.0471976	
43		33	3.14159265	
44		34	298.3	
45		35	300000.	
46		36	82505.922	

¹ For definitions of constants consult Table 5.

Table 5.

INTEG and C Constants Lists

INTEG	PARAMETERS OF THE TRAJECTORY INTEGRATION	
1	1	Formulation. 1 - Cowell (eqs. of motion), 2 - Encke (note: the Encke-T formulation is presently not available)
2	2	Differential equation subroutine. 1 - AMRK, 2 - COW
3		angle in degrees for changing mean to true equinox
4	1	Sun (4-9) are selectors for other-body perturbations
5	1	Moon If tape unit number at numb(18) is not zero,
6	0	Venus the perturbations are included or omitted
7	0	Mars according as the selector is non-zero or zero
8	0	Jupiter
9	0	Saturn
10	C(22)	Sun (10-15) are interpolation scale factors for use using contents of C(22), the number of earth-radii in an astronomical unit:
11	1.00002516	Moon
12	C(22)	Venus
13	C(22)	Mars
14	C(22)	Jupiter
15	C(22)	Saturn
16	0	Similar velocity scale factors. (not now used, and thru all zero).
21	0	
22		(used internally - Encke)
23	IE-10	E Bar, COW subroutine truncation error control parameter.
24		(used internally - Encke)
25		(used internally - Encke)
26	1.	A, see COW writeup.
27-29		(not used)
30	1.	Initial time step size.
31	.015625	Minimum time step size (1/64)
32	64.	Maximum time step size
33	1E-7	Kepler equation convergence criterion.
34	4	Ratio of Cowell step size to Runge-Kutta step size
35	1	if 1, do not recompute perturbations for corrector. if 2, do.
36		Flag for perturbation computation (used if INTEG(35) = 1).
37	.001	Least squares convergence criterion (relative)
38	0	Least squares convergence criterion (absolute)
39		(not used)
40	2820.1763	Speed of light (earth-radii/minute)
41	1	If non-zero, round position and velocity vectors for acceleration computation. If zero, truncate

Table 5 (cont.)

INTEG	PARAMETERS OF THE TRAJECTORY INTEGRATION	
42		Reserved for later use
C CONSTANTS		
1	.0043752691	Earth rotation rate (rad/min)
2	.0055303935	Gm, earth gravitation constant (ER**3/min**2)
3		Option for speed of light correction
4		B=1-E, relative semi-minor axis of ellipsoid (computed in CSET)
5		B**2/A**2 = (1-E)**2 (computed in CSET)
6	.5	Factor for decreasing bounds in L. S. solution
7		2*E-E**2 (computed in CSET)
8	.0043752691	Atmosphere rotation rate (rad/min)
9	1.	Earth radius
10		Input N for N-sigma residual editor
11		Input scale factor for N-sigma residual editor
12		If input non-zero, go thru 1 st iteration twice for sums
13	3280.8399	Feet/kilometer
14	57.2957795	Angle conversion factor
15	20925738.	A, earth radius in feet
16	332951.3	Relative mass of sun
17	.0122999	Moon
18	.814979	Venus
19	.107821	Mars
20	317.887	Jupiter
21	95.129	Saturn
22	23454.865	Earth-radii/astronomical unit
23	3443.9336	Nautical miles (6076.1155 ft)/earth radius
24	20925738.	I/O distance conversion factor
25	348762.3	I/O velocity conversion factor
26	32.174	Go (used for CDA/W and thrust/W)
27		Input parameter difference for trajectory differencing
28		Input threshold for percent difference for trajectory differencing
29		Constant for doppler rate
30	348762.3	Ft/sec per Er/min
31	1.5	Factor for increasing bounds in L. S. solution
32	1.0471976	Rad/min per deg/sec
33	3.14159265	PI
34	298.3	Reciprocal of E = ellipticity
35	300000.	Critical altitude (ft)
36	82505.922	Deg/day per rad/min
37-39		Direction cosines of body axis for look angle

3.2.2 Functions to be Performed

LINE #

47	D	ITIN	1234	
----	---	------	------	--

¹

Line 47 contains the ordered list of all functions to be performed during a single run. Selection of functions is governed in accordance with the following code numbers.

Code numbers	Functions
12	→ Orbit Determination
3	→ Trajectory Prediction
4	→ Data Generation

Up to twelve functions may be selected in any one run, i.e., the program will perform twelve specified functions in one continuous machine job. The example above specifies that an orbit determination be carried out first followed by a trajectory prediction and then a data generation.

3.2.3 Trajectory Specifications

3.2.3.1 Lines 48-54 Epoch

48	I	YEAR	1963	
49	I	MNTH	6	
50	I	DAY	15	
51		TZNE	0	
52		HR	12	
53		MIN	45	
54		SEC	15.5	

¹ Please notice that the field labels are no longer specified (i.e., Prefix, Value, etc.) but they are, of course, implied by the divisions.

In the usual case, wherein the year, month, and day are input with the year positive, the X-axis is directed to the vernal equinox. Alternatively, if the year is input negative, the X-axis would be directed to the longitude of Greenwich. The hour, minute, and second entries refer to midnight of zone time. Greenwich Mean Time is Time Zone 0.

3.2.3.2 Lines 55-61 Initial Conditions

55	I	ICTYP	2	
56		IC	126.1	
57		2	31.23	
58		3	89.	
59		4	14.	
60		5	22600114	
61		6	25117.3	

Line 55 indicates which of the ten IC types (1, 2, ..., 9, 0) are entered in Lines 56 through 61. The alternative ICTYP entries are characterized as follows:

- a. IC Type 1 Earth-centered inertial cartesian coordinates ($x, y, z, \dot{x}, \dot{y}, \dot{z}$ in units of feet and feet per second) (see Section 3.1.1.1).
- b. IC Type 2 Spherical coordinates ($\alpha, \delta, \beta, A, R, v$) in units of **degrees**, feet, and feet per second (see Section 3.1.1.2). In Line 14, negative r is interpreted as height above the earth's surface in feet. In Line 15, if v is negative, circular velocity is computed and used.
- c. IC Type 3 Orbital elements ($a, e, i, \Omega, \omega, \tau$) in units of feet, degrees, and minutes (see Section 3.1.1.3).
- d. IC Type 4 Same as Item b above, with longitude λ replacing right ascension α .
- e. IC Type 5 No IC's input. The last trajectory point of the immediately preceding case is used.
- f. IC Type 6 No IC's input. The corrected initial conditions from the last previous tracking run are used.

- g. IC Type 8 Either Type 1 or 2 above, but in units of earth radii, minutes, and radians. Type number is entered at CPRAM (see Section 5.1.2.2).
- h. IC Type 9 Same as Type 1 above, but in units of earth radii and earth radii per minute.
- i. IC Type 0 No IC's input. For a tracking run, two R, A, E sets are used from the data to calculate a set of initial conditions (see Section 3.6.6).

3.2.4 Force Model Inputs

3.2.4.1 Lines 62-68 Drag and T Matrix

62		DRAG	.01	
63	I	2	1	
64		4		
65		4		
66		6	-8.6	
67		7	-55.5	
68	I	TMATX	4	

Line 62 contains the drag parameter C_{DA}/W in square feet per pound and Line 63 contains the atmosphere model specification (ARDC 59 or Lockheed/ Jacchia). The ARDC model will be used when DRAG(2) is 0 and the Lockheed/Jacchia model when DRAG (2) is 1. If line 63 is a 1, Lines 64 and 65 contain quantities used in the Lockheed/Jacchia model.

Lines 64 and 65 contain d_1 and d_2 , respectively. These are values of certain constants in the Lockheed-Jacchia atmospheric density expressions. (Consult reference 1 for details).

An entry in Line 68, TMATX, will cause the T matrix (the 3×3 matrix describing the dependence of drag force upon vehicle position) to be used in the variational equations in accordance with the following options:

- a. TMATX = 0 T matrix is not used.
- b. TMATX = 1 Input $\partial\rho/\partial h$ is used with no earth flattening.
- c. TMATX = 2 Input $\partial\rho/\partial h$ is used with earth flattening.
- d. TMATX = 3 $\partial\rho/\partial h$ is calculated with no earth flattening.
- e. TMATX = 4 $\partial\rho/\partial h$ is calculated with earth flattening.

Also, with TMATX non-zero, Lines 66 and 67 should contain input values for $\partial\rho/\partial h$. Lines 66 and 67 contain $\partial\rho/\partial h$ for altitudes between 76 and 108 n. mi. and between 108 and 376, respectively.

It should be noted that input values for $\partial\rho/\partial h$ must be used with the ARDC 1959 model. If a variable C_D term is desired, the drag table option may be utilized. In this case, the drag parameter may be considered to consist of the product of two terms, $(C_{DA}/W) \times C'_D$, wherein C_{DA}/W is a constant which can be differentially corrected by the use of the variational equation and C'_D may be considered a function of Mach number below a certain altitude and as a function of altitude at points above that altitude. Alternatively, C'_D may be considered a function of time. In either case, use of the drag table is necessary.

When the drag table is not used, input of C_{DA}/W into the DRAG location does not change usual TRACE operation. In this case, C'_D is automatically set equal to 1. If the drag table is used, the following additional inputs are required:

- a. DRAG(10) If DRAG(10) = 0, tables not used.
If DRAG(10) = 1, Mach and altitude tables used.
If DRAG(10) = 2, time table only used.
- b. DRAG(11) Altitude above which altitude table is used and below which Mach table is used (needed if (DRAG(10) = 1).
- c. DRAG(12) = 0 Used by interpolation routine.

DRAG(13) Altitude table, or time table if
 through (35) DRAG(10) = 2 (h₁, C_D'(h₁), h₂, C_D'(h₂)
 . . . , h_n, C_D'(h_n), 0, 0, or
 t₁, C_D'(t₁), t₂, C_D'(t₂), . . . , t_n,
 C_D'(t_n), 0, 0).

d. DRAG(36) = 0 Used by interpolation routine.

DRAG(37) Mach table (stored as noted in Item c.
 through (59) above).

3.2.4.2 Lines 69-75 Other Body Perturbations

68	I	CTAPE	7	
----	---	-------	---	--

If perturbations due to other bodies in the solar system are to be included in the trajectory calculations, a planetary coordinate tape must be mounted and the logical-tape unit number 7 must be entered at CTAPE.

69	G	C		
70	I	4	1	
71	I	5	1	
72	I	6	0	
73	I	7	0	
74	I	8	0	
75	I	9	0	

Lines 69-75 contain the C constants that indicate which bodies are being considered. The six bodies corresponding to C(4) through C(9) are the Sun, Moon, Venus, Mars, Jupiter, and Saturn. Entering a 1 in C(4) implies that the Sun is to be considered, while entering a 0 in C(9) implies that Saturn is ignored. Therefore, in the example above only the Sun and Moon are used in the other-body perturbation computation.

3.2.4.3 Lines 76-79 Exponential Thrust

76		THRST		
77		2		
78		3		
79		4		

If an exponential thrust is to be used, the quantities T_1 in units of force/mass = ft/sec², T_2 in units of min⁻¹, and t_s and t_f in seconds from midnight of epoch date must be input at THRST, THRST(2), THRST(3), and THRST(4) locations, respectively.

3.2.4.4 Lines 80-96 Gravity Perturbations

80	I	IFLAG		
81	I	28	0	

Lines 80 and 81 above contain the input quantity IFLAG(28) = 0. This is an indicator that must be set in order to clear storage for the earth model that is to be specified.

82	I	IOB	10	
83	I	2	6	
84	I	3	10	
85	I	4	6	

Lines 82-85 define the number of terms to be used in the earth geopotential expansion. IOB(1) is the number of zonals and IOB(2) is the index of tesserals. Therefore, in the example above, 10 zonals will be used and tesseral terms up to and including the 6,6 term. Lines 84 and 85 specify IOB(3) and (4) which are the number of terms to be used in the V-matrix. The V-matrix is a measure of the dependence of the gravitational force upon vehicle position and is included as one of the many necessary calculations for the observation

partial derivatives (for differential correction).

If these two values are set to zero the V-matrix calculations are ignored. For a derivation of the V-matrix and its implications Appendix B of Reference 1 is recommended.

86		OBJZ		
87		2	1,826	-2
88		3	2,485	-6

Lines 86-88 specify the zonal coefficients in the following order:

OBJZ (1)		not used
(2)		J_2
(3)		J_3 etc.

89		OBJT		
90		2	1.556	-6
91		3	2.26	-6
92		4	1.72	-6
93		OBLT		
94		2	16.18	
95		3	35.62	
96		4	108.2	

Lines 89-96 specify the tesseral coefficients and the lambdas to be used, in the following order:

OBJT	J_{nm}	OBLT	τ_{nm}
(1)	J_{21}	(1)	τ_{21}
(2)	J_{22}	(2)	τ_{22}
(3)	J_{31}	(3)	τ_{31}
(4)	J_{32}	(4)	τ_{32}
(5)	J_{33}	(5)	τ_{33}
(6)	J_{41}	(6)	J_{41}
etc.		etc.	

3.2.5 Miscellaneous Inputs

3.2.5.1 Lines 97-100 Instantaneous Orbit Adjusts

97		PKICK	89020.31	
98		2	200.	
99		3	0	
100		4	62.	

Instantaneous orbit adjusts are input at PKICK. Line 97 contains t_1 (time of first orbit adjust, OA_1) in seconds from midnight of epoch; Line 98 contains K (magnitude of velocity change of OA_1) in feet per second; Line 99 contains θ (yaw angle for OA_1) in degrees, and Line 100 contains θ_p (pitch angle for OA_1) in degrees.

The TRACE-D program will accommodate up to six orbit adjusts. Additional cards may be added as necessary for OA_2 through OA_6 .

3.2.5.2 Lines 101-107 Extra Kicks

101	I	NXK	3	
102		XKICK	63456	
103		2	.2	
104		3	88721	
105		4	10.	
106		5	101018	
107		6	.02	

Up to fifty fixed orbit adjusts (i.e., instantaneous changes of the in-track velocity component) may be input at XKICK. It should be noted that these orbit adjusts are not parameters for differential correction, but are applied in the equations of motion only and are independent of the PKICK inputs. The number of extra kicks (≤ 50) is input at NXK, and the table of times and ΔV values is input beginning at XKICK. The format is time, ΔV , time, ΔV , etc., in units of seconds from midnight of epoch day and feet per second, respectively.

3.2.5.3 Line 108 Print Code

108	D	PRCDE	1	2	3	4	5	6	7	8	9	10	11	12
-----	---	-------	---	---	---	---	---	---	---	---	---	----	----	----

The print-code entry consists of two BCD words accommodating six character positions each. Entry of an X at any of these twelve positions will initiate corresponding outputs in accordance with the following:

- a. (1) Trajectory (trajectory only option).
- b. (2) Residuals (tracking only option).
- c. (3) Partial derivatives (tracking only option).
- d. (4) $A^T A$ after each iteration (tracking only option).
- e. (5) Variational equations (trajectory only option).

- f. (6) Orbital elements (trajectory only option).
- g. (7) Do not print station locations (tracking and data generation).
- h. (8) Not used.
- i. (9) Special trajectory prints¹
- j. (10) Orbital elements at ascending nodes only (trajectory only option).
- k. (11) Not used.
- l. (12) Suppress all trajectory print except ascending nodes (trajectory only option)²

3.2.5.4 Line 109 Equinox Precession Corrections

109		DALFG	.0002	
-----	--	-------	-------	--

The rotational position of the earth with respect to the inertial system is characterized by the right ascension of Greenwich at mid-night on the day of epoch (α_g) and is computed with respect to the mean equinox of epoch date. An additional factor for correcting to true equinox of epoch date optionally may be input at DALFG in units of degrees.

3.2.5.5 Lines 110-113 Direction of Integration

The TRACE-D program is capable of generating a time history of position and velocity in a forward or backward direction in any one run.

The inputs which determine this direction are INTEG(30), INTEG(31), INTEG(32). If these inputs are negative then backward integration from epoch time is assumed by the program. If positive,

¹ Prints will occur at times of maximum and minimum altitude above the oblate earth, at times when the flight-path angle equals 90 degrees and at special latitudes and longitudes if values are entered (see Section 3.3.6).

² If the option to write a binary trajectory tape (B7) has been selected, the writing of that tape is controlled by the PRIM entries (see Section 3.3.1).

as in the standard case, forward integration from epoch is performed.

110	G	INTEG	
111	30		-1.
112	31		-.01
113			-10.

The example shown above indicates to the program that backward integration must be performed starting at epoch with an initial time step of -1. minute (see Table 5 for the explanation of INTEG constants), a minimum time step of -.01 minutes and a maximum time step of -10. minutes.

When performing any of the three basic options, these inputs may be set negative. In trajectory generation a time history back from epoch will be produced. In the observation generation mode, observations previous to epoch may be generated. In the orbit determination mode, data previous to epoch may be fit. Generally this makes TRACE-D a more flexible program by making the position of epoch and the known initial conditions less rigid.

It should be noted that both backward and forward integration can not be performed in the same run but two runs would have to be made, each with a different direction of integration.

3.2.5.6 Line 114 Primary Scratch Tape

114	I	PTAPE	4
-----	---	-------	---

PTAPE is the number of the primary scratch tape that the program requires and 4 is its only permissible value. This card must be included in every data deck.

3.3 Trajectory-Only Data

In addition to the basic data previously described, the following data is relevant to the trajectory generation.

3.3.1 Lines 1-7 Print Time Vector Option

	1	I	PRTIM		
n	2	I	2		
t_0	3		3		
Δt_1	4		4		
t_1	5		5		
Δt_2	6		6		
t_2	7		7		

The above sequence of print times is for outputs selected by PRCDE entries (Line 108, Section 3.2.5.3). As many as nine sets of print intervals may exist (Line 2). In the case of the i^{th} set, output is from t_{i-1} to t_i at intervals of Δt_i , with all times in minutes from midnight of epoch date if PRTIM = 1 or from epoch if PRTIM = 0. Additional cards may be inserted if $3 \leq n \leq 9$. It should be noted that a normal print at epoch is automatic.

3.3.2 Lines 8-15 Variational Equation Partial Derivatives

8	D	CPRAM							
9	D	DPRAM							
10	D	3							
11	D	5							
12	D	7							
13	D	9							
14	D	KPRAM							
15	D	3							

An X entered in any CPRAM, DPRAM, or KPRAM character position causes the corresponding variational equation to be solved. Printout of the partial derivatives will occur only if an X is entered at Character Position 5 in the PRCDE print code entry location. The ordering of entries in the CPRAM, DPRAM, and KPRAM character position boxes is as follows:

a. CPRAM (Initial Condition Parameters) (Line 8)

The first position specifies which one of three types of initial conditions is applicable, and succeeding positions indicate the particular parameters that are desired in each case. Ordering of CPRAM parameter entries for initial condition (IC) Types 1, 2, and 3 as shown below.

(IC
Type)

(either)	1	x	y	z	\dot{x}	\dot{y}	\dot{z}	t_0				
(or)	2	α	δ	β	A	r	v	t_0				
(or)	3	a	e	i	Ω	ω	τ	t_0				

Ordering of CPRAM IC Parameter Entries

b. DPRAM and KPRAM (Differential Equation Parameters) (Lines 9 through 15)

The ordering of DPRAM and KPRAM parameter entries is shown below, wherein T_1 and T_2 are the exponential thrust parameters and a_i , K_i , θ_{y_i} , and θ_{p_i} are the OA number (1, 2, ..., 6), ΔV magnitude, yaw angle, and pitch angle, respectively.

Sixty differential equation parameters is the maximum number which may be selected for any one run.

DPRAM	DRAG	μ	J ₂	J ₃	J ₄	J ₅	J ₆	J ₇	J ₈	J ₉	J ₁₀	J ₂₁
3	J ₂₂	J ₃₁	J ₃₂	J ₃₃	J ₄₁	J ₄₂	J ₄₃	J ₄₄	J ₅₁	J ₅₂	J ₅₃	J ₅₄
5	J ₅₅	J ₆₁	J ₆₂	J ₆₃	J ₆₄	J ₆₅	J ₆₆	λ_{21}	λ_{22}	λ_{31}	λ_{32}	λ_{33}
7	λ_{41}	λ_{42}	λ_{43}	λ_{44}	λ_{51}	λ_{52}	λ_{53}	λ_{54}	λ_{55}	λ_{61}	λ_{62}	λ_{63}
9	λ_{64}	λ_{65}	λ_{66}		ω_a	T ₁	T ₂					

KPRAM	a ₁	K ₁	θ_{y_1}	θ_{p_1}	a ₂	K ₂	θ_{y_2}	θ_{p_2}	a ₃	K ₃	θ_{y_3}	θ_{p_3}
3	a ₄	K ₄	θ_{y_4}	θ_{p_4}	a ₅	K ₅	θ_{y_5}	θ_{p_5}	a ₆	K ₆	θ_{y_6}	θ_{p_6}

Ordering of DPRAM and KPRAM Differential
Equation Parameter Entries

3.3.3 Lines 16-18 Trajectory Comparison Options

16	I	IDIFF	1	
17	I	NTAPE	15	
18	I	DTAPE	14	

Tape units and case indicators required for the trajectory differencing function are as follows:

- a. IDIFF = 0 A regular trajectory run is indicated.
- b. IDIFF = 1 The reference trajectory will be written on the logical tape specified by NTAPE. If no entry is input at NTAPE, Logical Tape 15 will be used.
- c. IDIFF = 2 The differences between the present and reference cases are computed and written on the logical tape specified by DTAPE. If no entry is input at DTAPE, Logical Tape 14 will be used. The difference tape specified by DTAPE is rewound at the beginning of the case.
- d. IDIFF = 3 Conditions are the same as when IDIFF = 2 except that the tape specified by DTAPE is not rewound.

- e. IDIFF = 4 The tape specified by DTAPE is rewound at the beginning of the case and unloaded upon completion.
- f. IDIFF = 5 The tape specified by DTAPE is unloaded upon completion of the case.

The significance of the foregoing options is that if a single-comparison case is to be processed, IDIFF = 1 is used for the reference case and IDIFF = 4 for the perturbed case. If a series of perturbed cases are to be processed, IDIFF = 1 is used for the reference case, IDIFF = 2 for the first perturbed case, IDIFF = 3 for all intermediate cases, and IDIFF = 5 for the last perturbed case.

When this option is used, a special running deck must be obtained which defines the necessary tapes specified above.

3.3.4 Line 19 Revolution Number

19		REV	7	
----	--	-----	---	--

If an initial value other than zero is desired for the revolution number, it may be input at the REV location. This value must be re-initialized for each individual case.

3.3.5 Line 20 Trajectory Tape Generation

20	I	TTAPE	3	
----	---	-------	---	--

If TTAPE is non-zero, a binary trajectory tape will be generated on Logical Tape 19 in accordance with the following input options:

- a. TTAPE = 0 Tape will not be generated.
- b. TTAPE = 1 Tape will be rewound before generating but not unloaded after completion. This entry should be used for the first case when more than one case is involved.
- c. TTAPE = 2 Tape will not be rewound before generating and not unloaded after completion. This entry should be used for all intermediate cases.

- d. TTAPE = 3 Tape will be rewound before generating and unloaded after completion. This entry should be used when only one case is involved.
- e. TTAPE = 4 Tape will not be rewound before generating but will be unloaded after completion. This entry should be used for the last case.

This tape is not suitable for the trajectory-comparison option of the trajectory-only function.

For this option also, a special running deck containing the proper tape definitions must be used.

3.3.6 Lines 21-28 Latitude and/or Longitude Prints

n_1	21	I	LATPR	3	
	22		2	10.	
	23		3	15.	
	24		4	20.	
n_2	25	I	LONPR	3	
	26		2	200.	
	27		3	100.	
	28		4	180.	

Line 21 contains n_1 ($n_1 \leq 10$), or the number of special latitudes at which trajectory prints are requested, and Lines 22 through 24 contain the special latitudes. Additional cards may be added if $4 \leq n_1 \leq 10$.

Line 25 contains n_2 ($n_2 < 10$), or the number of special longitudes at which trajectory prints are requested, and Lines 26 through 28 contain the special longitudes. Additional cards may be added if $4 \leq n_2 \leq 10$.

Note that an X must be entered in Character Position 9 of the PRCDE entry if either of the foregoing options are selected.

This concludes the description of trajectory related data. For data deck samples and running deck setups see Section 3.6.

3.4 Observation Generation Data

The following data is pertinent only to the data generation option and is used in conjunction with the basic data (described in Section 3.3).

3.4.1 Lines 1-4 Special Output Option

1			IFLAG		
2		I	6	1	

If IFLAG(6) = 0, all generated data are printed. If IFLAG(6) = 1, rise, maximum elevation, and set times only are printed and the Data-Generation Specification Load Sheet II is not necessary except for listing of a card carrying TR in Columns 1 and 2 (see Section 3.4.5 and 3.4.6).

3		I	14		
---	--	---	----	--	--

If IFLAG(14) = 0, data are generated in time sequence until the available core space (bucket) is full. This output is then separated and printed by station in the same sequence as that of the input station cards. Further data are then generated until the bucket is again full, and the sort/print cycle is repeated. If IFLAG(14) = 1, data are printed as they are generated (i.e., in time sequence).

4		I	ETAPE	6	
---	--	---	-------	---	--

If ETAPE is non-zero, a BCD radar observation tape will be generated on the logical tape unit entered at ETAPE. The tape format will be the same as that of the tracking input data, including station locations and TF and TR cards.

3.4.2 Lines 5-23 Vehicle Attitude Specifications

y	5		YAW	1.	
p	6		PITCH	90.	
r	7		ROLL	180.	

Vehicle attitude may be specified by inputting yaw, pitch, and roll angles in degrees in the manner shown above. These entries normally are introduced in conjunction with aspect angle computations.

8		YAW		
9		811	1.	
10		812	120.	
11		813	.01	
12		814	.1	
13		815	0	
14		816	120.	
15		817	121.	
16		818	-.9	
17		819	-9.0	
18		820	0	
19		821	1420.	
20		822	1420.5	
21		823	360.	
22		824	0	
23		825	0	

The time history of vehicle attitude maneuvers may be specified by means of a table entered at YAW(811). The format of this table, which is used in connection with generation of radar aspect angles and may consist of up to three sets of five entries each, is itemized in Table 6.

The yaw-, pitch-, and roll-angle values that make up these input sets of angular rates are assumed to change at the rate given over the time interval defined by the start and stop times. Nominal orientation is zero yaw, pitch and roll which corresponds to the condition where the vehicle body axis is normal to the geocentric radius vector, the nose of the vehicle is in the in-track direction, and the top of the vehicle is in the direction of the extended radius vector.

Vehicle attitude at time of epoch and for the case where the entries in Table 6 are all zero (i.e., when nothing is input) is assumed to be the attitude specified at YAW, PITCH, and ROLL. If gaps in the time entries of the table are present, the angles are held constant at the last computed values.

Table 6.
YAW(811) TABLE FORMAT

Entry	Description
YAW(811)	Start time in minutes from epoch for first set of angular rates.
YAW(812)	Stop time in minutes from epoch for first set of angular rates.
YAW(813)	Yaw rate in degrees per minute.
YAW(814)	Pitch rate in degrees per minute.
YAW(815)	Roll rate in degrees per minute
YAW(816)	Start time in minutes from epoch for second set of angular rates.
YAW(817)	Stop time in minutes from epoch for second set of angular rates.
YAW(818)	Yaw rate in degrees per minute.
etc.	etc.

3.4.3 Lines 24-38 Data Error Inputs

24	B	NOISE	3 7 7 7 7 7 7 7 7	7 7
----	---	-------	-------------------	-----

If NOISE is non-zero (a positive octal number), normally distributed random noise with standard deviation and mean value specified by input at RAPAR is added to the generated data. The entry at NOISE is used to start the random-number generator.

25	M	RAPAR	05,99							
26	D	01,01	H	U		A	B	I	A	S
27		04,01								.057
28	D	01,02	A	L		H	B	I	A	S
29		04,02								200.

The RAPAR array is used to indicate bias values for measurements to be generated. Line 25 merely indicates to the program that the array is of maximum size 05,99. Lines 26 and 27 specify that for station HU and the azimuth measurements the bias value to be added is .057 degrees. Lines 28 and 29 indicate that for station AL and the height measurement computed from AL the bias value to be added is 200 feet. For additional entries the same two cards are repeated with increased subscripts.

30		SIGMA	200	
31		2	.1	
32		3	.1	
33		4	50.	
34	I	ISIG	1	
35	I	2	2	
36	I	3	3	
37	I	4	112	

Lines 30-37 contain the observation data weighting factors. For each SIGMA entry, a corresponding entry defining the sigma set and data type appears in ISIG Lines 34-37. The ISIG entries are of the form 100I + K, where I is the observation set number and K is the data type. Ten sets, corresponding to I = 0, 1, 2, ..., 9, may be entered. This selected value of I is the same as the entry in Column 5 of the station location card. (See Section 3,4,5.) The data type, K, must be one of those listed in Table 7.

In the above example, range, azimuth and elevation data would contain noise with a sigma of 200 feet, .1 degree and .1 degree respectively, while height would contain noise with a sigma of 5 feet.

38	REFR		
----	------	--	--

If elevation is a chosen measurement to be generated, then REFR is the input quantity that allows for elevation refraction correction. The computed elevation, E, is altered to account for refraction, using either

$$E' = E + \eta_{si} \cot E$$

if $E \geq 0.1$ radian, or

$$E' = E + \frac{1}{1000} \frac{\eta_{si} \times 10^6}{12+1000E} - \frac{80}{6+1000E}$$

if $E < 0.1$ radian and $\eta_{si} \neq 0$.

REFR contains the n_{si} term, wherein $i = 0, 1, 2, \dots, 9$. The appropriate value of i is entered on the station card in Column 6 (see Section 3.4.5). Nominally $n_{s0} = 3.12 \times 10^{-6}$. Rise, set, and maximum elevation values are determined from the geometric E which represents the elevation before refraction correction is applied. Additional cards may be inserted at this location if necessary.

Table 7.
Data Types for ISIG Entries

Data Type (K)	Data Description	Symbol
1	Range	R
2	Azimuth	A
3	Elevation	E
4	Topocentric right ascension	α_T
5	Topocentric declination	δ_T
6	Topocentric hour angle	HA
7	Geocentric right ascension	α_g
8	Geocentric declination	δ_g
10	Argument of latitude	u
11	Cross plane	v
12	Height	h
13	\hat{x}	\hat{x}
14	\hat{y}	\hat{y}
15	\hat{z}	\hat{z}
17	Range difference	P
18	Range difference	Q
19	Range rate	\dot{R}
20	\dot{R} difference	\dot{P}
21	\dot{R} difference	\dot{Q}

3.4.4 Lines 39-45 Orbit Covariance Matrix

39		ATAS	1.	-4
40		3	.5	-7
41		6	2.	-2
42		10	4	-2
43		15	2000.	
44		21	1.	

If observation uncertainties are to be calculated, a covariance matrix for the ADBARV elements at epoch must be input in lower triangular form at ATAS. The order of the elements is Row 1/Column 1 at ATAS(2), Row 2/Column 2 at ATAS(3).

In addition, the following input is needed.

45	D	CPRAM	2XXXXXX	
----	---	-------	---------	--

The CPRAM variable indicates to the program that the covariance matrix has been input and in the ADBARV notation. (For a more complete explanation of the CPRAM variable see Section 3.3.2).

3.4.5 Station Cards

The locations of tracking stations which are associated with the observations to be generated must be input by means of station cards carrying appropriate descriptive information.

Figure 1 on the next page shows the proper fields for the input that is described below:

- a. Station ID Columns 1 and 2 (ST).

No two stations may be identified by the same symbol. The three codes that are not permissible as station ID's are TS, TR, TF.

- b. Sigma Index Column 5

The sigma index identifies the set of observation sigmas

to be applied to data that is generated from this station (see Section 3.4.3).

- c. Type of Refractivity Correction Column 6
This indicator selects the type of refractivity correction which is to be applied to elevation readings. (This input depends on previous input. See Section 3.4.3).
- d. Latitude Columns 9-17
The latitude of the station is entered in degrees.
- e. Longitude Columns 19-27
The east longitude of the station is entered in degrees also.
- f. Altitude Columns 29-36
The altitude of the station is entered in feet.
- g. P, Q Indicators Columns 38-39 and 41-42
If P, Q, \dot{P} , \dot{Q} data (i.e., range difference and range rate difference between a master station and two slave stations) is to be generated these columns must contain the station ID's of the slave stations. Also, it is necessary to enter a station card for each slave station but columns 38-39 and 41-42 are to be left blank.

The station cards must be preceded by two cards with END in columns 1-3, and must be followed by a card with TS in columns 1-2.

3.4.6 Data Limit Specification Cards

- a. Station ID (ST) Columns 1-2
- b. Data Rate Columns 9-16
Time interval in seconds at which data for a given station are to be generated and testing interval for rise set option.
- c. Minimum Elevation Columns 18-23
The minimum elevation at which the vehicle is visible to this station.

- d. Maximum Elevation Columns 25-30
The maximum elevation at which the vehicle is visible to this station. Zero value implies a 90 degree limit.
- e. Maximum Range Columns 32-40
The maximum range in nautical miles to which the vehicle is visible. Zero value causes this test to be ignored.
- f. Start Time Columns 51-58
Start time from midnight of start date in days, hours, and minutes. Zero value implies that epoch is start time.
- g. Stop Time Columns 60-67
Stop time from midnight of start date in days, hours, and minutes.

The set of cards must follow the TS card in the deck and themselves be followed by a card with TR in the first two columns.

3.4.7 Data Type Cards

The following set of cards (which are the last in the card deck) specify the exact type of measurements to be generated from each station.

Figure 3 is a card image.

- a. Station ID Columns 1-2
- b. Observation Types Columns 7-33

An X in the appropriate column will produce specific measurements according to Table 8.

ST	Interval (sec.)*							Minimum Elevation (deg.)*			Maximum Elevation (deg.)*			Maximum Range (n mi)*							Start Time			Stop Time														
	9	10	11	12	13	14	15	16	18	19	20	21	22	23	25	26	27	28	29	30	32	33	34	35	36	37	38	39	40	day	hr	min	day	hr	min			
1																														60	61	62	63	64	65	66	67	
2																																						

NOTES

ST is the station identification code.
 Start and stop times are from midnight of epoch.
 If start time is 0 epoch itself is used.
 An asterisk (*) following a unit value indicates that a decimal point is necessary for that quantity.

Figure 2. Data Generation Limits Card Format

Table 8.
Output Quantities Corresponding to
Columns 7 through 33 of Data-Generation Type Card

Column	Output Quantity	Unit
7*	Range	n mi (ft on ETAPE)
8*	Azimuth	deg
9*	Elevation	deg
10*	Range rate	ft/sec
11-14*	\dot{P} , \dot{Q} , P, Q	ft/sec, ft
15	Azimuth rate	deg/min
16	Elevation rate	deg/min
17	Range acceleration	ft/sec ²
18	Mutual visibility (Output will be a list of numbers of stations visible at output time. Stations numbered in order of input on station cards. Number of stations, 8 maximum).	
19	Geodetic latitude of vehicle	deg
20	Longitude of vehicle	deg
21	Surface range from station to subvehicle point	n mi
22*	Altitude of vehicle	n mi (ft on ETAPE)
23	Doppler rate	
24	Look angle (Angle between a vehicle axis and the station/vehicle line of sight. The direction cosines of the vehicle axis in the basic inertial system must be entered in C(37), C(38), and C(39). These quantities	deg

* These quantities are output on ETAPE

Table 8 (cont.)

Column	Output Quantity	Unit
	may be input as constant or the user may provide a subroutine (FANG) to compute the direction cosines at each output point).	
25	Observation uncertainties. (If inverse $A^T A$ matrix for initial conditions is input at ATAS, the ADBARV elements are selected as parameters, and if an X is entered in Column 25, the $[A^T A]^{-1}$ is updated to observation times and the standard deviations in the quantities R, A, E, \hat{R} , \hat{A} , \hat{E} are derived and printed. The uncertainties are only those due to the uncertainty in the ephemeris which is implied by the given $[A^T A]^{-1}$ for the epoch conditions).	Same units as observations
26	Angle kappa (K). (Angle between station line-of-sight and geocentric radius vectors).	deg
27	Aspect angles. (Angle 1 (Φ) is defined as the angle between the vehicle yaw axis and projection of the station line-of-sight vector in the roll plane. Angle 2 (Θ) is defined as the angle between the vehicle roll axis and the line-of-sight vector to the station.	deg
28	Signal attenuation = $-40 \log_{10} R$, where R is slant range in feet	db
29*	\hat{x} , \hat{y} , \hat{z} (Same rectangular earth-fixed (X through Greenwich) geocentric quantities accepted as Type 5 observations for orbit determination).	n mi (ft on ETAPE)

* These quantities are output on ETAPE

Table 8 (cont.)

Column	Output Quantity	Unit
30*	Topocentric right ascension and declination	deg
31*	Geocentric right ascension and declination	deg
32*	Topocentric hour angle	deg
33*	Vehicle-centered argument of latitude and cross-plan angle	deg

* These quantities are output on ETAPE

3.5 Orbit Determination Data

This section gives a description of all the pertinent data for a differential correction run to be used in conjunction with the previously described basic data.

3.5.1 Lines 1-14 Multiple Satellite Option

As was mentioned in Section 2, TRACE-D will accept measurements for up to six satellites on any one run. The method of specifying the input for these vehicles is shown below.

Year	1	I	SAT2	1964	
Month	2	I	2	2	
Day	3	I	3	10	
Hour	4		4	3.	
Minute	5		5	30.	
Second	6		6	52.	
ICTYP	7	I	7	2	
IC	8		8	352.	
	9		9	10.	
	10		10	90.05	
	11		11	165.	
	12		12	22580632.	
	13		13	25205.3	
DRAG	14		14	.015	

If observations for a second satellite are to be input, Lines 1 through 14 are used for entry of epoch, initial conditions, and drag coefficient for Satellite 2. Lines 1 through 3 contain the year, month, and day, and Lines 4 through 6 contain the hour, minutes, and seconds, Greenwich time. Line 7 indicates the type of initial conditions that may be entered in Lines 8 through 13 (Type 1, 2, 3, 4, 8, or 9). Line 14 contains the drag coefficient (CDA/W). The input initial conditions

for IC Types 1, 2, and 3 is as shown in Section 3.3.2.

b. DPRAM (Differential Equation Parameters)
(Lines 16 through 20)

The ordering of DPRAM differential equation parameter entries is as shown in Section 3.3.2. However, in this application the T_1 and T_2 parameters are associated with Satellite 1 only.

c. PSAT2 through PSAT6 (Initial Condition and Drag Coefficient Parameters for Satellites 2-6)
(Lines 21 through 25)

The ordering of PSAT IC and drag parameter entries for Satellites 2 through 6 is shown below.

PSAT2	α_2	δ_2	β_2	A_2	r_2	v_2	t_{0_2}	DRAG ₂
PSAT3	α_3	δ_3	β_3	A_3	r_3	v_3	t_{0_3}	DRAG ₃
PSAT4	α_4	δ_4	β_4	A_4	r_4	v_4	t_{0_4}	DRAG ₄
PSAT5	α_5	δ_5	β_5	A_5	r_5	v_5	t_{0_5}	DRAG ₅
PSAT6	α_6	δ_6	β_6	A_6	r_6	v_6	t_{0_6}	DRAG ₆

It is important to note that only IC Type 2 may be specified for Satellites 2 through 6.

d. KPRAM (Orbit Parameters for Satellite 1)
(Lines 26 and 27)

Ordering of KPRAM orbit adjust parameters is as previously shown in Section 3.3.2. It should be noted that the orbit adjusts are for Satellite 1 only.

Sixty trajectory parameters is the maximum number which may be selected for simultaneous solution.

3.5.2.2 Radar Parameters

28	M	RAPAR	05, 99							
29	D	01, 01	B N	L A T						
30		03, 01	.01							
31		04, 01								
32	D	01, 02	C K 2 4 R B I A S							
33		03, 02	500.							
34		04, 02	750.							
35	D	01, 03	H U	T B I A S						
36		03, 03	.001							
37		04, 03	.0035							

Line 28 indicates that the data listed subsequent to RAPAR on the load sheet will be input into a 5×99 matrix array which has been preset to zero. The columns of this array correspond to parameters, and the rows correspond to parameter identification (Positions 1 and 2), bounds (Position 3), and bias estimates (Position 4) respectively. Row 5 is currently not used.

Lines 29 through 31 specify the first applicable radar parameter. Line 29 contains the station name (Positions 1 and 2), pass identification (Positions 3 and 4), and parameter name (Positions 5 through 10). Lines 30 and 31 contain the bound and initial value, respectively, in feet, degrees, and minutes except for \dot{R} , \dot{P} , and \dot{Q} , which are in feet per second. If the parameter is station latitude, longitude, or altitude, the initial value is taken from the station location card.

If the pass identification character position is left blank, all data with the indicated station name will be used to correct the parameter. If the pass identification is not omitted, only data that are identified by both the indicated station name and indicated pass identification will be used to correct the parameter. If the radar parameter specified is station latitude, longitude, or altitude, the pass identification is ignored and all data with the station name are used for the parameter correction.

Lines 32 through 34 and Lines 35 through 37 specify the second and third radar parameters respectively. Station names, pass identifications, parameter names, bounds, and initial values are treated in the same manner as the inputs in Lines 29 through 31 described above. Additional cards may be added in cases where more than three radar parameters are involved. Available radar parameters are listed in Table 9.

Note that the total number of parameters which may be selected for simultaneous solution must be less than one hundred.

Table 9.

PARAMETER	SYMBOL
Station latitude	LAT
Station longitude	LONG
Station altitude	ALT
Time bias	TBIAS
Range bias	RBIAS
Azimuth bias	ABIAS
Elevation bias	EBIAS
Topocentric right ascension bias	RTBIAS
Topocentric declination bias	DTBIAS
Topocentric hour angle bias	HABIAS
Geocentric right ascension bias	RGBIAS
Geocentric declination bias	DGBIAS
Argument of latitude (u) bias	UBIAS
Cross plane (v) bias	VBIAS
Height bias	HBIAS
\hat{x} bias	XBIAS
\hat{y} bias	YBIAS
\hat{z} bias	ZBIAS
P bias	PBIAS
Q bias	QBIAS
Range-rate bias	RDBIAS
\dot{P} bias	PDBIAS
\dot{Q} bias	QDBIAS
Range scale factor (K_R)	KR
Range-rate scale factor (K_D)	KD

3.5.3 Lines 38-50 Parameter Bounds

38		BNDS	.5	
39		2	.5	
40		3	.1	
41		4	.5	
42		5	1000.	
43		6	5	
44		7	.05	
45		8		
46		9		
47		10		
48		11		
49		12		
50		13		

A bound must be entered for each parameter selected. These bound entries must be in the same sequence as the parameters. For each iteration of the differential correction process, the change in each parameter is less in absolute value than the corresponding bound if that bound is positive, zero if the corresponding bound is zero, or unrestricted if the corresponding bound is negative.

3.5.4 Lines 51-62 Observation Sigmas

51		SIGMA	100.
52		2	.5
53		3	.5
54		4	1000.
55		5	200.
56		6	300.
57	I	ISIG	1
58	I	2	2
59	I	3	3
60	I	4	113
61	I	5	114
62	I	6	115

The observation sigmas for each observation type must be input in the same manner as was previously well described in Section 3.4.3.

3.5.5 Line 63 Maximum Iterations

63	I	MAXIT	4
----	---	-------	---

The symbol MAXIT must be input with an integer value to specify a stopping point to the run. If the differential correction process has not converged at the end of MAXIT iterations, the process will be terminated.

3.5.6 Lines 64-66 Residual Editing

64		CEDIT	3
65		2	.9
66		3	1

If CEDIT is zero, no editing is done. If CEDIT is non-zero, residuals will be edited in accordance with the following:

- a. CEDIT < 0 Residuals greater than (input sigma × |CEDIT|) will be discarded.
- b. CEDIT > 0 Residuals greater than (statistical sigma from the previous iteration × CEDIT) will be discarded. No editing is done on Iteration 1. Sigmas are computed for the first five data types encountered for each station.

Line 65 represents a scale factor such that if CEDIT(2) is non-zero, CEDIT is replaced by (CEDIT × CEDIT(2)) at the end of each iteration. If CEDIT(2) is zero, CEDIT is not modified.

Line 66 is a special option wherein if CEDIT(3) is non-zero, Iteration 1 will be repeated with editing performed with the sigmas computed during the first pass through Iteration 1. This will allow editing to be done on all iterations with computed sigmas.

Sigmas (rms) for the first five data types for each station are computed and printed at the end of each iteration regardless of the residual-editing option selected.

3.5.7 Data Correction Factors

3.5.7.1 Lines 67 and 68 Elevation Angle Refraction

67		REFR		
68		2	4.0	-6

A table of refraction indices n_1 , which may contain up to ten values, may be input starting at REFR. The entry used to compute refraction corrections for radar elevation observations is determined by the type number contained in Column 6 of the corresponding station location card. A zero in Column 6 causes the entry at REFR to be used, a 1 in Column 6 causes the entry at REFR + 1 to be used, etc.

If the table contains no entries, the value 312.0×10^{-6} , which is built in at location REFR, will be used to

compute refraction corrections for all data whose station location cards contain zero in Column 6. All other positions of the table are assembled as zeros.

3.5.7.2 Range Refraction Correction

69		RREFC	1	
----	--	-------	---	--

Refraction corrections to all range observations will be computed and applied if RREFC is non-zero.

3.5.7.3 Line 70 Propagation Time Correction

70		SLT	-2820.1763	
----	--	-----	------------	--

The velocity to be used in calculating the observation time correction due to propagation time is entered at SLT in units of earth radii per minute. In the absence of an entry, no correction will be applied. If an entry is present the correction will be applied to times associated with R, A, E, \dot{R} , h, P, Q, \dot{P} and Q data only.

3.5.8 Lines 71, 72 Data Tape Options

71	I	IBCDI	6	
72	I	IBINI	1	

If the radar observation and station location information is to be input via a BCD tape other than the normal FORTRAN system input tape, the tape number must be specified at IBCDI as 11. If a binary tape containing compacted radar data produced by a previous run is to be input, IBINI must be specified.

3.5.9 Lines 73, 74 True Equinox Correction

73		DALFG	-.004	
74		2		

An additive factor may be applied to the computed right ascension of Greenwich at midnight of epoch day by entering the appropriate value in units of degrees at DALFG for Vehicle 1, at DAFLG(2) for Vehicle 2, etc. This entry usually is used to correct from mean to true equinox reference coordinates.

3.5.10 Lines 75-78 Proximity Indicator

ϕ^*	75		ANØM1	
λ	76		2	
h	77		3	
R_0	78		4	

During an orbit determination run, an indicator may be obtained whenever the trajectory passes within a given distance (range) of a point on the surface of the earth by input of geodetic latitude (deg), east longitude (deg), and altitude (n mi) of the point at ANØM1 and the succeeding two positions and of the testing distance (the range from the point to the vehicle) at AMON1(4). Testing and printing is done for up to three such sets of input at AMON1, ANOM2, and ANOM3.

3.5.11 Lines 79 on Parameter Constraint Options

There are two different parameter constraint options available in TRACE-D. Both are described below in detail.

3.5.11.1 General Constraint Matrix

Option 1 allows the user to apply linear constraints to any of the variables in the parameter set, and to specify these constraints by means of an input matrix set up as shown below.

79	I	KNST	4
80	I	BLIST	1
81			1
b ₁₁	82		1
83	I		2
84	I		2
b ₂₂	85		1
86	I		3
87	I		3
b ₃₃	88		1
89	I		4
90	I		4
b ₄₄	91		1
92	I		5
93	I		1
b ₅₁	94		-1
95	I		6
96	I		2
b ₆₂	97		.5
98			5
99	I		5
c ₅₁	100		6
101	I		7
102	I		5
103			1

The clearest explanation of how this constraint matrix works is an example. Therefore, in the case shown above it is assumed that n parameters are to be solved for where $(p_1, p_2, \dots, p^n) = P$. The ordering of the P_i corresponds to the

order of the X 's for the CPRAM, DPRAM, and KPRAM and the RAPAR arrays, respectively. Further assuming that these parameters are to be subjected to m linear constraints, which, for example for $n = 6$ and $m = 2$ might be $p_1 + p_5 = 6$, $p_2 - 2p_6 = 0$, KNST above would be equal to $(n - m) = 4$, or the number of effective (unconstrained) parameters.

The BLIST constraint matrix is represented by the factor B in the expression $p = B\bar{p} + c$, where the \bar{p} are the effective parameters. In connection with the foregoing example, this expression would assume the form

$$\underbrace{\begin{bmatrix} p_1 \\ p_2 \\ p_3 \\ p_4 \\ p_5 \\ p_6 \end{bmatrix}}_p = \underbrace{\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -1 & 0 & 0 & 0 \\ 0 & .5 & 0 & 0 \end{bmatrix}}_B \times \underbrace{\begin{bmatrix} \bar{p}_1 \\ \bar{p}_2 \\ \bar{p}_3 \\ \bar{p}_4 \end{bmatrix}}_{\bar{p}} + \underbrace{\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 6 \\ 0 \end{bmatrix}}_c$$

Pertinent constraints are applied by input of the augmented $(n + 1)$ by $(n - m + 1)$ matrix

$$\begin{bmatrix} B & c \\ 0 & 1 \end{bmatrix}$$

in the BLIST array. If a_{ij} is an element of this augmented matrix, then i , j , and a_{ij} would be input. The inputs for the example given above would be as indicated in Lines 79-103. KNST (line 70) is input as 4 and then the BLIST matrix follows. Lines 80, 81, and 82 specify that BLIST (1, 1) is a 1 and lines 83, 84, and 85 that BLIST (2, 2) is a 1, etc. Elements of the matrix not input are assumed to be zero. In this way any subset of the set of parameters may be linearly constrained and the constraint matrix may be input to the program in the exact same manner.

3.5.11.2 Special Application to Station Location

The other option available is a specific case of the general constraint matrix which is applicable in the following type of problem. Consider a differential correction run with data from a tri-static system and a set of parameters including the latitudes, longitudes and altitudes of the three stations. In such a case, by choosing this constraint option, the correction of the station coordinates can be performed such that the baseline distances are held constant.

Mathematically, this implies that three constraining equations¹ are applied to the nine station locations; more specifically they are of the following form.

$$\Delta\phi_1 = a_1 \Delta\theta_1 + a_2 \Delta H_1 + a_3 \Delta\theta_2 + a_4 \Delta H_2 + a_5 \Delta\phi_3 + a_6 \Delta H_3$$

$$\Delta\phi_2 = b_1 \Delta\theta_1 + b_2 \Delta H_1 + b_3 \Delta\theta_2 + b_4 \Delta H_2 + b_5 \Delta\phi_3 + b_6 \Delta H_3$$

$$\Delta\theta_3 = c_1 \Delta\theta_1 + c_2 \Delta H_1 + c_3 \Delta\theta_2 + c_4 \Delta H_2 + c_5 \Delta\phi_3 + c_6 \Delta H_3$$

where

(θ_1, ϕ_1, H_1) are the three sets of latitude,
 (θ_2, ϕ_2, H_2) Longitude, and altitude for
 Stations 1, 2, and 3.
 (θ_3, ϕ_3, H_3)

and a_i, b_i, c_i $i = 1, \dots, 6$ are the 18 coefficients of the three equations.

With the equations in this particular form, it seems that the general constraint option could be applied easily. However, there are two reasons for the separate treatment of this application that are not immediately apparent. First, the constants a_i, b_i, c_i $i = 1, \dots, 6$ are functions of the current station location² and are not easily and accurately calculable by the user. Second, since

¹ The detailed derivation of this particular form of the constraining equations is not given here but may be found in Reference 3.

² The exact expressions for the coefficients can be found in Reference 3.

the constants are functions of the current station locations, they must be reevaluated every time the station locations change (i.e., after every iteration of the correction process the constants must be reset since the station locations have been adjusted). In other words, the type of constraint matrix needed here is a dynamic one that is adaptable to change throughout the estimation procedure. It is now obvious that the general constraint matrix of Section 3.5.11.1 is too rigid for this purpose.

Thus, added to the TRACE-D program is the capability to compute these necessary constants from input information, insert them into the appropriate location of the constraint matrix, recompute the constants as a function of the new station locations after each iteration and adjust the constraint matrix accordingly. Once the user has set up the appropriate input the rest is performed by the program.

The input necessary is best described with an example. Consider a differential correction run with data from three stations and a parameter set consisting of the ADBARV elements, drag, and station locations. To employ the fixed baseline distance constraints on the station locations consider B in the following expression.

$$\Delta \rho' = B \Delta P + c$$

There are 16 parameters to be estimated but there are 3 constraint equations, therefore there are 13 effective or unconstrained parameters. B is then of dimension 16×13 and looks like this:

$$\begin{array}{c}
 [\Delta\rho'] = [B] \\
 \begin{array}{l}
 \Delta\alpha \\
 \Delta\delta \\
 \Delta B \\
 \Delta A \\
 \Delta R \\
 \Delta V \\
 \Delta \text{ drag} \\
 \Delta \text{ lat}_1 \\
 \Delta \text{ long}_1 \\
 \Delta \text{ alt}_1 \\
 \Delta \text{ lat}_2 \\
 \Delta \text{ long}_2 \\
 \Delta \text{ alt}_2 \\
 \Delta \text{ lat}_3 \\
 \Delta \text{ long}_3 \\
 \Delta \text{ alt}_3
 \end{array}
 =
 \begin{array}{cccccccccccc}
 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1
 \end{array}
 \begin{array}{l}
 \Delta\alpha \\
 \Delta\delta \\
 \Delta B \\
 \Delta A \\
 \Delta R \\
 \Delta V \\
 \Delta \text{ drag} \\
 \Delta \text{ long}_1 \\
 \Delta \text{ alt}_1 \\
 \Delta \text{ long}_2 \\
 \Delta \text{ alt}_2 \\
 \Delta \text{ lat}_3 \\
 \Delta \text{ alt}_3
 \end{array}
 +
 \begin{array}{l}
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0
 \end{array}
 \end{array}$$

The quantities $a_i, b_i, c_i, i = 1, \dots, 6$ are, of course, the coefficients in the constraint equations which are unknown to the user.

This B matrix is input in exactly the same manner as the general constraint matrix except that each element that is a coefficient (either a_i, b_i, c_i) must be input with a value of -10,000. This is merely to indicate to the program the position in the matrix of these terms.

Lines 104 on show the appropriate format for the necessary input of this case.

104		NUMB		116	I	8	
105	I	44	-1	117	I	8	
106	I	KNST	13	118	I	-10,000.	
107	I	BLIST	1	119	I	8	
108	I		1	120	I	9	
109			1	121		-10,000.	
110	I		2				
111	I		2		etc.		
112	:		1				
113	:						
114	etc.						
115							

Lines 104 and 105 specify the quantity NUMB(44) which must be input as a - 1 to choose this constraint option. Line 106 is the number of unconstrained parameters in the parameter set. Lines 107 on are the non-zero elements of the B matrix entered in order.

3.5.12 Station Identification Cards

The locations of tracking stations or of points on the surface of the earth which are associated with observations must be input by means of station cards carrying appropriate information indicating the manner in which the corresponding observations are to be processed. These cards were previously discussed in Section 3.4.5 and shown in Figure 1, but the format is included again here for completeness.

- a. Columns 1 and 2 (ST): Station identification symbol. No two stations may be identified by the same symbol or any one station by the symbol TS.
- b. Column 5: Sigma index identifying observation-sigma set to be applied to data from corresponding station. The sets of sigmas are input with the base data.
- c. Column 6: Type of refractivity correction to be used for elevation readings from this station. Refractivities are numbered in their input order within the base data (see Line 67, REFR).

- d. Columns 9 through 17: North latitude of station in degrees.
- e. Columns 19 through 27: East longitude of station in degrees.
- f. Columns 29 through 36: Altitude of station in feet.
- g. Columns 38/39 and 41/42: If a station reports P, Q, or P̄, Q̄ data, Columns 38/39 and 41/42 contain the two letter symbols for the associated station(s) of the tracking configuration. Each such associated station must be represented by a separate station card, but it is not necessary for Columns 38/39 and 41/42 to be filled out on the latter.

These cards must be preceded by a card with END in Columns 1-3 and followed by a card with TS in Columns 1 and 2.

3.5.13 Observation Data Cards

The observations to be processed must be the last set of cards in the deck and must follow the station location cards.

Since the number of observations that may be input to TRACE-D is unlimited, there is a flocking procedure that must be followed. A flock of data consists of 200 or less observation cards for a single satellite. There is no limit to the number of flocks that can be stacked; however, each flock must be followed by a card with TF in Columns 1 and 2 and the times associated with the observations of a flock can never be earlier than the latest time of the previous flock. This means that the data is not time sorted within a flock but the flocks are sorted according to earliest and latest times therein contained.

The contents of an observation card is formatted in the following way, as shown in Figure 4.

- a. Columns 1 and 2 (ST): Station Identification, symbol which must correspond to a station location card.
- b. Columns 3 and 4: Pass identification (optional).
- c. Columns 5 through 21: month (columns 5 and 6), day (columns 7 and 8), hours (columns 9 and 10)

minutes (columns 11 and 12), and seconds (columns 13-21), of the corresponding observations relative to Greenwich Mean Time.

- d. Column 22: Observation set number.
- e. Columns 23-76: Observation 1 (columns 23-40), Observation 2 (columns 41-58), Observation 3 (columns 59-76).
- f. Column 77: Card number indicating observations, variances, or covariances.

The observation set (d) number and the card number (f) are the two indicators that define exactly what type of observations are contained on each card. Table 10 gives a complete listing of all types according to observation set number and card number.

After the last observation card in the deck, a TF card is not necessary, however a card with TR in Columns 1 and 2 plus an END card must be attached as the last two cards of the deck. If data from more than one satellite are to be used, the Satellite 1 data are set up in the same manner except that the TR card must be replaced by a TT card. The data for Satellite 2 are then similarly arranged. If Satellite 2 is the last vehicle, corresponding data are followed by a TR card and an END card: if it is not the last satellite, data are followed by a TT card. Data for Satellites 3 through 6, as applicable, are added in the same manner. A TR card rather than a TT card must follow the data corresponding to the last satellite, and an END card must follow the TR card. See Section 3.6 for a picture of the correct setup.

3.6 Input Deck Arrangements

Since the basic running deck to be used for each function to be performed can be obtained, the user need not concern himself with its contents. Therefore in each of the Figures the separate parts of this deck are ignored and it is labeled totally as the basic running deck. The categories of data used are described in detail in previous sections (for instance, Basic Data is explained in Section 3.2, etc.).

Observation Set Number (Column 22)	Observation Card Type (Column 77)	Field 1	Field 2	Field 3
1	0	Slant range (R)	Azimuth (A)	Elevation (E)
1	1	Variance (R)	Variance (A)	Variance (E)
1	2	Covariance (R,A)	Covariance (R,E)	Covariance (A,E)
2	0	Topocentric right ascension (α_T)	Topocentric declination (δ_T)	Topocentric hour angle (HA)
2	1	Variance (α_T)	Variance (δ_T)	Variance (HA)
2	2	Covariance (α_T, δ_T)		Covariance (δ_T, HA)
3	0	Geocentric right ascension (α_g)	Geocentric declination (δ_g)	
3	1	Variance (α_g)	Variance (δ_g)	
3	2	Covariance (α_g, δ_g)		
4	0	Argument of latitude (u)	Cross plane (v)	Altitude (h)
4	1	Variance (u)	Variance (v)	Variance (h)
4	2	Covariance (u,v)	Covariance (u,r)	Covariance (v,h)
5	0	\hat{x}	\hat{y}	\hat{z}
5	1	Variance (\hat{x})	Variance (\hat{y})	Variance (\hat{z})
5	2	Covariance (\hat{x}, \hat{y})	Covariance (\hat{x}, \hat{z})	Covariance (\hat{y}, \hat{z})
6	0	Slant range (R)	Range difference (P)	Range difference (Q)
6	1	Variance (R)	Variance (P)	Variance (Q)
6	2	Covariance (R,P)	Covariance (R,Q)	Covariance (P,Q)
7	0	Range rate (\dot{R})	Range rate difference (\dot{P})	Range rate difference (\dot{Q})
7	1	Variance (\dot{R})	Variance (\dot{P})	Variance (\dot{Q})
7	2	Covariance (\dot{R}, \dot{P})	Covariance (\dot{R}, \dot{Q})	Covariance (\dot{P}, \dot{Q})

Table 10. Observation Types and Indicators

3.6.1 Trajectory Prediction Deck Arrangement

When the function to be performed is a single trajectory prediction (function code ITIN = 3), the arrangement is as in Figure 5.

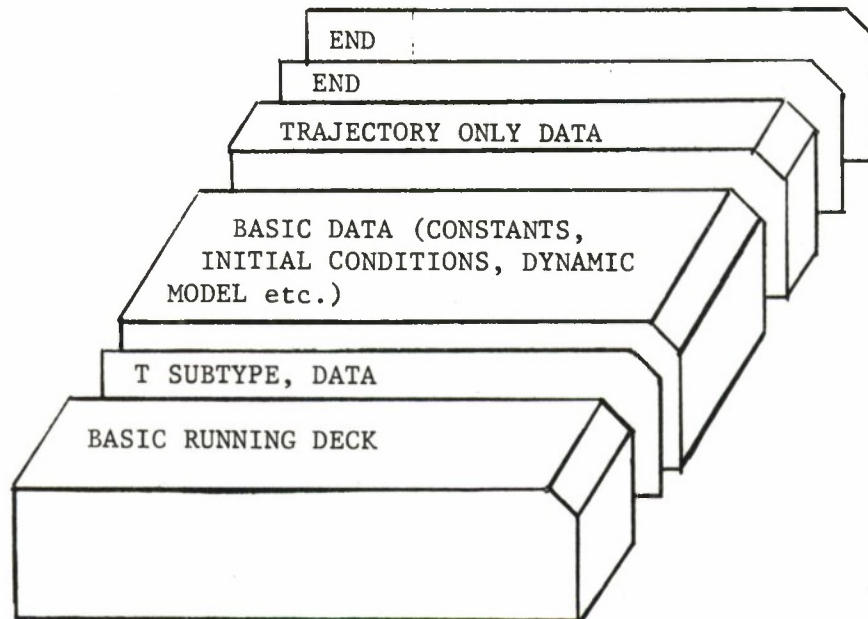


Figure 5.

TRAJECTORY PREDICTION DECK ARRANGEMENT

When several trajectory predictions are to be done in one run (function code ITIN = 333, etc.) then the deck arrangement is merely an extension of that for the single case (Figure 6).

3.6.2 Observation Generation Deck Arrangement

Figure 7 and Figure 8 show the correct data setup for a single data generation run (function code ITIN = 4) and several cases (function code ITIN = 4.4, etc.) respectively.

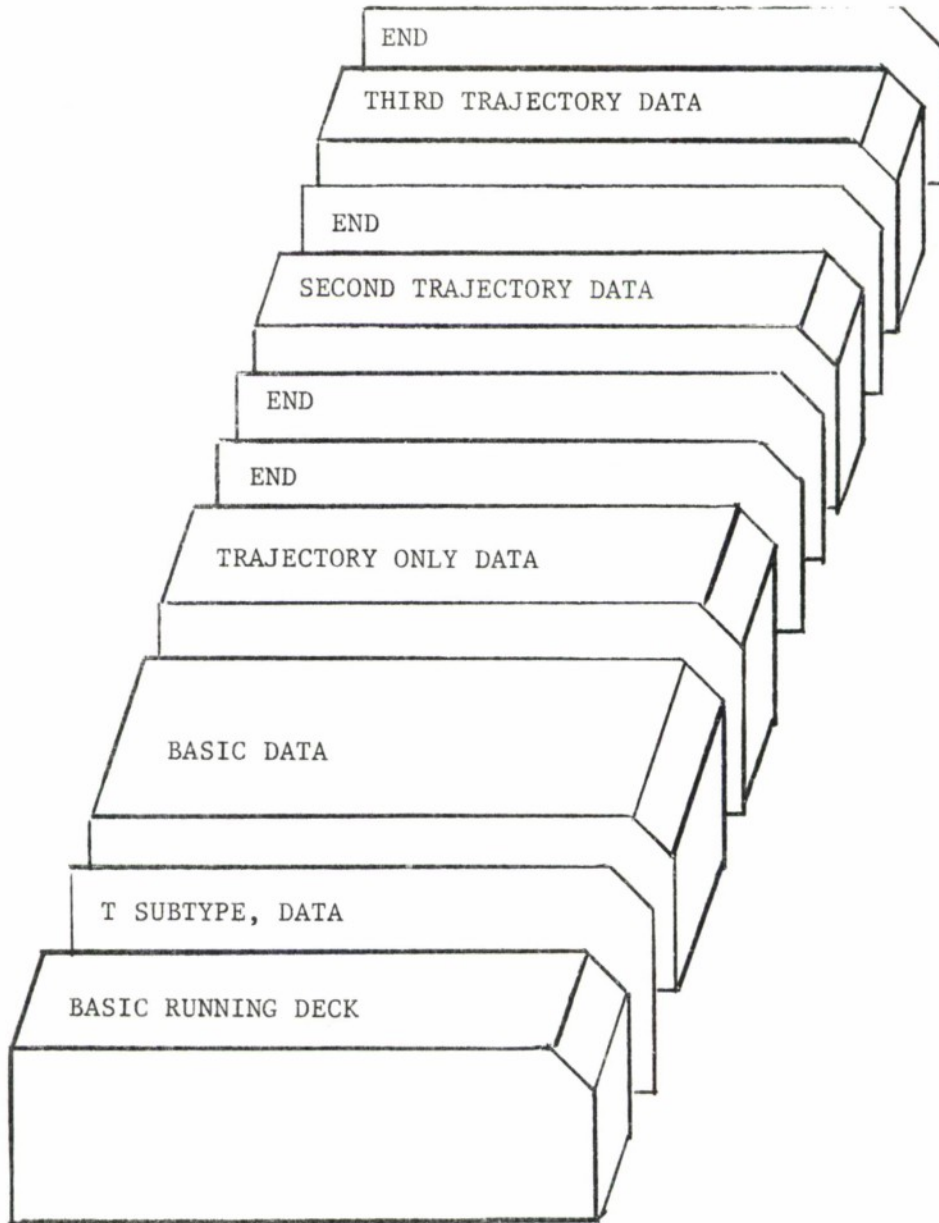


Figure 6.

MULTIPLE TRAJECTORY PREDICTIONS DECK ARRANGEMENT

Figure 7.

DECK ARRANGEMENT FOR
OBSERVATION GENERATION
SINGLE CASE.

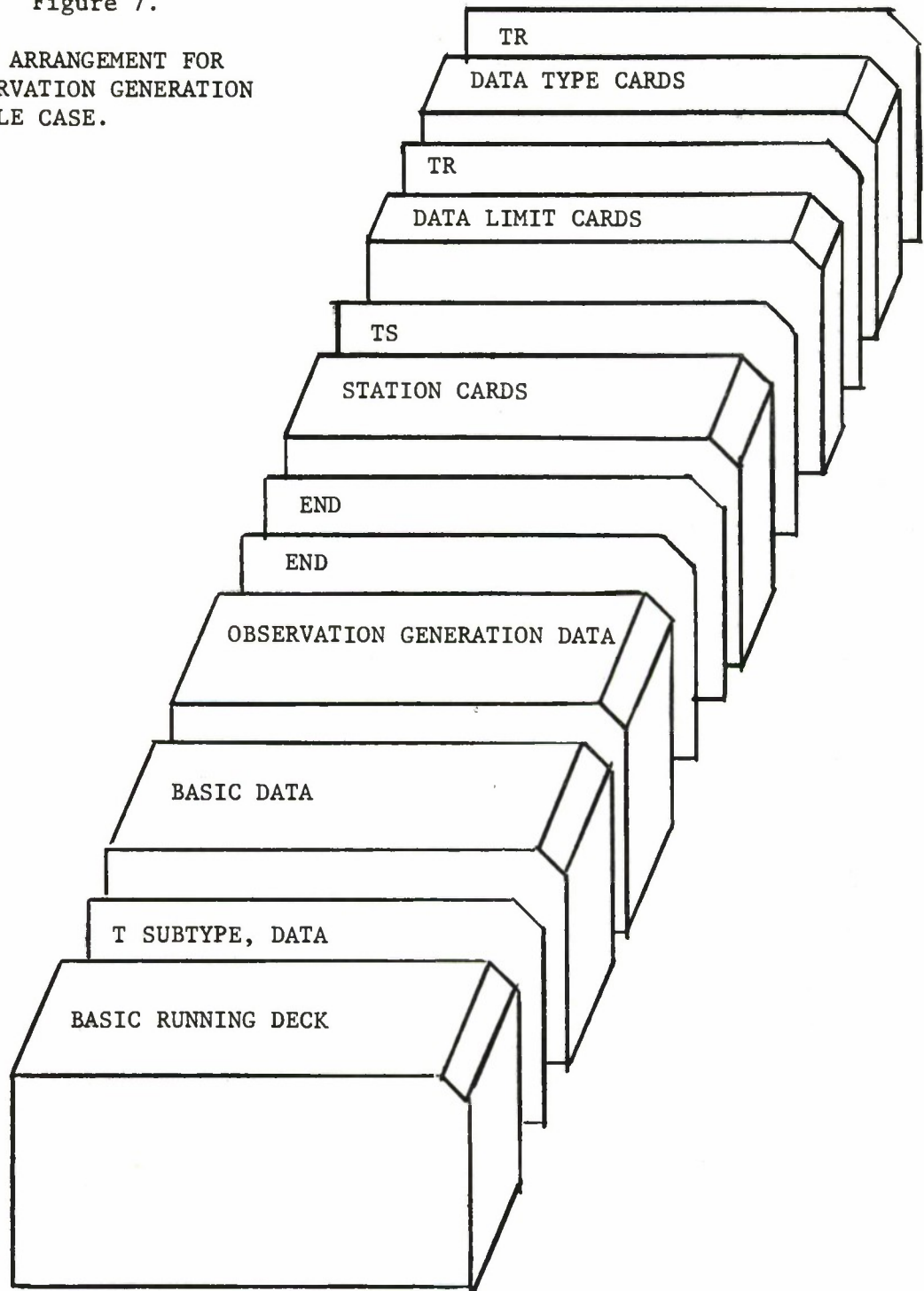
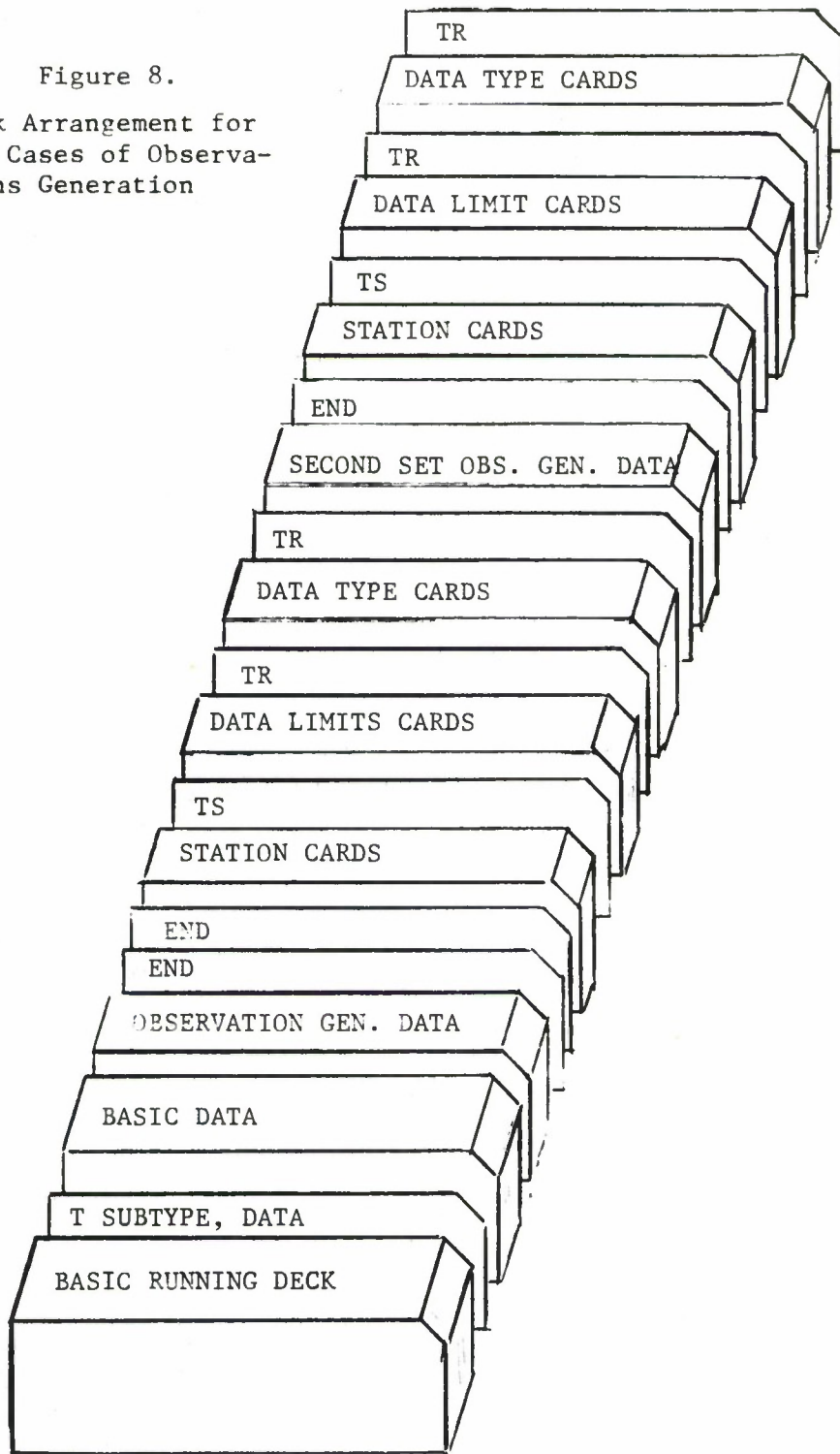


Figure 8.
Deck Arrangement for
Two Cases of Observa-
tions Generation



3.6.3 Orbit Determination Deck Arrangement

There are several different deck setups that are permissible for an orbit determination run (function code ITIN = 12) according to the choice of several suboptions.

Figure 9 is the simplest deck setup and applies when the observation data is being input on tape (i.e., IBCDI input variable is used).

Figure 10 is the ordinary deck setup for a single case when the observation data is attached to the deck. Figure 11 is the deck setup for two such stacked cases.

Figure 12 is the appropriate data arrangement for the situation of multiple satellites (in this case three satellites).

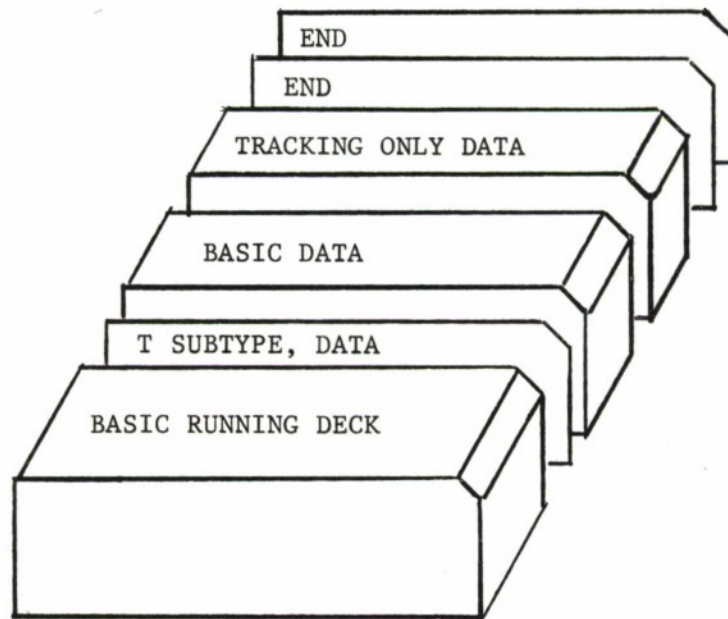


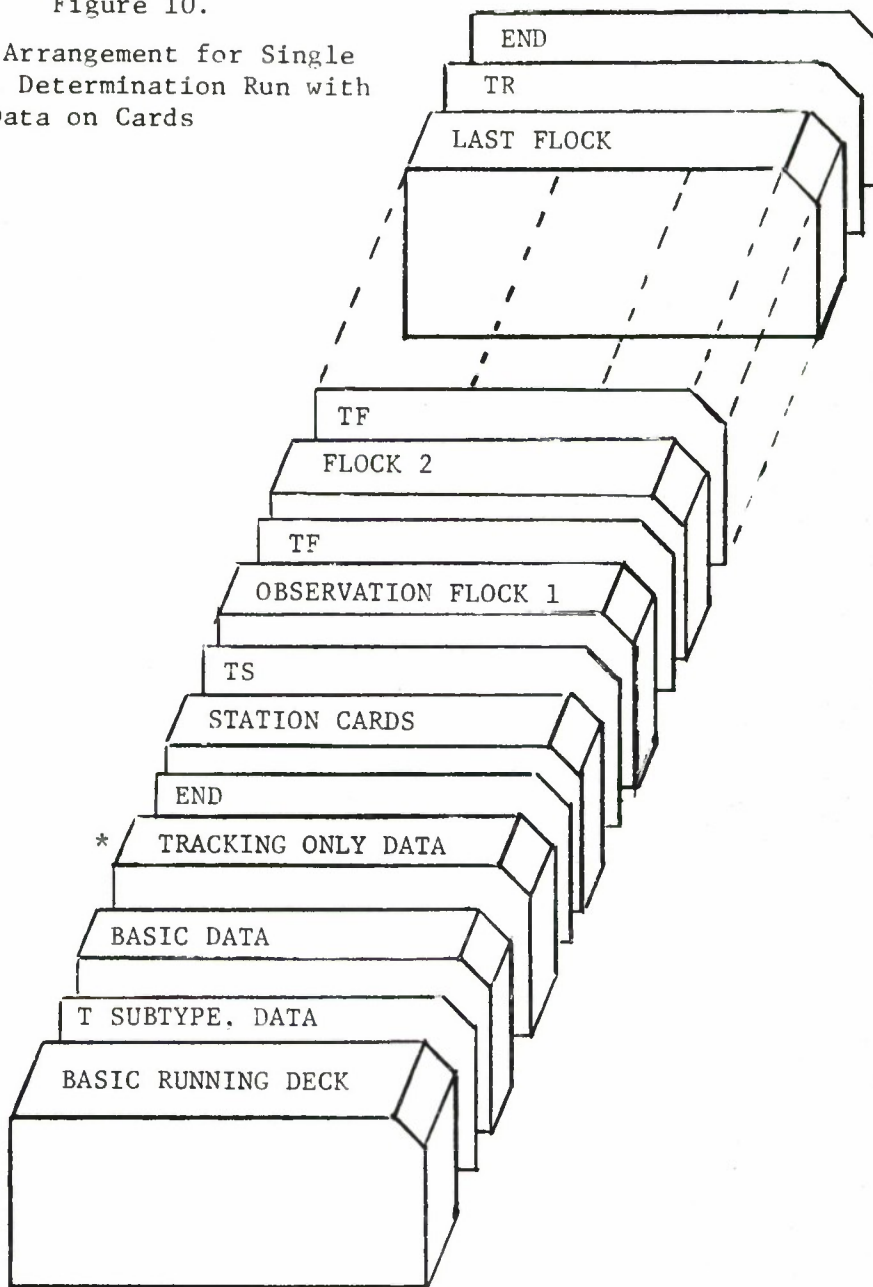
Figure 9.

Deck Arrangement for Orbit Determination with Input Tape*

- * Note that the BCD tape of observations must contain as its first set of cards the station cards followed by a TS card and then the observations in proper flocks followed by TF cards with a TR card replacing the TF card of the last flock.

Figure 10.

Deck Arrangement for Single
Orbit Determination Run with
All Data on Cards



* Note that the word "tracking" is used interchangeably with the words "Orbit Determination".

Figure 11.
 Deck Arrangement for
 Two Orbit Determination
 Cases All Data on
 Cards

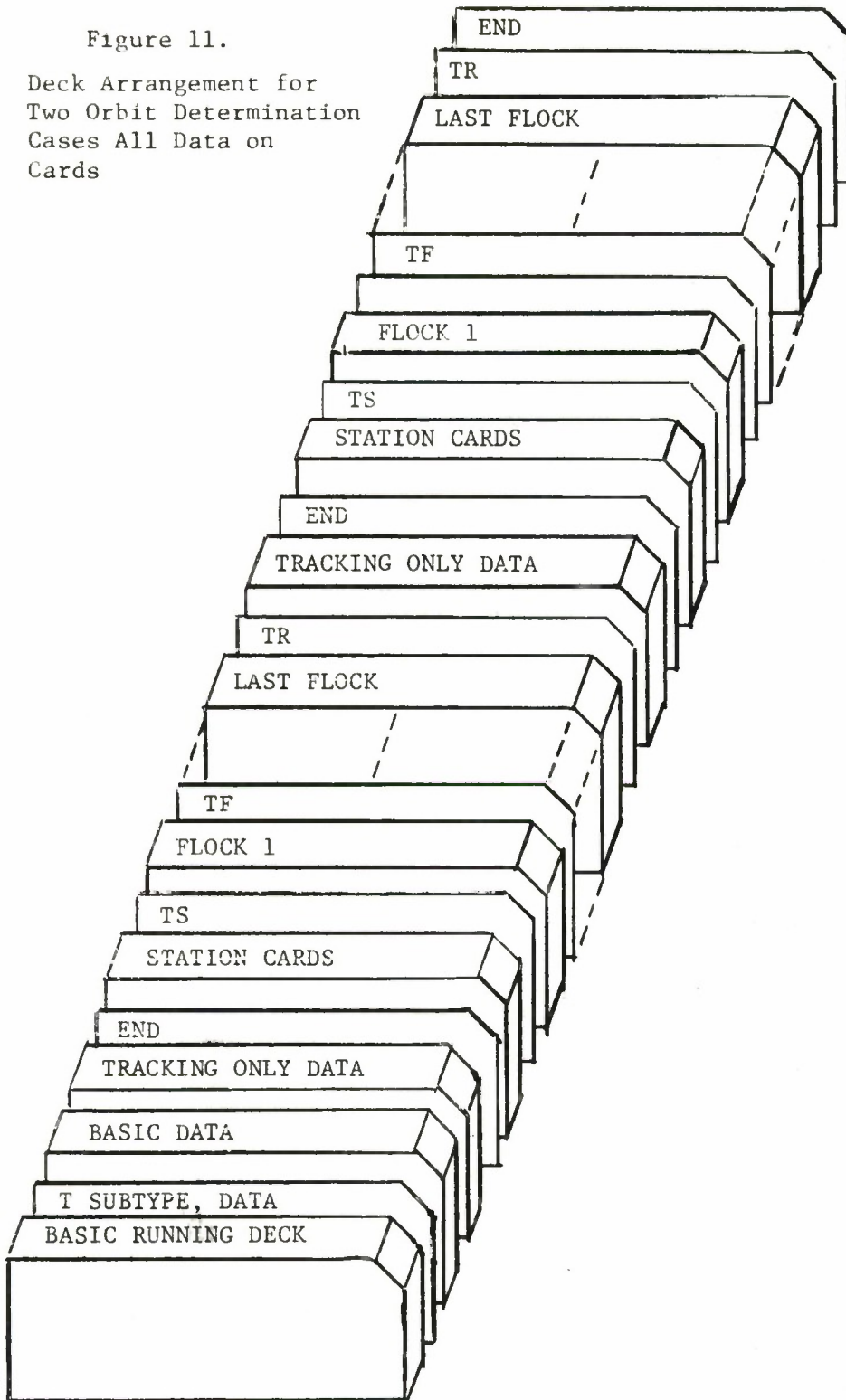
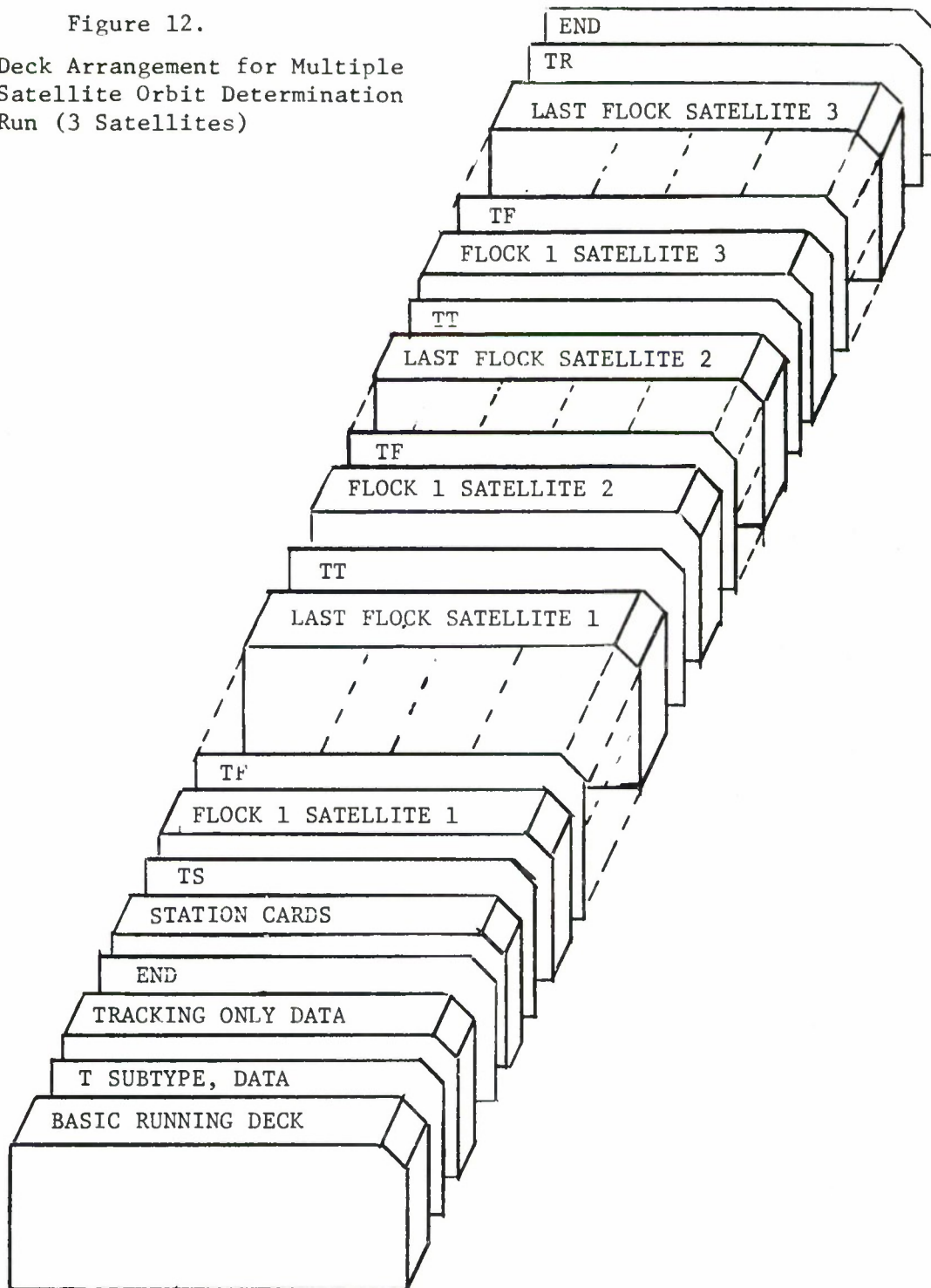


Figure 12.
 Deck Arrangement for Multiple
 Satellite Orbit Determination
 Run (3 Satellites)



3.6.4 Sample Input Decks

Figures 13, 14, and 15 are listings of sample data decks for trajectory prediction, observation generation, and orbit determination. Besides giving the user an idea of what a typical deck looks like, they may also be used to familiarize the user with the operation of TRACE-D before he creates his own input. Another reason for running a test case of this sort is to determine the status of the program tape, for it is possible for the contents of a tape to deteriorate and no longer be useful¹.

It is not to be assumed that these sample cases exercise all the possible options of TRACE-D, but rather that they exhibit typical input and output. A complete description of the output obtained from these runs is included in Section 4.

¹ In this instance, there is no cause for alarm. MITRE has the capability to create a new and correct program tape in 24 hours.

Figure 14

T	SURTYPE	DATA	GINTEG	TRACE-D	STANDARD	INTEGRATION	CONSTANTS
			11	12	2	13	0
4	1		5	1	11	1.00002516	
23	.1		-9	26	1		
31	.015625		32	64	33		
134	4		135	1	37	.001	
38	0.		40	2820.1763	141	1	
GC							
1	.437526904	-2	2	.5530370	-2	6	.5
6	.5		8	.43752695	-2		
9	1.		10	10			
13	3280.8399		14	57.2957795	15	20925738	
16	332951.3		17	.0122999	18	.814979	
19	.107821		20	317.887	21	25.129	
22	23454.865		23	3443.9336	24	20925738	
25	348762.3		26	32.174	30	348762.3	
31	1.5		32	1.0471976	33	3.14159265	
34	298.3		35	300000.	36	82505.922	
ITMATX4							
DRAG	.01		12	1	3	6.83	
4	-15.684						
RREFC1.							
GC	STANDARD DECK FOR GUIERS	6. TH ORDER	EARTH MODEL				10/15/65
1	.043752695	-1	2	.55304505	-2	15	20925741.
24	20925741.		OBJT		2	1.723	-6
3	1.856	-6	4	.4482	-6	5	.1643
6	.7278	-6	7	.1536	-6	8	.05719
9	.004781	-6	10	.1509	-6	11	.05329
12	.005842	-6	13	.004093	-6	14	.0009462
15	.06611	-6	16	.03746	-6	17	.01166
18	.002256	-6	19	.0003328	-6	20	.00005153
OBLT			2	-13.18	3	5.31	
4	-13.33		5	16.00	6	-136.68	
7	27.47		8	-1.10	9	36.01	
10	-81.86		11	-2.60	12	-3.45	
13	58.25		14	-15.32	15	157.21	
16	113.15		17	-1.75	18	60.74	
19	-17.75		20	-14.34	05JZ		
2	1082.76	-6	3	-2.693	-6	4	-1.56
5	-.006	-6	6	.39	-6	7	-.633
8	0.		9	.210	-6	10	9
12	6		13	9	14	6	
DITIN	4		YEAR	1965	MONTH	2	

Figure 14 (cont.)

IDAY 23
 IIC1YP4
 IC -60.

2 0. 3 90.
 4 25.
 5 -607612. 6 -1.

IPTAPE4

BNOISE1 IISIG 1 12 2

13 3 14 4 15 5

16 6 17 7 18 8

19 13 110 14 111 15

112 19 SIGMA100. 2 .1

3 .1 4 .05 5 .05 6 .05

7 .05 8 .05 9 1000.

10 1000. 11 1000. 12 .1

END

MRAPAR05.99

DOI.01BB RBIAS 03.011000.

END

AA 75.0 300.0 1000.

BB 45.0 240. 100.

CC 0. 315.0 500.

DD 0. 15.0 200.0

EE -15.0 135.0 100.

FF -65.0 75.0 5000.0

TS

AA 15. 70 24

BB 15. 70 24

CC 15. 70 24

DD 15. 70 24

EE 15. 70 24

FF 15. 70 24

TR

AA XXXX X XXXXX

BB XXXX XXXXX

CC XXXX X XXXXX

DD XXXX XXXXX

EE XXXX XX XXXXX

FF XXXX XXXXX

TR

Figure 15

SUBTYPE DATA		INTEGRATION CONSTANTS										
GINTEG	TRACE-D	STANDARD	INTEGRATION	CONSTANTS	10/	1/65	10/	1/65	10/	1/65	10/	1/65
11	1	12	2	15	0							
4	1	5	1	11	1.00002516							
23	.1											
26	1											
30	1	31	.015625	32	64	33	1					-7
134	4	135	1	37	.0001	38	0.					
40	2820.16012	141	1									
GC		TRACE-D STANDARD PHYSICAL CONSTANTS										
1	.437526904	-2	2	.55304203	-2	6	.5					
8	.437526904	-2	9	1.		10	10					
13	3280.8399	14	57.2957795	15	20925738							
16	332951.3	17	.01229853	18	.814979							
19	.107621	20	317.887	21	95.129							
22	23454.865	23	3443.93355	24	20925738							
25	348762.3	26	32.174	30	348762.3							
31	1.5	32	1.0471976	33	3.14159265							
34	298.3	35	300000.	35	82505.922							
NUMB		42	3443.9336									
DITIN 12												
DPRCDE X X												
IICTYP2												
IC	23.11454											
2	26.51516											
3	89.88977											
4	45.73312											
5	24780836.7											
6	23765.259											
IMAXIT1												
IYEAR 1967												
IMNTH 7												
IDAY 8												
TZNE 0												
HR	14.											
MIN	45.											
DRAG	.2849	12	1									
3	6.83	4	-15.684									
110B	10	12	6	13	10							
14	6											
OBJZ												
2	.1082645	-2										
3	-.2546000	-5										
4	-1.649	-6										

Figure 15 (cont.)

5	-.210	-6 6	.646	-6 7	-.333	-6
8	-.270	-6 9	-.053	-6 10	-.054	-6
OBJT		2	1.5664	-6 3	1.7287	-6
4	.3025	-6 5	.1966	-6 6	.5234	-6
7	.1372	-6 8	.04166	-6 9	.009376	-6
10	.1247	-6 11	.05846	-6 12	.02219	-6
13	.001605	-6 14	.001029	-6 15	.09572	-6
16	.02928	-6 17	.001037	-6 18	.001500	-6
19	.000381	-6 20	.000140	-6		
OBLT		2	-15.50	3	-1.43	
4	-32.30	5	32.31	6	-133.53	
7	35.75	8	-2.75	9	26.09	
10	-164.13	11	-24.19	12	58.58	
13	32.27	14	-15.79	15	99.46	
16	-38.87	17	0.0	18	-19.96	
19	-25.28	20	-16.92			
SIGMA	22.96					
2	.06056					
3	22.96					
4	.06056					
5	22.96					
6	.06056					
IPTAPE	4					
IISIG	101					
12	119					
13	201					
14	219					
15	301					
16	319					
DCPRAM	2XXXXXX					
DDPRAM	XXXXXX					
BND	1.5					
2	1.5					
3	.3					
4	.75					
5	4920.					
6	492.					
7	.15					
8	.1	-7				
9	.1	-7				
10	.1	-7				
END						
MF	1	42.617373	289.50953	223.0970		
BD	2	42.505961	289.76481	-91.8640		

Figure 15 (cont.)

BH	3	42.645973	285.90644	+154.199
TS				
MH	7	8145316.	7706017	-17007.799540638
MH	7	8145321.	2185237	-16953.515419959
MH	7	8145325.	5664477	-16893.817585227
MH	7	8145329.	9603707	-16841.864501236
MH	7	8145334.	4422917	-16781.986876605
MH	7	8145338.	7262187	-16723.026246665
MH	7	8145342.	5561527	-16668.616601036
MH	7	8145343.	5394681	8494671.751891473
MH	7	8145346.	4340867	-16612.446522233
MH	7	8145350.	2880207	-16554.9625998321
MH	7	8145354.	0479567	-16497.401902913
MH	7	8145357.	9418897	-16436.200131176
MH	7	8145358.	5792151	8245884.580015854
MH	7	81454	1.7558247	-16374.666010437
MH	7	81454	5.5157637	-16312.415026127
MH	7	81454	9.2756987	-16248.541010438
MH	7	8145410.	9870091	8043320.997374223
MH	7	8145413.	0356387	-16183.004265009
MH	7	8145416.	7955787	-16115.793963192
MH	7	8145420.	5955147	-16046.087926446
MH	7	8145422.	4548211	7858498.293914379
MH	7	8145424.	3554517	-15975.296587883
MH	7	8145428.	1153907	-15902.686679719
MH	7	8145431.	8753317	-15828.202099680
MH	7	8145434.	1106331	7673186.286040589
MH	7	8145435.	6352727	-15751.774506226
MH	7	8145439.	3952127	-15673.353674529
MH	7	8145443.	1551527	-15592.931758462
MH	7	8145445.	5784501	7493579.593139116
MH	7	8145446.	9150947	-15510.397637783
MH	7	8145450.	6750367	-15425.733267663
MH	7	8145454.	4349781	-15338.886154829
MH	7	8145456.	8582741	7319714.402892145
MH	7	8145458.	1949217	-15250.050524889
MH	7	81455	1.9548637	-15158.382217763
MH	7	81455	5.7148057	-15064.618438243
MH	7	81455	8.1381001	7148905.314970903
MH	7	81455	9.4747457	-14968.425524830
MH	7	8145513.	2346877	-14869.749999939
MH	7	8145516.	9946297	-14768.547572134
MH	7	8145519.	4179301	6981341.469786883
MH	7	8145520.	7545717	-14664.727034000

Figure 15 (cont.)

MH	7	8145524	5145167	-14558	236876605
MH	7	8145528	2744597	-14449	018372655
MH	7	8145530	8857601	6814605	019683455
MH	7	8145532	0344047	-14336	992453991
MH	7	8145535	7943507	-14222	113188861
MH	7	8145539	5542967	-14104	283136425
MH	7	8145542	3535951	6651813	746672701
MH	7	8145543	3142427	-13983	450459300
MH	7	8145547	0741897	-13859	567585288
MH	7	8145550	8341377	-13732	5337922613
MH	7	8145553	6334361	6495847	080016261
MH	7	8145554	5940857	-13602	290026126
MH	7	8145558	3540367	-13468	763779519
MH	7	81456	21139867	-13331	885498642
MH	7	81456	49132821	6344314	041960785
MH	7	81456	58739347	-13191	593175827
MH	7	81456	96338827	-13047	799540638
MH	7	8145613	3938307	-12900	444881855
MH	7	8145616	1931331	6197545	177123089
MH	7	8145617	1537817	-12749	447178482
MH	7	8145620	9137307	-12594	758858202
MH	7	8145624	6736827	-12436	287401556
MH	7	8145627	4729891	6055927	460570700
MH	7	8145628	4336357	-12273	993438301
MH	7	8145631	8175937	-12124	569553790
MH	7	8145656	8006431	5714590	387114810
MH	7	8145657	4792947	-10883	785433053
BH	7	8145657	4792947	-11177	128936945
MH	7	81457	12392527	-10685	356955347
BH	7	81457	12392527	-10965	440616785
MH	7	81457	49992117	-10482	535761116
BH	7	81457	49992117	-10789	370406805
MH	7	81457	87591717	-10275	271653532
BD	7	81457	87591717	-10406	458661375
BH	7	81457	87591717	-10588	925853012
MH	7	8145711	0884891	5564041	174498868
MH	7	8145712	5191337	-10063	540682374
BH	7	8145712	5191337	-10384	057414709
MH	7	8145716	2790977	-9847	312335968
BD	7	8145716	2790977	-9987	448490798
BH	7	8145716	2790977	-10174	793635128
MH	7	8145720	0390627	-9626	570538043
BD	7	8145720	0390627	-9771	381561637
BH	7	8145720	0390627	-9961	031495988

Figure 15 (cont.)

MH	7	8145722.	3683761	5453289.	173186419
MH	7	8145723.	7990317	-9401.	292979001
BD	7	8145723.	7990317	-9550.	736220479
BH	7	8145723.	7990317	-9742.	778215229
MH	7	8145727.	0889977	-9200.	437007844
BD	7	8145727.	0889977	-9354.	033136427
BH	7	8145727.	0889977	-9548.	052165329
MH	7	8145731.	3189557	-8937.	069553792
BD	7	8145731.	3189557	-9096.	087598383
BH	7	8145731.	3189557	-9292.	640748024
MH	7	8145733.	6482721	5350155.	314940820
MH	7	8145735.	0789207	-8698.	130249321
BD	7	8145735.	0789207	-8861.	911417305
BH	7	8145735.	0789207	-9060.	719816267
MH	7	8145738.	9388877	-8454.	659120738
BD	7	8145738.	9388877	-8623.	455380558
BH	7	8145738.	9388877	-8824.	287401556
MH	7	8145742.	5988557	-8206.	674540639
BD	7	8145742.	5988557	-8390.	480971097
BH	7	8145742.	5988557	-8583.	324803113
MH	7	8145744.	9281751	5255145.	669280096
MH	7	8145746.	3588267	-7954.	190944850
BD	7	8145746.	3588267	-8132.	829068213
BH	7	8145746.	3588267	-8337.	750656127
MH	7	8145749.	4608047	-7742.	543635130
BH	7	8145749.	4608047	-8131.	808398932
MH	7	8145753.	8787677	-7435.	911417305
BH	7	8145753.	8787677	-7833.	289698153
MH	7	8145756.	2080871	5168704.	527526415
MH	7	8145757.	6387377	-7170.	207020938
BH	7	8145757.	6387377	-7574.	386154860
MH	7	81458	1.3987087	-6900.	222440958
BH	7	81458	1.3987087	-7311.	076443552
MH	7	81458	5.1586817	-6626.	022637784
BH	7	81458	5.1586817	-7043.	491797864
MH	7	81458	7.4880091	5091246.	948790910
MH	7	81458	8.9186567	-6347.	699803144
BD	7	81458	8.9186567	-6556.	983267694
BH	7	81458	8.9186567	-6771.	640091836
MH	7	8145812.	5446367	-6075.	487532765
BD	7	8145812.	5446367	-6289.	579724401
BH	7	8145812.	5446367	-6505.	478674530
MH	7	8145816.	4386167	-5779.	078412056
BH	7	8145816.	4386167	-6215.	483267694

Figure 15 (cont.)

MH	7	8145818	7679401	5023233	398925128
MH	7	8145821	2865907	-5404	372703403
BD	7	8145821	2865907	-5630	134186327
BH	7	8145821	2865907	-5848	448818892
MH	7	8145823	9585737	-5195	242782116
BD	7	8145823	9585737	-5424	551837265
BH	7	8145823	9585737	-5643	421587914
MH	7	8145827	7185517	-4897	978674531
BD	7	8145827	7185517	-5132	214238822
BH	7	8145827	7185517	-5351	723425179
MH	7	8145830	0478801	4965042	486846300
BD	7	8145830	0478801	5012599	803130797
BH	7	8145830	0478801	4995518	011779438
MH	7	8145831	4785337	-4597	302821517
BD	7	8145831	4785337	-4836	414370060
BH	7	8145831	4785337	-5056	453412056
MH	7	8145835	2385177	-4293	425853014
BD	7	8145835	2385177	-4537	234251946
BH	7	8145835	2385177	-4757	695209950
MH	7	8145838	9985057	-3986	493438288
TF					
BD	7	8145838	9985057	-4234	887795269
BH	7	8145838	9985057	-4455	634842515
MH	7	8145841	3278321	4917039	402862144
BD	7	8145841	3278321	4961818	208648054
BH	7	8145841	3278321	4942276	738799478
MH	7	8145842	7584917	-3676	690288708
BD	7	8145842	7584917	-3929	666666657
BH	7	8145842	7584917	-4150	414041996
MH	7	8145846	5184747	-3364	213910743
BD	7	8145846	5184747	-3621	639435679
BH	7	8145846	5184747	-3842	224081352
MH	7	8145850	2784607	-3049	265091851
BD	7	8145850	2784607	-3310	935695529
BH	7	8145850	2784607	-3531	279527545
MH	7	8145854	0384497	-2732	049868762
BD	7	8145854	0384497	-2997	869094476
BH	7	8145854	0384497	-3217	771653533
MH	7	8145854	2997901	4874828	936980719
BD	7	8145854	2997901	4916232	545807969
BH	7	8145854	2997901	4893819	619384345
MH	7	8145857	7984417	-2412	770997360
BD	7	8145857	7984417	-2682	662401557
BH	7	8145857	7984417	-2901	898622036

Figure 15 (cont.)

MH	7 81459	1.5584367	-2091.681430444
BD	7 81459	1.5584367	-2365.384842515
BH	7 81459	1.5584367	-2583.833661422
MH	7 81459	5.7884277	-1728.552493438
BD	7 81459	5.7884277	-2006.360564291
BH	7 81459	5.7884277	-2223.667322829
MH	7 81459	8.3997591	4845091.108886094
BD	7 81459	8.3997591	4882650.951415570
BH	7 81459	8.3997591	4857161.154845925
MH	7 81459	9.5484177	-1404.350393690
BD	7 81459	9.5484177	-1685.668963253
BH	7 81459	9.5484177	-1901.723097108
MH	7 81459	13.3084117	-1079.074803144
BD	7 81459	13.3084117	-1363.636154853
BH	7 81459	13.3084117	-1578.378280841
MH	7 81459	17.0684087	-752.939304460
BD	7 81459	17.0684087	-1040.523950130
BH	7 81459	17.0684087	-1253.791994750
MH	7 81459	20.8284087	-426.215879263
BD	7 81459	20.8284087	-716.666994750
BH	7 81459	20.8284087	-928.166338582
MH	7 81459	21.9357471	4832679.461913471
BD	7 81459	21.9357471	4866340.157470290
BH	7 81459	21.9357471	4837948.622008667
MH	7 81459	24.5884107	-99.171587926
BD	7 81459	24.5884107	-392.191272965
BH	7 81459	24.5884107	-601.836286090
MH	7 81459	28.3784097	230.581036744
BD	7 81459	28.3784097	-64.978018373
BH	7 81459	28.3784097	-272.511482939
MH	7 81459	32.1384077	557.538713906
BD	7 81459	32.1384077	259.744094485
BH	7 81459	32.1384077	54.458989501
MH	7 81459	34.7197491	4835563.877929160
BD	7 81459	34.7197491	4865462.664031525
BH	7 81459	34.7197491	4834413.188934121
MH	7 81459	35.8984087	884.088254586
BD	7 81459	35.8984087	584.356955375
BH	7 81459	35.8984087	381.427165352
MH	7 81459	39.6584137	1209.959317572
BD	7 81459	39.6584137	909.599081360
BH	7 81459	39.6584137	708.104658786
MH	7 81459	43.8584217	1572.849081352
BD	7 81459	43.8584217	1269.870734920

Figure 15 (cont.)

BH	7	8145943.8584217	1072.327099726
MH	7	8145946.1877641	4850222.375304724
BD	7	8145946.1877641	4876679.429107042
BH	7	8145946.1877641	4843354.790006049
MH	7	8145948.0484327	1933.403871380
BD	7	8145948.0484327	1629.105314948
BH	7	8145948.0484327	1434.749999992
MH	7	8145951.8084357	2255.420275569
BD	7	8145951.8084357	1950.168963231
BH	7	8145951.8084357	1758.819225714
MH	7	8145955.5684427	2575.734251946
BD	7	8145955.5684427	2269.760498673
BH	7	8145955.5684427	2081.488845125
MH	7	8145957.6557901	4876194.192870570
BD	7	8145957.6557901	4899150.426482634
BH	7	8145957.6557901	4863629.035399981
MH	7	8145959.3284527	2894.118110210
BD	7	8145959.3284527	2587.678149581
BH	7	8145959.3284527	2402.614829376
MH	7	815 0 3.0884657	3210.351706013
BD	7	815 0 3.0884657	2903.638123333
BH	7	815 0 3.0884657	2721.910761133
MH	7	815 0 6.8484807	3524.234580040
BD	7	815 0 6.8484807	3217.569553778
BH	7	815 0 6.8484807	3039.201443538
MH	7	815 0 8.9358271	4912595.636443626
BD	7	815 0 8.9358271	4932098.687652342
BH	7	815 0 8.9358271	4894511.450103209
MH	7	815 010.6084957	3835.544947475
BD	7	815 010.6084957	3529.190288693
BH	7	815 010.6084957	3354.2922650893
MH	7	815 014.3685077	4144.094160080
BD	7	815 014.3685077	3838.201443538
BH	7	815 014.3685077	3666.901902854
MH	7	815 018.1285227	4449.713910728
BD	7	815 018.1285227	4144.511154830
BH	7	815 018.1285227	3976.858923867
MH	7	815 020.2158751	4959522.047210072
SD	7	815 020.2158751	4975564.665343767
BH	7	815 020.2158751	4936068.044585795
MH	7	815 021.8885397	4752.191272944
BD	7	815 021.8885397	4447.928805738
BH	7	815 021.8885397	4283.965551138
MH	7	815 025.6485587	5051.377624631

Figure 15 (cont.)

BD	7	815	025.6485587	4748.261154800
BH	7	815	025.6485587	4588.059383154
MH	7	815	029.4085807	5347.116797834
BD	7	815	029.4085807	5045.252952695
BH	7	815	029.4085807	4888.933398932
MH	7	815	031.8719351	5018746.915984593
BD	7	815	031.8719351	5031255.183715188
BH	7	815	031.8719351	4989900.393676407
MH	7	815	033.1686047	5639.257545888
BD	7	815	033.1686047	5338.932086557
BH	7	815	033.1686047	5186.435039341
MH	7	815	036.9986227	5933.008530140
BD	7	815	036.9986227	5634.471128583
BH	7	815	036.9986227	5485.930118054
MH	7	815	040.7586437	6217.502296537
BD	7	815	040.7586437	5920.948162675
BH	7	815	040.7586437	5776.171915978
MH	7	815	043.9040091	5090921.423858105
BD	7	815	043.9040091	5099845.669249987
BH	7	815	043.9040091	5056728.182372580
MH	7	815	044.9586707	6530.578740120
BD	7	815	044.9586707	6236.347112805
BH	7	815	044.9586707	6095.967191547
MH	7	815	048.7186957	6806.551181048
BD	7	815	048.7186957	6514.459645599
BH	7	815	048.7186957	6378.108267665
MH	7	815	052.4787237	7078.336942196
BD	7	815	052.4787237	6788.751968443
BH	7	815	052.4787237	6656.162401527
MH	7	815	055.5600901	5171103.772948697
BD	7	815	055.5600901	5176625.852996039
BH	7	815	055.5600901	5131899.540648845
MH	7	815	056.2387537	7345.880905449
BD	7	815	056.2387537	7058.797900200
BH	7	815	056.2387537	6930.158792585
MH	7	815	059.9987877	7609.067926447
BD	7	815	059.9987877	7324.712926447
BH	7	815	059.9987877	7199.950459271
MH	7	815	13.7588157	7867.925196796
TF				
BD	7	815	13.7588157	7586.324146956
BH	7	815	13.7588157	7465.447178393
MH	7	815	16.8401781	5257859.514403833
BD	7	815	16.8401781	5260174.606292054

Figure 15 (cont.)

BH	7 815 1	6.8401781	5214070.603636997
MH	7 815 1	7.5188437	8122.322834610
BD	7 815 1	7.5188437	7843.663057655
BH	7 815 1	7.5188437	7726.558726966
MH	7 815 111	2.788747	8372.245078623
BD	7 815 111	2.788747	8096.620406776
BH	7 815 111	2.788747	7983.298556387
MH	7 815 115	0.689077	8619.612860798
BD	7 815 115	0.689077	8346.987860857
BH	7 815 115	0.689077	8237.502952694
MH	7 815 118	8.289417	8860.457349002
BD	7 815 118	8.289417	8591.197178423
BH	7 815 118	8.289417	8485.350393593
MH	7 815 119	6.242891	5366496.719115616
BD	7 815 119	6.242891	5365318.110198558
BH	7 815 119	6.242891	5317782.283416079
MH	7 815 122	6.129777	9098.269356846
BD	7 815 122	6.129777	8832.220800399
BH	7 815 122	6.129777	8730.143700718
MH	7 815 126	3.730157	9330.004921137
BD	7 815 126	3.730157	9067.309711218
BH	7 815 126	3.730157	8968.818569481
MH	7 815 130	1.730557	9559.574474990
BD	7 815 130	1.730557	9300.414370000
BH	7 815 130	1.730557	9205.468503892
MH	7 815 133	5.364211	5496434.055083341
BD	7 815 133	5.364211	5491595.702086584
BH	7 815 133	5.364211	5442693.471099318
MH	7 815 133	9.330907	9782.182086526
BD	7 815 133	9.330907	9526.528215170
BH	7 815 133	9.330907	9435.012467145
MH	7 815 137	7.871267	10005.643044530
BD	7 815 137	7.871267	9753.615157365
BH	7 815 137	7.871267	9665.611876547
MH	7 815 141	5.471637	10219.110236107
BD	7 815 141	5.471637	9970.648293912
BH	7 815 141	5.471637	9885.977690219
MH	7 815 145	3.072027	10428.093175767
BD	7 815 145	3.072027	10183.123359500
BH	7 815 145	3.072027	10101.816241356
MH	7 815 146	3.205521	5625686.089202367
BD	7 815 146	3.205521	5617857.086577942
BH	7 815 146	3.205521	5567863.188934012
MH	7 815 149	0.672427	10632.640091775

Figure 15 (cont.)

BD	7	815	149.0672427	10391.355642973
BH	7	815	149.0672427	10313.204068123
MH	7	815	152.8272847	10832.774278102
BD	7	815	152.8272847	10595.088582574
RH	7	815	152.8272847	10520.081364749
MH	7	815	156.6173287	1130.091535328
BD	7	815	156.6173287	10796.124671815
BH	7	815	156.6173287	10724.212926446
MH	7	815	157.9861881	5751823.622008629
BD	7	815	157.9861881	5741009.711272369
RH	7	815	157.9861881	5690133.136443336
MH	7	815	157.9861881	11221.512467085
BD	7	815	157.9861881	10991.209973632
BH	7	815	157.9861881	10922.284776805
MH	7	815	157.9861881	11411.817585169
BD	7	815	157.9861881	11185.169291256
BH	7	815	157.9861881	11119.246062933
MH	7	815	157.9861881	11614.185367344
BD	7	815	157.9861881	11391.668635069
BH	7	815	157.9861881	11328.860236108
MH	7	815	157.9861881	5886674.212554225
BD	7	815	157.9861881	5873193.569518377
BH	7	815	157.9861881	5821524.179747825
MH	7	815	157.9861881	11792.444881795
BD	7	815	157.9861881	11573.566272854
BH	7	815	157.9861881	11513.571522175
MH	7	815	157.9861881	11966.633202015
BD	7	815	157.9861881	11751.365157424
RH	7	815	157.9861881	11694.017060278
MH	7	815	157.9861881	12153.583661316
BD	7	815	157.9861881	11942.331364750
BH	7	815	157.9861881	11887.836286607
MH	7	815	157.9861881	6023854.396300691
BD	7	815	157.9861881	6007901.541960904
BH	7	815	157.9861881	5955575.688933976
MH	7	815	157.9861881	12319.373031436
BD	7	815	157.9861881	12111.740485488
BH	7	815	157.9861881	12059.779855547
MH	7	815	157.9861881	12481.275262413
BD	7	815	157.9861881	12277.156167922
RH	7	815	157.9861881	12227.710957942
MH	7	815	157.9861881	6297622.965850138
BD	7	815	157.9861881	6277370.177123344
BH	7	815	157.9861881	6224033.038024572

Figure 15 (cont.)

MH	7	815	252.	1960267	13451.	150590418
BD	7	815	252.	1960267	13269.	581036685
MH	7	815	255.	2440667	13560.	611876545
BD	7	815	255.	2440667	13381.	692585168
BH	7	815	255.	2440667	13348.	261482833
MH	7	815	259.	0041177	13692.	635170518
BD	7	815	259.	0041177	13517.	040682314
BH	7	815	259.	0041177	13485.	424868642
MH	7	815	3	2.7641687	13821.	411089180
BD	7	815	3	2.7641687	13648.	956364690
BH	7	815	3	2.7641687	13619.	210629819
MH	7	815	3	4.5295311	6589499.	901518962
BD	7	815	3	4.5295311	6565339.	074767280
BH	7	815	3	4.5295311	6511265.	748015802
MH	7	815	3	6.5242217	13947.	020669220
BD	7	815	3	6.5242217	13777.	706692813
BH	7	815	3	6.5242217	13749.	744422494
MH	7	815	310.	2842737	14069.	526574670
BD	7	815	310.	2842737	13903.	421587883
BH	7	815	310.	2842737	13877.	105642913
MH	7	815	314.	0443277	14188.	993110178
BD	7	815	314.	0443277	14025.	900918482
BH	7	815	314.	0443277	14001.	330708562
MH	7	815	315.	8096931	6748148.	654815082
BD	7	815	315.	8096931	672211.	843779430
BH	7	815	315.	8096931	6667728.	379241424
MH	7	815	317.	8043827	14305.	507545827
BD	7	815	317.	8043827	14145.	435367344
BH	7	815	317.	8043827	14122.	393044530
MH	7	815	321.	5644377	14419.	122375249
BD	7	815	321.	5644377	14262.	004921137
BH	7	815	321.	5644377	14240.	514763652
MH	7	815	325.	3244927	14529.	902558981
BD	7	815	325.	3244927	14375.	769028781
BH	7	815	325.	3244927	14355.	728346346
MH	7	815	327.	0898581	6910747.	342498240
BD	7	815	327.	0898581	6882935.	334624562
BH	7	815	327.	0898581	6828283.	891020845
MH	7	815	329.	0845497	14637.	905839799
BD	7	815	329.	0845497	14486.	576771555
BH	7	815	329.	0845497	14468.	010498583
MH	7	815	332.	8446067	14743.	215879141
BD	7	815	332.	8446067	14594.	769684970
BH	7	815	332.	8446067	14577.	565944789

Figure 15 (cont.)

MH	7	815	337.0346707	14857.481299101
BD	7	815	337.0346707	14712.082020938
BH	7	815	337.0346707	14696.371719001
MH	7	815	338.7460331	7082608.464537685
BD	7	815	338.7460331	7053073.622008696
BH	7	815	338.7460331	6998254.921233382
MH	7	815	340.8347287	14958.344488023
BD	7	815	340.8347287	14815.736548482
BH	7	815	340.8347287	14801.311351595
MH	7	815	344.5947877	15055.630577264
BD	7	815	344.5947877	14915.664041875
BH	7	815	344.5947877	14902.468503831
MH	7	815	348.3548467	15150.477690218
BD	7	815	348.3548467	15013.160761057
TF				
BH	7	815	348.3548467	15001.161089121
MH	7	815	350.4022111	7258079.166655875
BD	7	815	350.4022111	7226923.884490048
BH	7	815	350.4022111	7171943.011748140
BD	7	815	352.1149037	15108.292650818
BH	7	815	352.1149037	15097.360564170
MH	7	815	352.1149037	15242.949146806
BD	7	815	355.8749617	15200.868110119
BH	7	815	355.8749617	15191.113845048
MH	7	815	355.8749617	15333.080380497
BD	7	815	359.6350187	15291.283792554
BH	7	815	359.6350187	15282.527558920
MH	7	815	359.6350187	15420.961614071
BD	7	815	4 3.3950767	15379.297900138
BH	7	815	4 3.3950767	15371.667978940
MH	7	815	4 3.3950767	15506.632217763
BD	7	815	4 8.0951507	15486.382873951
BH	7	815	4 8.0951507	15479.983595668
MH	7	815	4 8.0951507	15610.690288602
BD	7	815	410.9151937	15548.895013033
BH	7	815	410.9151937	15543.189960537
MH	7	815	410.9151937	15671.555117963
BD	7	815	414.6752537	15630.648293851
BH	7	815	414.6752537	15625.808726905
MH	7	815	414.6752537	15750.909120617
BD	7	815	418.4353137	15710.228674410
BH	7	815	418.4353137	15706.309383152
MH	7	815	418.4353137	15828.269028781
MH	7	8164730.6465557		-17539.915026186

Figure 15 (cont.)

MH	7	8164734	5704857	-17499	509186265
MH	7	8164734	7698161	8636694	520933860
MH	7	8164738	1664227	-17461	455380558
MH	7	8164741	9263557	-17420	572178481
MH	7	8164745	6862897	-17378	532152174
MH	7	8164746	0496161	8640011	646911034
MH	7	8164749	4462237	-17335	312007782
MH	7	8164753	2061577	-17290	874999998
MH	7	8164756	9660917	-17245	211286066
MH	7	8164757	3294171	8444773	425170239
MH	7	81648	7260267	-17198	274278162
MH	7	81648	44859627	-17150	004593133
MH	7	81648	82458967	-17100	393700836
MH	7	81648	86092211	8251104	855620212
MH	7	8164812	0058307	-17049	391732214
MH	7	8164815	7657647	-16996	995734809
MH	7	8164819	5256997	-16943	101706026
MH	7	8164819	8890251	8059156	660094117
MH	7	8164823	2856331	-16887	695866105
MH	7	8164827	0455687	-16830	776574730
MH	7	8164830	8055047	-16772	262139080
MH	7	8164831	1688321	7869046	062987763
MH	7	8164834	5654377	-16712	106627225
MH	7	8164838	3253747	-16650	266404150
MH	7	8164842	0853107	-16586	702427743
MH	7	8164842	4486411	7680961	876617118
MH	7	8164845	8452467	-16521	368110178
MH	7	8164849	6051837	-16454	212598441
MH	7	8164853	7171137	-16378	610564289
MH	7	8164853	7284521	7495052	526244734
MH	7	8164857	1250577	-16314	214566884
MH	7	81649	8849947	-16241	262139021
MH	7	81649	46449327	-16166	276246605
BD	7	81649	46449327	-16232	407808361
MH	7	81649	50092651	7311539	566893685
MH	7	81649	84048707	-16089	182742713
BD	7	81649	84048707	-16157	326771615
MH	7	8164911	7888157	-16017	973097083
BD	7	8164911	7888157	-16088	047900258
BD	7	8164911	7888157	-16165	283136366
MH	7	8164916	2880811	7130592	421233359
MH	7	8164916	3007427	-15920	201115488
MH	7	8164919	6846877	-15844	732611476
BD	7	8164919	6846877	-15919	783464489

Figure 15 (cont.)

MH	7	8164923.4446287	-15758.648950098
BD	7	8164923.4446287	-15835.989188921
MH	7	8164927.2045687	-15670.154855607
BD	7	8164927.2045687	-15749.922572134
MH	7	8164927.5679001	6952442.585295983
MH	7	8164930.9645097	-15579.190616785
BD	7	8164930.9645097	-15661.680774151
BH	7	8164930.9645097	-15745.266732214
MH	7	8164934.7244517	-15485.679790018
BD	7	8164934.7244517	-15570.657480238
BH	7	8164934.7244517	-15655.693897603
MH	7	8164937.9204027	-15404.130577383
BH	7	8164937.9204027	-15577.519028840
MH	7	8164938.8477221	6777355.314909954
MH	7	8164942.5963317	-15281.318569540
BD	7	8164942.5963317	-15372.062992035
BH	7	8164942.5963317	-15459.887467204
MH	7	8164947.0782627	-15159.574146925
BD	7	8164947.0782627	-15254.576115427
MH	7	8164949.4822247	-15092.621719060
BD	7	8164949.4822247	-15188.787729619
MH	7	8164950.1275481	6605573.326720275
MH	7	8164953.8061557	-14969.174868761
BD	7	8164953.8061557	-15068.604330717
BH	7	8164953.8061557	-15160.727034031
MH	7	8164957.2841027	-14866.995078682
BD	7	8164957.2841027	-14969.642060278
BH	7	8164957.2841027	-15062.645800458
MH	7	81650.8960467	-14758.098753212
BD	7	81650.8960467	-14863.678477584
BH	7	81650.8960467	-14958.409776865
MH	7	81650 1.4073771	6437383.792601565
MH	7	81650 4.8039867	-14636.990813612
TR			
END			

Section 4.

SAMPLE OUTPUT

4.0 This section presents the actual output from the test cases described in Section 3.6.4 whose input is listed in Figures 13, 14, and 15. Each test case is covered separately and the code numbers next to certain sections of the output correspond to the numbered paragraphs of the explanation that follows.

Due to lack of space only pieces of the total output are shown; however, the full actual output is available.

4.1 Trajectory Prediction Output

The following sequenced paragraphs describe the different parts of trajectory prediction test case output shown in Figures 16 to 19.

1. The constants used in the program (c, INTEG, NUMB, IFLAG) are printed out here in exact input card image.
2. These numbers are the geopotential inputs printed out exactly as read in.
3. The last part of the input data printed out is all the trajectory-only input.
4. Program name and identification of the particular Aerospace version.
5. The Epoch time for this run.
6. Indicators printed out giving the logical flow from segment to segment and old and new function numbers.
7. Card image of last END card in the deck.
8. Trajectory initial conditions in three coordinate systems. Initial-condition values as shown are the result of transformations which have been applied to the input values. The transformation for the input coordinate set (a. δ , β , A. r, v in this case) consists of conversion from decimal to octal numbers,

conversion of units from feet, degrees, and seconds to earth radii, radians, and minutes, and performance of corresponding inverse conversions for output. The two other types of elements sets also require accomplishment of coordinate-system transformations in addition to the number- and units-systems conversions noted above. Accuracy of the values as printed therefore is subject to numerical roundoff errors.

Quantities in the left-hand column are position and velocity components in the basic vernal equinox coordinate system, with units of feet and of feet per second. The center column gives the usual ADBARV spherical system coordinates (i.e., Type-2 initial conditions in units of feet, feet per second, and degrees). The right-hand column from top to bottom contains orbit semi-major axis, eccentricity, inclination, right ascension of ascending node, argument of perigee, and time of last perigee passage in minutes from midnight of epoch day. Other units are feet and degrees.

9. Identification of atmosphere model to be used in computing drag force. LOCKHEED and ARDC 1959 refer to the Lockheed-Jacchia and the ARDC 1959 model atmospheres, respectively. Reciprocal of ballistic coefficient, $C_D A/W$. Ballistic coefficient, $W/C_D A$. d_1 and d_2 are values of certain constants in the Lockheed-Jacchia atmosphere density expressions.
10. The product GM , or the universal gravitational constant times the mass of the earth (frequently designated by μ), expressed in units of earth radii cubed per minute squared. Unitless coefficients of the zonal harmonic terms in the earth potential field expansion (i.e., J_2 through J_{15}). Coefficients and longitudinal arguments of tesseral and sectorial terms in earth potential field expansion, with J indicating a coefficient and L an argument in degrees. The digits following J or L are the

associated Legendre polynomial degree and order, respectively.

11. Names of solar-system bodies included in computation of perturbative accelerations. In this case none are used.
12. Trajectory method indicator. The Cowell formulation of the equations of motion is the only trajectory method available in the present TRACE-D program.

Numerical integration parameters. The Gauss-Jackson method (subroutine DE02) is the only integration method available in the present TRACE-D program.

13. The indices N_1 and N_2 input in the IOB array respectively indicate the highest-degree zonal term and the highest-degree and -order tesseral term. No term higher than those indicated by these input numbers will be computed, regardless of the model coefficients and arguments that are input to the physical constants region.
14. Physical constants and units conversion factors. Decimal and octal equivalents are given for the following quantities.
 - a. OMEGA E (ω_e) Earth rotation rate in radians per minute,
 - b. ALPHA G (α_g) Right ascension of Greenwich at midnight of the day of epoch in radians,
 - c. FT/KM Feet per kilometer,
 - d. E.R/A.U. Earth radii per astronomical unit,
 - e. I-O, DISTANCE Input/output units conversion factor in feet per earth radius,
 - f. G Acceleration due to gravity in feet per second squared,
 - g. DEG/SEC//
RAD/MIN Units conversion factor in degrees per second/radians per minute,

- | | | |
|----|------------------------|---|
| h. | RELATIVE
MASS (SUN) | Mass of sun relative to
mass of earth, |
| i | (VENUS) | Mass of Venus relative to
mass of earth, |
| j. | (JUPITER) | Mass of Jupiter relative
to mass of earth, |
| k. | GM | Earth gravitational constant
(μ) in earth radii cubed per
minute squared, |
| l. | EARTH
RADIUS-FT | Number of feet per earth radius
for internal calculations
(rather than I-0), |
| m. | N.M/E.R | Number of nautical miles per
earth radius, |
| n. | I-0, VELOCITY | Conversion factor for input/
output in feet per second/
earth radii per minute, |
| o. | FT/SEC//
E.R./MIN. | Units conversion factor in
feet per second/earth radii
per minute, |
| p. | 1/EPS | Earth flattening (reciprocal
of earth ellipticity), |
| q. | (MOON) | Mass of moon relative to
mass of earth, |
| r. | (MARS) | Mass of Mars relative to
mass of earth, |
| s. | (SATURN) | Mass of Saturn relative to
mass of earth. |
15. Date and time of day (Greenwich Mean Time) with which the quantities in the print block following are to be associated.
16. Minutes from epoch, minutes from midnight of current day, system time (i.e.; seconds from midnight of current day), and current integration step size in minutes.
17. x, y, z, r : Components and magnitude of the radius vector from geocenter to satellite in the basic coordinate system in units of feet.
18. $\dot{x}, \dot{y}, \dot{z}, v$: Components and magnitude of the inertial velocity vector with respect to the basic coordinate

system in units of feet per second.

19. Geodetic latitude, in degrees, of the point where the radius vector intersects the ellipsoidal surface of the earth, geographic longitude measured east from Greenwich in degrees, altitude of the satellite above the oblate earth in nautical miles, and geodetic latitude of the subvehicle point in degrees. All latitude quantities are considered positive north of the equator and negative south of the equator.
20. α , δ , β , A: Right ascension of satellite position, declination of satellite position, flight path angle, and inertial azimuth of velocity vector in units of degrees.
21. Revolution number, nodal period in minutes, nodal period decay rate in minutes per revolution, and nodal regression rate in degrees per revolution. Due to the fact that the nodal period is calculated by simple subtraction of ascending-node crossing times, this quantity cannot be determined until two ascending node crossings have been detected. Also, since the nodal-period decay rate is computed by differencing the nodal-period values at successive ascending nodes, this rate cannot be calculated until three ascending nodes have been crossed. The nodal regression rate is computed by differencing values of right ascension at successive ascending nodes.

4.2 Observation Generation Sample Output

Figures 20 to 24 contain the output from the observation generation test case. There are numbered descriptions corresponding to the number codes on the output; however, only the output that has not been previously described in Section 4.1 is covered here. Therefore, Figures 20 and 21 are included for completeness but need no further description (see Section 4.1 for this information).

1. Bias inputs for data and last END card.
2. Sigmas. In the case of a data generation run, the sigma table is used for the purpose of specifying the standard deviation of random noise which is to be applied to the generated data. Interpretation of the printed output shown is otherwise the same as described under section for Data Generation.
3. Station locations, latitude, longitude, and altitude.

4. Data Limit Specifications. The eight columns from left to right contain station identification, data interval, minimum elevation angle, maximum elevation angle, maximum range in nautical miles, and data-generation start and stop times in days, hours, and minutes from midnight of epoch day.

The information shown indicates that the following specifications have been given to the program:

- a. Observations are to be generated for station AA at 15-second intervals whenever the computed local elevation angle is above zero degrees.
- b. No maximum elevation angle is assumed and no maximum range is to be considered (data generated for all ranges and for all elevation angles greater than zero).
- c. Station AA is assumed to be active during the time interval from epoch until a time 24 hours after midnight of epoch day.

In the case of this particular data generation run, the corresponding Specification-I input items for Stations BB through FF are identical to those for Station AA. However, this need not be true in general, inasmuch as each station is independent of the others with respect to these input items.

5. Parameter indication. The message indicates that the range bias parameter has been selected for Station BB. In the case of a data generation run, radar parameters are selected only for the purpose of applying biases to the generated data, in this case a range bias on Station BB data. The message alluding to the correction of parameters therefore should be ignored.
6. Data Types. These headings define the format of the table appearing beneath them. The purpose of this table is to define the types of data which are to be generated for each station. Except for the station-identification column header, which is printed vertically, the headings appear in two horizontal rows, with the top row displaying the symbols RANGE on the left and LONG. on the right and the second row the symbols SUR.R on the left and U, V on the right. The individual headings are interpreted in accordance with the following:

<u>Heading</u>	<u>Description or Symbol</u>	<u>Units</u>
RANGE	Range	n mi
AZMTH	Local azimuth angle	deg
ELEV.	Local elevation angle	deg
R. DOT	Range rate	ft/sec
P. DOT	Range-rate difference	ft/sec
Q. DOT	Range-rate difference	ft/sec
P	Range difference	ft
Q	Range difference	ft
AZ. DT	Rate of change of local azimuth	deg/sec
E. DOT	Rate of change of local elevation	deg/sec
R. DDT	Second time derivative of range	ft/sec ²
MU. VIS	Mutual visibility	(indicator)
LAT	Latitude of sub-vehicle point	deg
LONG	Longitude of sub-vehicle point	deg
SUR. R	Surface range, station to sub-vehicle point	n mi
HIGHT	Altitude above oblate earth	n mi
DOPLR	Doppler frequency shift	cps
LOOK	Look angle	deg
VARI	Variances	Same as corresp. observations
KAPPA	Angle between radius vector and local vertical	deg
ASPCT	Aspect angles	deg
ATTEN	Signal attenuation	db
X, Y, Z	\hat{x} , \hat{y} , \hat{z}	n mi
T-R, D	Topocentric right ascension and declination	deg
HR, ANG	Topocentric hour angle	deg
U, V	Horizon-scanner angles, u, v	deg

The two horizontal lines associated with each station are the line containing the station-identification symbol and the line immediately below it. An X on the first line of a Y on the second line indicate that the corresponding quantity as defined by the table header is to be generated. In the present example, the indicated data types for Station AA are range, azimuth, elevation, range rate, height (altitude), \hat{x} , \hat{y} , \hat{z} , topocentric hour angle, and horizon-sensor angles u and v .

7. Segment transfer messages.
8. Rise message. The time when the satellite becomes visible from a particular station (at the specified minimum elevation angle) is obtained by interpolation and printed in the manner shown along with the local azimuth angle for the corresponding time.
9. Time corresponding to generated data. The time shown is to be associated with the data quantities appearing on the line to the right of the time printout and on the line following. The time is given both in hours (0 through 24) and minutes of the day as identified at the top of the output page, as well as in minutes from start (i.e., minutes from epoch). In the case of the particular output shown, time from start corresponds to the time of day because the epoch chosen for the run happened to be midnight.
10. Maximum elevation point. The time when the elevation angle reaches its maximum is obtained by interpolation and printed along with the corresponding values for the elevation and azimuth angles in the manner shown.
11. Set message. When the time at which the elevation angle reaches the specified minimum from above is obtained by interpolation, the print shown at this position occurs.
12. Duration message. After each pass, a message is printed giving the time in minutes during which the elevation angle was above the input minimum value and the range was below the input maximum value.

4.3 Orbit Determination Sample Output

This section contains the output from the orbit determination test case. Here also, only that output which has not been previously described is considered, although all of the output is shown in Figures 25 through 31.

1. The station location card quantities, refraction indicator, sigma set, latitude, longitude, and altitude.
2. Each line is the printout of one observation card. Given are the date, station ID, both the type and set number for these measurements, and the three measurements. In this case Line 1 has a Range Rate measurement only.
3. This line contains a Range measurement only.
4. Indicates those parameters chosen in input to be estimated.
5. In this case, the spherical set of initial conditions, drag coefficient, GM, J_2 and J_3 are to be estimated.
6. The number of iterations after which the program stops. In this case, one only.
7. A count of the parameters to be estimated.
8. A count of the number of observation cards read.
9. A total obtained by assuming three observations per cards.
10. A count of all the sites entered on station location cards.
11. The number of locations that all the data has been packed into and then stored on scratch tape.
12. The number of flocks (TF and TR cards) read.
13. Segment transfer messages.
14. Differential correction bounds. This sequence corresponds to the previously described sequence of the parameter indications.
15. Weighting sigmas. The observation type number and the value of the weighting value are shown.
16. Definition of current orbit. For each iteration the current values for the parameters are used to compute the quantities shown
17. Node print. Each time the integrated trajectory crosses the equator (as determined by interpolation between integration steps) the date, time in minutes from midnight of epoch, and the rectangular elements ($x, y, z, \dot{x}, \dot{y}, \dot{z}$,) in units

of earth radii and earth radii per minute are printed. The numerical integration interval for each satellite begins at epoch and ends at the time of the latest observation for that satellite. A message is printed each time any of the events of equator crossing, start of thrusting, end of thrusting, or orbit adjust are detected during the integration interval.

18. Station identification and system time of residuals. These are to be associated with all residuals which appear on the same line. It should be noted that system time is defined as seconds from midnight of the current day.
19. Residuals. These are unnormalized differences between the input observations (as modified by bias or refraction corrections) and corresponding values for the same observation types computed from the integrated trajectory position at the observation times. Up to six residuals for the same time are printed on one line. The observation type is indicated in parentheses immediately following the residual value in each case. Note that residuals appear for the unweighted as well as for the weighted observations.

Identification of the foregoing observation-type indicators with observation descriptions or symbols defined elsewhere in this report is in accordance with the following:

<u>Indicator</u>	<u>Description or Symbol</u>	<u>Unit</u>
R	Range	ft
A	Azimuth	deg
E	Elevation	deg
TR	Topocentric right ascension	deg
TD	Topocentric declination	deg
HA	Topocentric hour angle	deg
GR	Geocentric right ascension	deg
GD	Geocentric declination	deg
U	Horizon scanner in-plane angle	deg
V	Horizon scanner cross-plane angle	deg
H	Altitude (h)	ft

<u>Indicator</u>	<u>Description or Symbol</u>	<u>Unit</u>
X	\hat{x}	ft
Y	\hat{y}	ft
Z	\hat{z}	ft
R	Range	ft
P	Range difference	ft
Q	Range difference	ft
RD	Range rate	ft/sec
PD	Range-rate difference	ft/sec
QD	Range-rate difference	ft/sec

20. Observation time. The time identified in Item 2 in terms of seconds from midnight is given in alternate form, wherein the day of the month and the hour and minute of the day are given as integers and seconds are given to two decimal places.
21. RMS summary of residuals. The root-mean-square of the residuals for each type of observation from each station is computed by the residuals editor and the result is printed at this location. Included are the station identification, number of residuals included in the RMS (i.e., the total number for that station and type minus the number deleted by the editor on this iteration), RMS, and the RMS divided by input weighting sigma. The observation-type indicators are the same as those used in the residuals print output. Units are feet, degrees and seconds. Interpretation of the range-rate summary for station MH is that 206 range rate measurements were used to compute the rms which equals 1.61216 feet per second. RMS over sigma is equal to 26.6209 feet per second.
22. Iteration number. TRACE-D performs the tracking, or orbit determination function, by computing series of differential corrections to the parameters selected by the user. The iteration number is advanced each time the process of computing a set is repeated. The number may be interpreted as an indication of the number of times the trajectory-integration/least-squares process has been performed.
23. Observation count. The number of individual observations included in the current least-squares computation is indicated.

24. Convergence indicator. If the weighted RMS for all residuals for the current iteration is less than that for any previous iteration, then the fitting process is converging and the message shown is printed. If the RMS obtained on the current iteration is greater than the smallest RMS obtained on previous iterations, the message

CURRENT ITERATION IS NOT GOOD

(RMS = 0.xxxxxxxxx xx)

is printed in this position.

25. Current solution. If the iteration is successful (i.e., the overall RMS has been lowered), indicated values are the parameter values used in the trajectory, partial derivative, and residuals computations which have just been completed. In the case of Iteration No. 1, they are the input values of the parameters.

If the iteration is bad, the words

GO BACK TO

are printed, and the values of the parameters which so far have produced the lowest RMS are recovered from memory and printed at this point. Parameter names are generally self-explanatory, with the possible exceptions of the multiple-vehicle elements. The satellite number is printed before the element name for Satellites 2 through 6.

26. Current solution in octal digits and machine units. These numbers corresponding to those described in Item 30 are given both in the octal mode and in the units used for internal computations. Use of these quantities permits bypassing units and number-system conversions during input and output.
27. RMS. This is the quantity which is to be minimized in the tracking or orbit determination process and is the root-mean-square of the normalized residuals included in the least-squares calculations on the current iteration.
28. Corrections. The result of solving the system of normal equations associated with the parameter which occupies the corresponding position in the current solution block. Units are feet, degrees, and seconds.
29. Bounds. Current values of the numbers used to limit the size of corrections. In general, these bounds are

automatically increased on a good iteration and automatically decreased on a bad one.

30. Bounding indicator. This message will be either

HITTING BOUNDS

or

NOT HITTING BOUNDS

The first message indicates that the magnitudes of the corrections have been controlled by solving the system in such a way that the constraint implied by the bounds is satisfied, and the latter that the normal equations have been solved without applying the bounds.

31. Next solution. Each value is the sum of the parameter value given in the corresponding position under "current solution" and the associated correction. These are the parameter values which will be used for the next solution.
32. Next solution in octal mode and units of earth radii, radians, and minutes.
33. Predicted RMS. If the fitting process is converging in a completely linear fashion, this will be the RMS on the next iteration. The comparison of this number with the current RMS (see Item 32) may be used to measure the degree to which the process has already converged.
34. Sigma of parameters divided by sigma of the normalized observations. The numbers given are the square roots of the diagonal elements of the inverse normal matrix. If certain assumptions are made about the characteristics of the observation set, the numbers may then be taken as the variances on the parameter solutions.
35. Correlation matrix, correlation coefficients for the parameter set. These values are computed directly from the covariance matrix (i.e., the inverse normal matrix). Rows and columns are in the same sequence as the Item 34 data.
36. This is the upper half of the normal matrix.
37. This is the lower half of the inverse normal matrix.

Figure 16. Trajectory Prediction Output Listing of Input

TRACE-D STANDARD INTEGRATION CONSTANTS										
11	1	12	2	13	0	BASIC INPUT CARD				
12	1	13	0	BASIC INPUT CARD						1
13	0	14	1	15	11	16	17	18	19	20
14	1	15	1	16	17	18	19	20	21	22
15	1	16	1	17	18	19	20	21	22	23
16	1	17	1	18	19	20	21	22	23	24
17	1	18	1	19	20	21	22	23	24	25
18	1	19	1	20	21	22	23	24	25	26
19	1	20	1	21	22	23	24	25	26	27
20	1	21	1	22	23	24	25	26	27	28
21	1	22	1	23	24	25	26	27	28	29
22	1	23	1	24	25	26	27	28	29	30
23	1	24	1	25	26	27	28	29	30	31
24	1	25	1	26	27	28	29	30	31	32
25	1	26	1	27	28	29	30	31	32	33
26	1	27	1	28	29	30	31	32	33	34
27	1	28	1	29	30	31	32	33	34	35
28	1	29	1	30	31	32	33	34	35	36
29	1	30	1	31	32	33	34	35	36	37
30	1	31	1	32	33	34	35	36	37	38
31	1	32	1	33	34	35	36	37	38	39
32	1	33	1	34	35	36	37	38	39	40
33	1	34	1	35	36	37	38	39	40	41
34	1	35	1	36	37	38	39	40	41	42
35	1	36	1	37	38	39	40	41	42	43
36	1	37	1	38	39	40	41	42	43	44
37	1	38	1	39	40	41	42	43	44	45
38	1	39	1	40	41	42	43	44	45	46
39	1	40	1	41	42	43	44	45	46	47
40	1	41	1	42	43	44	45	46	47	48
41	1	42	1	43	44	45	46	47	48	49
42	1	43	1	44	45	46	47	48	49	50
43	1	44	1	45	46	47	48	49	50	51
44	1	45	1	46	47	48	49	50	51	52
45	1	46	1	47	48	49	50	51	52	53
46	1	47	1	48	49	50	51	52	53	54
47	1	48	1	49	50	51	52	53	54	55
48	1	49	1	50	51	52	53	54	55	56
49	1	50	1	51	52	53	54	55	56	57
50	1	51	1	52	53	54	55	56	57	58
51	1	52	1	53	54	55	56	57	58	59
52	1	53	1	54	55	56	57	58	59	60
53	1	54	1	55	56	57	58	59	60	61
54	1	55	1	56	57	58	59	60	61	62
55	1	56	1	57	58	59	60	61	62	63
56	1	57	1	58	59	60	61	62	63	64
57	1	58	1	59	60	61	62	63	64	65
58	1	59	1	60	61	62	63	64	65	66
59	1	60	1	61	62	63	64	65	66	67
60	1	61	1	62	63	64	65	66	67	68
61	1	62	1	63	64	65	66	67	68	69
62	1	63	1	64	65	66	67	68	69	70
63	1	64	1	65	66	67	68	69	70	71
64	1	65	1	66	67	68	69	70	71	72
65	1	66	1	67	68	69	70	71	72	73
66	1	67	1	68	69	70	71	72	73	74
67	1	68	1	69	70	71	72	73	74	75
68	1	69	1	70	71	72	73	74	75	76
69	1	70	1	71	72	73	74	75	76	77
70	1	71	1	72	73	74	75	76	77	78
71	1	72	1	73	74	75	76	77	78	79
72	1	73	1	74	75	76	77	78	79	80
73	1	74	1	75	76	77	78	79	80	81
74	1	75	1	76	77	78	79	80	81	82
75	1	76	1	77	78	79	80	81	82	83
76	1	77	1	78	79	80	81	82	83	84
77	1	78	1	79	80	81	82	83	84	85
78	1	79	1	80	81	82	83	84	85	86
79	1	80	1	81	82	83	84	85	86	87
80	1	81	1	82	83	84	85	86	87	88
81	1	82	1	83	84	85	86	87	88	89
82	1	83	1	84	85	86	87	88	89	90
83	1	84	1	85	86	87	88	89	90	91
84	1	85	1	86	87	88	89	90	91	92
85	1	86	1	87	88	89	90	91	92	93
86	1	87	1	88	89	90	91	92	93	94
87	1	88	1	89	90	91	92	93	94	95
88	1	89	1	90	91	92	93	94	95	96
89	1	90	1	91	92	93	94	95	96	97
90	1	91	1	92	93	94	95	96	97	98
91	1	92	1	93	94	95	96	97	98	99
92	1	93	1	94	95	96	97	98	99	100
93	1	94	1	95	96	97	98	99	100	101
94	1	95	1	96	97	98	99	100	101	102
95	1	96	1	97	98	99	100	101	102	103
96	1	97	1	98	99	100	101	102	103	104
97	1	98	1	99	100	101	102	103	104	105
98	1	99	1	100	101	102	103	104	105	106
99	1	100	1	101	102	103	104	105	106	107
100	1	101	1	102	103	104	105	106	107	108
101	1	102	1	103	104	105	106	107	108	109
102	1	103	1	104	105	106	107	108	109	110
103	1	104	1	105	106	107	108	109	110	111
104	1	105	1	106	107	108	109	110	111	112
105	1	106	1	107	108	109	110	111	112	113
106	1	107	1	108	109	110	111	112	113	114
107	1	108	1	109	110	111	112	113	114	115
108	1	109	1	110	111	112	113	114	115	116
109	1	110	1	111	112	113	114	115	116	117
110	1	111	1	112	113	114	115	116	117	118
111	1	112	1	113	114	115	116	117	118	119
112	1	113	1	114	115	116	117	118	119	120
113	1	114	1	115	116	117	118	119	120	121
114	1	115	1	116	117	118	119	120	121	122
115	1	116	1	117	118	119	120	121	122	123
116	1	117	1	118	119	120	121	122	123	124
117	1	118	1	119	120	121	122	123	124	125
118	1	119	1	120	121	122	123	124	125	126
119	1	120	1	121	122	123	124	125	126	127
120	1	121	1	122	123	124	125	126	127	128
121	1	122	1	123	124	125	126	127	128	129
122	1	123	1	124	125	126	127	128	129	130
123	1	124	1	125	126	127	128	129	130	131
124	1	125	1	126	127	128	129	130	131	132
125	1	126	1	127	128	129	130	131	132	133
126	1	127	1	128	129	130	131	132	133	134
127	1	128	1	129	130	131	132	133	134	135
128	1	129	1	130	131	132	133	134	135	136
129	1	130	1	131	132	133	134	135	136	137
130	1	131	1	132	133	134	135	136	137	138
131	1	132	1	133	134	135	136	137	138	139
132	1	133	1	134	135	136	137	138	139	140
133	1	134	1	135	136	137	138	139	140	141
134	1	135	1	136	137	138	139	140	141	142
135	1	136	1	137	138	139	140	141	142	143
136	1	137	1	138	139	140	141	142	143	144
137	1	138	1	139	140	141	142	143	144	145
138	1	139	1	140	141	142	143	144	145	146
139	1	140	1	141	1					

6	.7017339	-6 7	.1652	-6 8	.521C912	-7 9	.4986992	-8	BASIC INPUT CARD	32
10	.1111605	-6 11	.1088C12	-6 12	.1717943	-7 13	.2122685	-8	BASIC INPUT CARD	33
14	.1507404	-8 15	.4256694	-7 16	.4633369	-7 17	.1291007	-8	BASIC INPUT CARD	34
18	.1967936	-8 19	.4477079	-9 20	.3729502	J0 21	.1839230	-6	BASIC INPUT CARD	35
22	.3972437	-7 23	.3543C592	-8 24	.3887152	-9 25	.3299649	J0	BASIC INPUT CARD	36
26	.1515140	J0 27	.2052417	J1 28	.6820109	-7 29	.3849809	-8	BASIC INPUT CARD	37
30	.3762496	-9 31	.2771455	-9 32	.2341330	J0 33	.8894014	J1	BASIC INPUT CARD	38
34	.1641761	J2 35	.3418347	J2 36	.7842382	-7 37	.2440136	-8	BASIC INPUT CARD	39
44	.8609215	J4 45	.1013471	-6 46	.6724120	-8 47	.4173952	-9	BASIC INPUT CARD	40
48	.7857074	J0 55	.3251625	-7 66	.1006553	-6 67	.4704701	-8	BASIC INPUT CARD	41
77	.2783799	J8							BASIC INPUT CARD	42
89	.1717906	J8 90	.3549629	J9 91	.8360589	-8			BASIC INPUT CARD	43
101	.1059143	K0							BASIC INPUT CARD	44
102	.1326684	J9 104	.1974783	K1					BASIC INPUT CARD	45
113	.5398041	J8 116	.1393759	J9 117	.1472896	K0 118	.5702221	K2	BASIC INPUT CARD	46
OBLT										
2	165.2042	3	7.623267	4	161.-8799	5	23.-63307		BASIC INPUT CARD	47
6	219.3494	7	31.73482	8	115.8047	9	25.74411		BASIC INPUT CARD	48
10	232.5121	11	169.9065	12	59.74292	13	41.60563		BASIC INPUT CARD	49
14	56.95252	15	209.876	16	140.-3382	17	50.-04699		BASIC INPUT CARD	50
18	66.28621	19	47.13021	20	42.58828	21	38.37493		BASIC INPUT CARD	51
22	12.06147	23	1.37273	24	53.46592	25	7.078959		BASIC INPUT CARD	52
26	27.20422	27	8.598698	28	139.-0856	29	28.-15497		BASIC INPUT CARD	53
30	57.94327	31	45.80993	32	22.-83747	33	15.-51001		BASIC INPUT CARD	54
34	15.09665	35	19.70539	36	5.856014	37	48.-25990		BASIC INPUT CARD	55
44	13.95194	45	309.8056	46	100.-9007	47	68.-25838		BASIC INPUT CARD	56
48	59.07748	55	164.1975	66	203.3371	67	91.-41733		BASIC INPUT CARD	57
-77	14.87681								BASIC INPUT CARD	58
89	11.44440	90	9.804658	91	160.-5400				BASIC INPUT CARD	59
101	30.31227	102	23.88277	104	13.72105	113	27.-04833		BASIC INPUT CARD	60
116	15.65423								BASIC INPUT CARD	61
117	16.-80139	118	20.-10848						BASIC INPUT CARD	62
DITM 3										

Figure 16 (cont.)

Figure 18. Initial Information

BASIC INPUT CARD 1 01

END

INITIAL CONDITIONS

X = .20748520E+08 ALPHA = .35820000E+03 A = .23107813E+08
 Y = -.65204847E+06 DELTA = -.25500000E+02 C = .77068993E-02
 Z = .99014220E+07 BETA = .90350000E+02 I = .344344E+02
 X007 = .76871283E+04 AZ = .47180000E+02 O = .23118841E+02 (8)
 Y007 = .17953868E+05 R = .22999226E+08 U = .17721544E+02
 Z007 = .19277888E+05 V = .24797590E+05 F = .81613989E+03

ATMOSPHERE - LOCKNEED CDA/M = .80000000E-02 W/CDA = .12500000E+03 (9)
 D1 = .68300000E+01 D2 = .15684000E+02

EARTH MODEL

G1 = .55303700E-02 J2 = .10826450E-02 J3 = .25460000E-05 J4 = .16490000E-05 J5 = .21000000E-06
 J6 = .64600000E-06 J7 = .33300000E-06 J8 = .27000000E-06 J9 = .53000000E-07 J10 = .54000000E-07
 J11 = .30200000E-06 J12 = .35700000E-06 J13 = .11400000E-06 J14 = .17900000E-06 J15 = .00000000E-00
 J16 = .00000000E-00 J17 = .00000000E-00 J18 = .10880120E-06 J19 = .16990650E+03
 J20 = .17659800E-05 J21 = .16220420E+03 J22 = .17179430E-07 J23 = .59742920E+02
 J24 = .21107450E-05 J25 = .78232670E+01 J26 = .21226850E-08 J27 = .41605630E+02
 J28 = .31084290E-06 J29 = .16187990E+03 J30 = .15074040E-08 J31 = .56952520E+02
 J32 = .23905980E-06 J33 = .23633070E+02 J34 = .42646940E-07 J35 = .20987600E+03
 J36 = .70171390E-06 J37 = .21934940E+03 J38 = .46333690E-07 J39 = .14033820E+03
 J40 = .16528080E-06 J41 = .31744820E+02 J42 = .12910070E-08 J43 = .50046980E+02
 J44 = .32309120E-07 J45 = .11588070E+03 J46 = .19679360E-08 J47 = .6286210E+02
 J48 = .49869920E-08 J49 = .23744110E+02 J50 = .44770790E-09 J51 = .47130210E+02
 J52 = .111116050E-06 J53 = .23251210E+03 J54 = .37295020E-10 J55 = .42588280E+02

J 7 1 = .18392300E-06 J12 5 = .00000000E-00 L12 5 = .00000000E-00
 J 7 2 = .39724370E-07 J12 6 = .00000000E-00 L12 6 = .00000000E-00
 J 7 3 = .35430592E-00 J12 7 = .00000000E-00 L12 7 = .00000000E-00
 J 7 4 = .38871520E-09 J12 8 = .00000000E-00 L12 8 = .00000000E-00
 J 7 5 = .32996490E-10 J12 9 = .00000000E-00 L12 9 = .00000000E-00
 J 7 6 = .15151400E-10 J1210 = .00000000E-00 L1210 = .00000000E-00
 J 7 7 = .20524170E-11 J1211 = .00000000E-00 L1211 = .00000000E-00
 J 8 1 = .68281090E-07 J1212 = .27837990E-18 L1212 = .14876810E+02
 J 8 2 = .3848090E-08 J13 1 = .00000000E-00 L13 1 = .00000000E-00
 J 8 3 = .37624860E-09 J13 2 = .00000000E-00 L13 2 = .00000000E-00
 J 8 4 = .27714550E-09 J13 3 = .00000000E-00 L13 3 = .00000000E-00
 J 8 5 = .23413300E-10 J13 4 = .00000000E-00 L13 4 = .00000000E-00
 J 8 6 = .88940140E-11 J13 5 = .00000000E-00 L13 5 = .00000000E-00
 J 8 7 = .16411610E-12 J13 6 = .00000000E-00 L13 6 = .00000000E-00
 J 8 8 = .34183470E-12 J13 7 = .00000000E-00 L13 7 = .00000000E-00
 J 8 9 = .76423820E-07 J13 8 = .00000000E-00 L13 8 = .00000000E-00
 J 9 2 = .24401360E-08 J13 9 = .00000000E-00 L13 9 = .00000000E-00
 J 9 3 = .00000000E-00 J1310 = .00000000E-00 L1310 = .00000000E-00
 J 9 4 = .00000000E-00 J1311 = .00000000E-00 L1311 = .00000000E-00
 J 9 5 = .00000000E-00 J1312 = .17179060E-18 L1312 = .11444440E+02
 J 9 6 = .00000000E-00 J1313 = .35494290E-19 L1313 = .7804580E+01
 J 9 7 = .00000000E-00 J14 1 = .00000000E-00 L14 1 = .16054000E+03
 J 9 8 = .00000000E-00 J14 2 = .00000000E-00 L14 2 = .00000000E-00
 J 9 9 = .86092150E-14 J14 3 = .00000000E-00 L14 3 = .00000000E-00
 J10 1 = .10134710E-06 J14 4 = .00000000E-00 L14 4 = .00000000E-00
 J10 2 = .6713520E-08 J14 5 = .00000000E-00 L14 5 = .00000000E-00
 J10 3 = .6173520E-09 J14 6 = .00000000E-00 L14 6 = .00000000E-00
 J10 4 = .68527460E-10 J14 7 = .00000000E-00 L14 7 = .00000000E-00

(10)

J10 5=	.0000000E 00	J10 5=	.0000000E 00	J14 8=	.0000000E 00	L14 8=	.0000000E 00
J10 6=	.0000000E 00	J10 6=	.0000000E 00	J14 9=	.0000000E 00	L14 9=	.0000000E 00
J10 7=	.0000000E 00	J10 7=	.0000000E 00	J14 10=	.0000000E 00	L14 10=	.0000000E 00
J10 8=	.0000000E 00	J10 8=	.0000000E 00	J14 11=	.0000000E 00	L14 11=	.0000000E 00
J10 9=	.0000000E 00	J10 9=	.0000000E 00	J14 12=	.0000000E 00	L14 12=	.0000000E 00
J10 10=	.0000000E 00	J10 10=	.0000000E 00	J14 13=	.0000000E 00	L14 13=	.0000000E 00
J11 1=	.32516250E-07	J11 1=	.16419750E+03	J14 14=	.19747830E-21	L14 14=	.13741050E+02
J11 2=	.0000000E 00	J11 2=	.0000000E 00	J15 1=	.0000000E 00	L15 1=	.0000000E 00
J11 3=	.0000000E 00	J11 3=	.0000000E 00	J15 2=	.0000000E 00	L15 2=	.0000000E 00
J11 4=	.0000000E 00	J11 4=	.0000000E 00	J15 3=	.0000000E 00	L15 3=	.0000000E 00
J11 5=	.0000000E 00	J11 5=	.0000000E 00	J15 4=	.0000000E 00	L15 4=	.0000000E 00
J11 6=	.0000000E 00	J11 6=	.0000000E 00	J15 5=	.0000000E 00	L15 5=	.0000000E 00
J11 7=	.0000000E 00	J11 7=	.0000000E 00	J15 6=	.0000000E 00	L15 6=	.0000000E 00
J11 8=	.0000000E 00	J11 8=	.0000000E 00	J15 7=	.0000000E 00	L15 7=	.0000000E 00
J11 9=	.0000000E 00	J11 9=	.0000000E 00	J15 8=	.0000000E 00	L15 8=	.0000000E 00
J11 10=	.0000000E 00	J11 10=	.0000000E 00	J15 9=	.53988410E-18	L15 9=	.2708538E+02
J11 11=	.0000000E 00	J11 11=	.0000000E 00	J15 10=	.0000000E 00	L15 10=	.0000000E 00
J12 1=	.18069530E-06	J12 1=	.20559710E+03	J15 11=	.0000000E 00	L15 11=	.0000000E 00
J12 2=	.47047010E-08	J12 2=	.91471730E+02	J15 12=	.13937590E-19	L15 12=	.15654230E+02
J12 3=	.0000000E 00	J12 3=	.0000000E 00	J15 13=	.14928960E-20	L15 13=	.16801390E+02
J12 4=	.0000000E 00	J12 4=	.0000000E 00	J15 14=	.57022210E-22	L15 14=	.20108480E+02
				J15 15=	.0000000E 00	L15 15=	.0000000E 00

(18)

THE FOLLOWING BODIES ARE USED FOR PLANETARY PERTURBATIONS (11)

NONE

FORMULATION CONELL FEQ.S.DF ADIION)

DIFFERENTIAL EQUATION SUBROUTINE E BAR= .1000E-09 A= 1.000 RATIO OF CONELL STEP TO RUNGE KUTTA 4 (12)
 GAUSS-JACKSON INITIAL= .1000E+01 MINIMUM= .1562E-01 MAXIMUM= .6480E+02
 DO NOT RECOMPUTE PERTURBATIONS FOR CORRECTOR
 EQUATIONS OF MOTION USE N1=14 N2=15 (13)

OMEGA C	DECIMAL	DECIMAL	DECIMAL
ALPHA G	.43752690E-02	.32540203260	.55303706E-02
EPHRA	.49787546E+01	75221325620	66221635100
E.R./A.U.	.32868399E+04	34935533740	.20928738E+08
I-O, DISTANCE	.23454865E+05	565605075320	.34439335E+04
WAVESEC/RAD/MIN	.20925738E+08	452000000000	.34876230E+06
RELATIVE MASS(SUN)	.32176000E+02	132071260100	.34876230E+06
(VENUS)	.10471976E+01	444250714340	.29900000E+03
(JUPITER)	.81497900E+00	33295130E+06	.12788700E-01
	.31788700E+03	422335136140	.95129000E+02
			.30446722720

CAME FROM SEGMENT 2 ARE IN SEGMENT 02 FUNCTION IS 3
 OLD FUNCTION IS 3 NEW FUNCTION IS 3

12.18.49 BEGIN EXECUTION
 CAME FROM SEGMENT 62 ARE IN SEGMENT 1 FUNCTION IS 3
 OLD FUNCTION IS 3 NEW FUNCTION IS 3

12.18.52 BEGIN EXECUTION
 CAME FROM SEGMENT 1 ARE IN SEGMENT 12 FUNCTION IS 3
 OLD FUNCTION IS 3 NEW FUNCTION IS 3

Figure 18 (cont.)

Figure 20. (Cont.)

OBLT	2	-13.18	3	5.31		BASIC INPUT CARD	32		
	4	-13.33	5	16.00	6	-135.60	BASIC INPUT CARD 33		
	7	27.47	8	-1.10	9	36.01	BASIC INPUT CARD 34		
	10	-81.86	11	-2.60	12	-3.45	BASIC INPUT CARD 35		
	13	50.25	14	-15.32	15	157.21	BASIC INPUT CARD 36		
	16	115.15	17	-1.75	18	60.74	BASIC INPUT CARD 37		
	19	-17.75	20	-14.34			SIC INPUT CARD 38		
	2	1082.76	6	3	-6	4	-1.56	BASIC INPUT CARD 39	
	5	-0.06	8	8	39	-6	7	-6.33	BASIC INPUT CARD 40
	8	0.	9	.210		-61108	9		BASIC INPUT CARD 41
	12	6	13	9	14	6			BASIC INPUT CARD 42
	15	4	16	1965		1MATH 2			BASIC INPUT CARD 43
	IDAY	23							BASIC INPUT CARD 44
	RECTYPE								BASIC INPUT CARD 45
	IC	-60.							BASIC INPUT CARD 46
	2	0.	3	90.					BASIC INPUT CARD 47
	4	25.							BASIC INPUT CARD 48
	5	-607612.	6	-1.					BASIC INPUT CARD 49
	IPTAPE4								BASIC INPUT CARD 50
	PROJECT	11516	1	12	2				BASIC INPUT CARD 51
	13	3	14	4	15	5			BASIC INPUT CARD 52
	16	6	17	7	18	8			BASIC INPUT CARD 53
	19	13	110	14	111	15			BASIC INPUT CARD 54
	112	19							BASIC INPUT CARD 55
	3	.1	4	.05	5	.05	6	.05	BASIC INPUT CARD 56
	7	.05	8	.05	9	1000.			BASIC INPUT CARD 57
	10	1000.	11	1000.	12	.1			BASIC INPUT CARD 58
	END								BASIC INPUT CARD 59

Figure 22. Initial Information

```

RRPARDS+99
D01,0188 RHIAS 03,011000 } (1)
BASIC INPUT CARD 1
BASIC INPUT CARD 2
BASIC INPUT CARD 3
END
    
```

```

SIGMA TABLE
1 .1000000E+03 2 .1000000E-00 3 .1000000E-00 4 .5000000E-01 5 .5000000E-01 6 .5000000E-01 (2)
7 .5000000E-01 8 .5000000E-01 13 .1000000E+04 14 .1000000E+04 15 .1000000E+04 19 .1000000E-00
    
```

```

INITIAL CONDITIONS
X = -.10056004E+07 ALPHA = .92676667E+02 A = .21533333E+08
Y = .21509860E+08 DELTA = .00000000E 00 E = .3586534E-09
Z = .00000000E 00 BETA = .90000000E+02 I = .65000000E+02
XDOT = -.10793656E+05 AZ = .25000000E+02 C = .92676667E+02
YDOT = -.50461068E+03 R = .21533333E+08 U = .90005515E+02
ZDOT = .23172351E+05 V = .25567860E+05 T = .66145701E+02
    
```

```

ATMOSPHERE - LOCKHEED CDA/M = .10000000E-01 W/CDA = .10000000E+03
D1 = .68300000E+01 D2 = -.15684000E+02
    
```

```

EARTH MODEL
GM = .55304505E-02 J2 = .10827600E-02 J3 = -.26930000E-05 J4 = -.15600000E-05 J5 = -.60000000E-08
J6 = .39000000E-06 J7 = -.63300000E-06 J8 = .00000000E 00 J9 = .21000000E-06 J10 = .00000000E 00
J21 = .00000000E 00 L21 = .00000000E 00 J52 = .53290000E-07 L52 = -.26000000E+01
J22 = .17230000E-05 L22 = -.13180000E+02 J53 = .58420000E-08 L53 = -.34500000E+01
J31 = .18560000E-05 L31 = .53100000E+01 J54 = .40930000E-08 L54 = .58250000E+02
J32 = .44820000E-06 L32 = -.13330000E+02 J55 = .84620000E-09 L55 = -.15320000E+02
J33 = .16430000E-06 L33 = .16000000E+02 J61 = .66110000E-07 L61 = .15721000E+03
J41 = .27800000E-06 L41 = -.13680000E+03 J62 = .37460000E-07 L62 = .11315000E+03
J42 = .15360000E-06 L42 = .21740000E+02 J63 = .11660000E-08 L63 = -.17500000E+01
J43 = .57190000E-07 L43 = -.11000000E+01 J64 = .22560000E-08 L64 = .60740000E+02
J44 = .47810000E-08 L44 = .36010000E+02 J65 = .33280000E-09 L65 = -.17750000E+02
J51 = .15090000E-06 L51 = -.81860000E+02 J66 = .51530000E-10 L66 = -.14340000E+02
    
```

THE FOLLOWING BODIES ARE USED FOR PLANETARY PERTURBATIONS

NONE

FORMULATION COWELL (EQS.OF MOTION)

```

DIFFERENTIAL EQUATION SUBROUTINE E BAR = .1000E-09 A = 1.000 RATIO OF COWELL STEP TO RUNGE KUTTA 4
STEP SIZE - GAUSS-JACKSON INITIAL = .100E+01 MINIMUM = .1562E-01 MAXIMUM = .640E+02
DO NOT RECOMPUTE PERTURBATIONS FOR CORRECTOR
    
```

EQUATIONS OF MOTION USE N1 = 9 N2 = 6

```

CONSTANTS
DECIMAL OCIN
OMEGA E .43752695E-02 327323635240 GM
ALPHA G .26647105E+01 474077224500
DECIMAL OCIAL
.55304505E-02 620017123540
    
```



```

FT/KM      .32008399E+04  34035333740  EARTH RADIUS - FT  .20925741E+08  455000000000
E.R./A.U.  .23454865E+05  565605075320  N.M./E.R.        .34439336E+04  740032155600
I-O, DISTANCE  .20925741E+08  455000000000  I-O, VELOCITY    .34876230E+06  223146314620
G          .32176000E+02  132071260100  FY/SEC/7E.R./MIN.  .34876230E+06  223146314620
DEG/SEC//RAD/MIN  .19471976E+01  444250714340  I/EPS.           .29830000E+03  314631463140
RELATIVE MASS(SUN)  .33293130E+06  723146314620  (MOON)           .12299900E-01  412076346600
(VENUS)      .31497900E+00  35533752020  (MARS)           .10782100E-00  203232223700
(JUPITER)    .31789700E+03  422335136140  (SATURN)        .95129000E+02  304467227200

```

```

CAME FROM SEGMENT 2 ARE IN SEGMENT 62 FUNCTION IS 4
OLD FUNCTION IS 4 NEW FUNCTION IS 4

```

14.36.56 BEGIN EXECUTION

```

CAME FROM SEGMENT 62 ARE IN SEGMENT 1 FUNCTION IS 4
OLD FUNCTION IS 4 NEW FUNCTION IS 4

```

14.36.58 BEGIN EXECUTION

```

CAME FROM SEGMENT 1 ARE IN SEGMENT 12 FUNCTION IS 4

```

Figure 22 (Cont.)

Figure 23. Data Specifications

STATIONS	SIG	REF	LATITUDE	LONGITUDE	HEIGHT
AA	.	.	75.00000000	300.00000000	1000.0000
BB	.	.	45.00000000	240.00000000	100.0000
CC	.	.	00.00000000	315.00000000	500.0000
DD	.	.	00.00000000	15.00000000	200.0000
EE	.	.	-15.00000000	135.00000000	100.0000
FF	.	.	-65.00000000	75.00000000	5000.0000

(3)

DATA	INTERVAL	MIN.EL	MAX.EL	MAX.RANGE	MDT	START	STOP
	SEC.	DEG.	DEG.	N,M	MIN.	DA HR MN	DA HR MN
AA	15.00000	-00	+00	.	.0	. . 70.	. 24.
BB	15.00000	+00	+00	.	.0	. . 70.	. 24.
CC	15.00000	+00	+00	.	.0	. . 70.	. 24.
DD	15.00000	+00	+00	.	.0	. . 70.	. 24.
EE	15.00000	+00	+00	.	.0	. . 70.	. 24.
FF	15.00000	+00	+00	.	.0	. . 70.	. 24.

(4)

PARAMETERS TO BE CORRECTED

BB
BIAS (5)

DATA TYPES	S	RANGE	AZMTH	ELEV.	R.DOT	P.DOT	Q.DOT	P	Q	AZ.DT	E.DOT	R.DOT	MU.VIS	LAT.	LONG.
T
A
F

ASPECT ATTEN X,Y,Z T-R,C G-R,D HR.ANG. U,V

AA	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
BB	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
CC	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
DD	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
EE	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
FF	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X

(6)

CAME FROM SEGMENT 12 ARE IN SEGMENT 1 FUNCTION IS 4
 OLD FUNCTION IS 4 NEW FUNCTION IS 4
 CAME FROM SEGMENT 1 ARE IN SEGMENT 62 FUNCTION IS 4
 OLD FUNCTION IS 4 NEW FUNCTION IS 4

Figure 24. Generated Data

FEBRUARY 23, 1965

ST HR	MINS	T-ST	RANGE QM'Y YARDS	AZIMUTH DEGREES	ELEVATION DEGREES	RANGE RATE FT/SEC	DECLIN DEGREES	GEO DEGREES	TOP HR-ANG DEGREES	HEIGHT QM'Y YARDS	X DEGREES	Y DEGREES	Z KILC YARDS
AA	RISE (.00 DEGREES	ELEV.)	3. HOURS	14.57 MINUTES	AZIMUTH	162.149 DEGREES	(8)					
AA	3.	14.75	194.75	159.154	-835	-7043.454	105.410	1088.808	-1286.868	3112.074			
AA	3.	15.00	195.00	159.308	-5391.169	334.506	77.061	64.395					
AA	3.	15.25	195.25	151.007	1.340	-3656.130	105.447	1138.030	-1177.339	3137.836			
AA	3.	15.50	195.50	146.840	1.315	-1881.900	330.236	78.083	64.483				
AA	3.	15.75	195.75	142.366	1.218	-36.293	325.904	79.104	64.583				
AA	3.	16.00	196.00	137.939	1.426	1790.209	317.202	81.148	64.700				
AA	3.	16.25	196.25	133.852	1.129	3586.645	105.463	1234.504	-954.212	3176.608			
AA	3.	16.50	196.50	129.605	.998	5325.267	105.455	1257.468	-898.441	3184.295			
AA	3.	16.75	196.75	125.807	.955	6981.888	308.742	83.192	64.808				
AA	3.	17.00	197.00	119.851	-8.465	168.705	304.604	84.214	64.851				
AA	SET I	.00 DEGREES	ELEV.)	3. HOURS	16.93 MINUTES	AZIMUTH	122.587 DEGREES	(11)					
AA	4.	43.00	283.00	827.557	201.704	-15084.728	105.313	552.279	-1572.426	3122.351			
AA	4.	43.25	283.25	791.759	198.381	-13902.781	105.330	595.668	-1531.189	3134.880			
AA	4.	43.50	283.50	759.095	194.527	-12552.291	105.342	639.448	-1488.138	3146.351			
AA	4.	43.75	283.75	729.978	190.348	-11022.434	105.349	682.631	-1446.793	3156.854			
AA	4.	44.00	284.00	704.815	185.950	-9308.496	105.351	725.885	-1404.008	3166.334			
AA	4.	44.25	284.25	684.137	181.183	-7416.445	105.348	769.494	-1361.406	3174.670			
AA	4.	44.50	284.50	668.364	178.239	-5364.263	105.340	812.380	-1318.244	3182.736			
AA	4.	44.75	284.75	657.782	170.775	-3185.517	105.327	855.121	-1274.715	3188.946			
AA	4.	45.00	285.00	652.696	165.697	-926.626	105.309	898.104	-1230.643	3194.411			
AA	MAX EL	4.25 DEGREES	ELEV.)	4. HOURS	45.10 MINUTES	AZIMUTH	163.452 DEGREES						
AA	5.	45.25	285.25	653.199	160.142	1356.185	105.287	940.288	-1186.490	3198.845			
AA	4.	45.50	285.50	659.353	155.064	3604.314	105.259	982.733	-1142.031	3202.239			
AA	4.	45.75	285.75	648.811	-9.735	174.948	336.541	87.042	64.936				

Figure 24 (cont.)

FEBRUARY 23, 1965

ST HR	MINS	T-ST	RANGE QM·Y YARDS	AZIMUTH DEGREES	ELEVATION DEGREES	RANGE RATE FT/SEC	X QM·Y YARDS	Y KM·YARDS	Z TOP RT, ASC DEGREES		
BB	4.	33.25	273.25	146.101	9.97	-14120.608	-1090.303	-2761.350	1931.005	142.384	
				109.545	32.927	318.752	36.990	2.207			
BB	4.	33.50	273.50	144.468	1.352	-12858.371	-1052.616	-2744.016	1976.559	146.073	
				791.225	33.831	315.185	38.011	52.849			
BB	4.	33.75	273.75	140.606	1.847	-11430.015	-1014.499	-2725.958	2020.881	149.823	
				110.856	34.761	311.506	39.032	53.463			
BB	4.	34.00	274.00	136.292	2.426	-9830.536	-876.125	-2706.477	2064.999	153.686	
				111.499	35.634	307.717	40.053	54.052			
BB	4.	34.25	274.25	131.735	2.580	-8061.687	-937.243	-2686.516	2108.533	157.456	
				112.253	36.483	303.912	41.074	54.617			
BB	4.	34.50	274.50	127.075	3.059	-6136.014	-897.994	-2666.067	2151.478	161.617	
				122.830	37.453	299.906	42.095	55.157			
BB	4.	34.75	274.75	121.944	3.273	-4078.574	-858.816	-2644.261	2193.127	165.635	
				113.480	36.209	295.850	43.116	55.675			
BB	4.	35.00	275.00	116.710	3.554	-1927.175	-818.891	-2621.992	2234.590	169.611	
				114.217	39.090	291.897	44.137	56.172			
BB	MAX EL (3.63	DEGREES ELEV.)	4.	HOURS	35.24	MINUTES	AZIMUTH	111.684	DEGREES	
BB	4.	35.25	275.25	111.575	3.539	271.158	-778.823	-2599.453	2275.219	173.764	
				114.980	40.061	287.876	45.158	56.648			
BB	4.	35.50	275.50	106.379	3.310	2462.983	-738.242	-2575.600	2315.230	177.842	
				9.039	115.767	283.914	46.179	57.103			
BB	4.	35.75	275.75	101.208	3.412	4596.676	-697.821	-2551.261	2354.177	181.731	
				116.557	41.678	280.135	47.200	57.540			
BB	4.	36.00	276.00	96.345	2.951	6626.616	-657.093	-2526.583	2392.713	185.522	
				2.469	117.317	276.378	48.221	57.959			
BB	4.	36.25	276.25	91.502	2.695	8518.012	-615.847	-2500.517	2430.301	189.163	
				118.176	43.330	272.712	49.242	58.360			
BB	4.	36.50	276.50	87.009	2.224	10248.754	-574.153	-2473.836	2467.506	192.671	
				118.931	44.102	269.398	50.263	58.744			
BB	4.	36.75	276.75	82.804	1.852	11808.934	-532.641	-2446.770	2503.773	196.169	
				119.796	44.983	263.928	51.285	59.111			
BB	4.	37.00	277.00	79.017	1.125	13198.797	-490.672	-2418.845	2538.768	199.309	
				8.378	120.652	262.762	52.306	59.464			
BB	4.	37.25	277.25	75.579	1.038	14425.412	-448.228	-2390.327	2573.149	202.320	
				10.429	121.607	259.860	53.327	59.801			
BB	SET (0.00	DEGREES ELEV.)	4.	HOURS	37.38	MINUTES	AZIMUTH	73.682	DEGREES	
BB	ELAPSED VISIBLE TIME =	4.27	MINUTES	6.	HOURS	1.85	MINUTES	AZIMUTH	228.700	DEGREES	
BB	6.	2.00	362.00	808.339	229.231	1.394	-23616.336	-1939.243	-2134.200	2055.880	65.177
				26.924	111.217	35.496	58.250	39.835	53.932		
BB	6.	2.25	362.25	750.146	230.414	1.911	-23518.703	-1896.105	-2130.351	2099.512	65.049
				25.454	111.879	36.375	58.453	40.856	54.501		
BB	6.	2.50	362.50	692.273	231.523	3.312	-23387.981	-1852.034	-2126.213	2142.083	64.774
				23.949	112.497	37.206	58.698	41.877	55.047		
BB	6.	2.75	362.75	634.744	233.061	4.435	-23212.145	-1807.965	-2122.050	2184.493	64.550
				22.047	113.209	38.127	59.115	42.898	55.570		

Figure 25. Orbit Determination Output Listing of Input

TRACE-D STANDARD INTEGRATION CONSTANTS									
11	12	2	13	6	1	11	1.00002516	BASIC INPUT CARD 1	BASIC INPUT CARD 2
4	1	5	1	11	1.00002516			BASIC INPUT CARD 3	BASIC INPUT CARD 4
23	.1	-9						BASIC INPUT CARD 5	BASIC INPUT CARD 6
26	1							BASIC INPUT CARD 7	BASIC INPUT CARD 8
30	1	31	.015625	32	64	33	1	-7	BASIC INPUT CARD 9
134	4	135	1	37	.0001	38	0.		BASIC INPUT CARD 10
40	2826.18012	141	1						BASIC INPUT CARD 11
TRACE-D STANDARD PHYSICAL CONSTANTS 10/ 1/65									
1	.437526904-2	2	.58304203 -2	6	.5			BASIC INPUT CARD 12	BASIC INPUT CARD 13
8	.437526904-2	9	1.	10	10			BASIC INPUT CARD 14	BASIC INPUT CARD 15
13	3280.8399	14	57.2957795	15	20925738			BASIC INPUT CARD 16	BASIC INPUT CARD 17
16	332951.3	17	.01229853	18	.814979			BASIC INPUT CARD 18	BASIC INPUT CARD 19
19	.107821	20	317.887	21	95.129			BASIC INPUT CARD 20	BASIC INPUT CARD 21
22	23454.865	23	3443.93355	24	20925738			BASIC INPUT CARD 22	BASIC INPUT CARD 23
25	348762.3	26	32.174	30	348762.3			BASIC INPUT CARD 24	BASIC INPUT CARD 25
31	1.5	32	1.0471976	33	3.14159265			BASIC INPUT CARD 26	BASIC INPUT CARD 27
34	298.3	35	300000.	36	82505.922			BASIC INPUT CARD 28	BASIC INPUT CARD 29
NUMB	42	3443.9336						BASIC INPUT CARD 30	BASIC INPUT CARD 31
DTIN 12								BASIC INPUT CARD 32	BASIC INPUT CARD 33
DPRCDE X X								BASIC INPUT CARD 34	BASIC INPUT CARD 35
TICTYP2								BASIC INPUT CARD 36	BASIC INPUT CARD 37
IC 23.11454								BASIC INPUT CARD 38	BASIC INPUT CARD 39
2	26.51516							BASIC INPUT CARD 40	BASIC INPUT CARD 41
3	89.88977							BASIC INPUT CARD 42	BASIC INPUT CARD 43
4	45.73312							BASIC INPUT CARD 44	BASIC INPUT CARD 45
5	24780836.7							BASIC INPUT CARD 46	BASIC INPUT CARD 47
6	23785.259							BASIC INPUT CARD 48	BASIC INPUT CARD 49
IMAX111								BASIC INPUT CARD 50	BASIC INPUT CARD 51
IYEAR 1967								BASIC INPUT CARD 52	BASIC INPUT CARD 53
IMNTH 7								BASIC INPUT CARD 54	BASIC INPUT CARD 55
IRAY 8								BASIC INPUT CARD 56	BASIC INPUT CARD 57

Figure 25 (cont.)

5	22.96	BASIC INPUT CARD	64
6	.06056	BASIC INPUT CARD	65
		BASIC INPUT CARD	66
		BASIC INPUT CARD	67
		BASIC INPUT CARD	68
		BASIC INPUT CARD	69
		BASIC INPUT CARD	70
		BASIC INPUT CARD	71
		BASIC INPUT CARD	72
		BASIC INPUT CARD	73
		BASIC INPUT CARD	74
		BASIC INPUT CARD	75
		BASIC INPUT CARD	76
		BASIC INPUT CARD	77
		BASIC INPUT CARD	78
		BASIC INPUT CARD	79
		BASIC INPUT CARD	80
		BASIC INPUT CARD	81
		BASIC INPUT CARD	82
		BASIC INPUT CARD	83
		BASIC INPUT CARD	84
		BASIC INPUT CARD	85

Figure 26 (cont.)

7	8	14	54	13.0356	MH	70	--.16183004E+05	.00000000E 00	.00000000E 00
7	8	14	54	16.7956	MH	70	--.16115794E+05	.00000000E 00	.00000000E 00
7	8	14	54	20.5955	MH	70	--.16046088E+05	.00000000E 00	.00000000E 00
7	8	14	54	24.4548	MH	10	--.78594983E+07	.00000000E 00	.00000000E 00
7	8	14	54	28.3555	MH	70	--.15975297E+05	.00000000E 00	.00000000E 00
7	8	14	54	29.1154	MH	70	--.15902687E+05	.00000000E 00	.00000000E 00
7	8	14	54	31.8753	MH	70	--.15828202E+05	.00000000E 00	.00000000E 00
7	8	14	54	34.1106	MH	10	--.76731863E+07	.00000000E 00	.00000000E 00
7	8	14	54	35.6353	MH	70	--.15751795E+05	.00000000E 00	.00000000E 00
7	8	14	54	39.3952	MH	70	--.15673354E+05	.00000000E 00	.00000000E 00
7	8	14	54	43.1552	MH	70	--.15592932E+05	.00000000E 00	.00000000E 00
7	8	14	54	45.5784	MH	10	--.74935796E+07	.00000000E 00	.00000000E 00
7	8	14	54	46.9151	MH	70	--.15510398E+05	.00000000E 00	.00000000E 00
7	8	14	54	50.6750	MH	70	--.15425733E+05	.00000000E 00	.00000000E 00
7	8	14	54	54.4350	MH	70	--.15338886E+05	.00000000E 00	.00000000E 00
7	8	14	54	56.8503	MH	10	--.73197144E+07	.00000000E 00	.00000000E 00
7	8	14	54	58.1949	MH	70	--.15250051E+05	.00000000E 00	.00000000E 00
7	8	14	55	1.9549	MH	70	--.15158382E+05	.00000000E 00	.00000000E 00
7	8	14	55	5.7148	MH	70	--.15064618E+05	.00000000E 00	.00000000E 00
7	8	14	55	8.1361	MH	10	--.71489035E+07	.00000000E 00	.00000000E 00
7	8	14	55	9.4747	MH	70	--.14968426E+05	.00000000E 00	.00000000E 00
7	8	14	55	13.2347	MH	70	--.14869750E+05	.00000000E 00	.00000000E 00
7	8	14	55	16.9946	MH	70	--.14768548E+05	.00000000E 00	.00000000E 00
7	8	14	55	19.4179	MH	10	--.69813415E+07	.00000000E 00	.00000000E 00
7	8	14	55	20.7546	MH	70	--.14664727E+05	.00000000E 00	.00000000E 00
7	8	14	55	24.5145	MH	70	--.14558237E+05	.00000000E 00	.00000000E 00
7	8	14	55	28.2745	MH	70	--.14449018E+05	.00000000E 00	.00000000E 00
7	8	14	55	30.6858	MH	10	--.68146050E+07	.00000000E 00	.00000000E 00
7	8	14	55	34.0344	MH	70	--.14336992E+05	.00000000E 00	.00000000E 00
7	8	14	55	35.7943	MH	70	--.14222113E+05	.00000000E 00	.00000000E 00
7	8	14	55	39.5543	MH	70	--.14104283E+05	.00000000E 00	.00000000E 00
7	8	14	55	42.3536	MH	10	--.66518137E+07	.00000000E 00	.00000000E 00
7	8	14	55	43.3142	MH	70	--.13983450E+05	.00000000E 00	.00000000E 00
7	8	14	55	47.0742	MH	70	--.13859568E+05	.00000000E 00	.00000000E 00
7	8	14	55	50.8341	MH	70	--.13732534E+05	.00000000E 00	.00000000E 00
7	8	14	55	53.6334	MH	10	--.64958471E+07	.00000000E 00	.00000000E 00
7	8	14	55	54.5941	MH	70	--.13602290E+05	.00000000E 00	.00000000E 00
7	8	14	55	58.3540	MH	70	--.13468764E+05	.00000000E 00	.00000000E 00
7	8	14	56	2.1140	MH	70	--.13331885E+05	.00000000E 00	.00000000E 00
7	8	14	56	4.9133	MH	10	--.63443148E+07	.00000000E 00	.00000000E 00
7	8	14	56	5.8739	MH	70	--.13191593E+05	.00000000E 00	.00000000E 00
7	8	14	56	9.6339	MH	70	--.13047800E+05	.00000000E 00	.00000000E 00
7	8	14	56	13.3938	MH	70	--.12900445E+05	.00000000E 00	.00000000E 00
7	8	14	56	16.1931	MH	10	--.61975452E+07	.00000000E 00	.00000000E 00
7	8	14	56	17.1538	MH	70	--.12749447E+05	.00000000E 00	.00000000E 00
7	8	14	56	20.9137	MH	70	--.12594759E+05	.00000000E 00	.00000000E 00
7	8	14	56	24.6737	MH	70	--.12436287E+05	.00000000E 00	.00000000E 00
7	8	14	56	27.4730	MH	10	--.60559275E+07	.00000000E 00	.00000000E 00
7	8	14	56	28.4336	MH	70	--.12273993E+05	.00000000E 00	.00000000E 00
7	8	14	56	31.8176	MH	70	--.12124570E+05	.00000000E 00	.00000000E 00
7	8	14	56	36.8006	MH	10	--.57145949E+07	.00000000E 00	.00000000E 00
7	8	14	56	37.4793	MH	70	--.10883785E+05	.00000000E 00	.00000000E 00
7	8	14	56	41.4793	MH	70	--.11177129E+05	.00000000E 00	.00000000E 00
7	8	14	57	1.2393	MH	70	--.10685378E+05	.00000000E 00	.00000000E 00
7	8	14	57	1.2393	MH	70	--.10985441E+05	.00000000E 00	.00000000E 00
7	8	14	57	4.9992	MH	70	--.10462536E+05	.00000000E 00	.00000000E 00
7	8	14	57	4.9992	MH	70	--.10789379E+05	.00000000E 00	.00000000E 00
7	8	14	57	8.7592	MH	70	--.10275272E+05	.00000000E 00	.00000000E 00
7	8	14	57	8.7592	MH	70	--.10406459E+05	.00000000E 00	.00000000E 00
7	8	14	57	8.7592	MH	70	--.10588926E+05	.00000000E 00	.00000000E 00
7	8	14	57	11.0885	MH	10	--.5640412E+07	.00000000E 00	.00000000E 00
7	8	14	57	12.5191	MH	70	--.10063541E+05	.00000000E 00	.00000000E 00
7	8	14	57	12.5191	MH	70	--.10384037E+05	.00000000E 00	.00000000E 00
7	8	14	57	16.2791	MH	70	--.98473123E+04	.00000000E 00	.00000000E 00
7	8	14	57	16.2791	MH	70	--.99474444E+04	.00000000E 00	.00000000E 00

7	8	16	49	16.3007	MH	70	-.1592C201E+05	.C000000E 00	.C0CC0C0E 00
7	8	16	49	19.6847	MH	70	-.15844733E+05	.C00C000E 00	.0000000E 00
7	8	16	49	19.6847	BD	70	-.15919783E+05	.C00C000E 00	.0000000E 00
7	8	16	49	23.4446	MH	70	-.15758649E+05	.C000000E 00	.0000000E 00
7	8	16	49	23.4446	BD	70	-.15835988E+05	.C00C000E 00	.0000000E 00
7	8	16	49	27.2046	MH	70	-.15670155E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	27.2046	BD	70	-.15749923E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	27.5679	MH	70	-.69524426E+07	.C000000E 00	.C0C0000E 00
7	8	16	49	30.9645	MH	70	-.15579191E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	30.9645	BD	70	-.15601681E+05	.C000000E 00	.0000000E 00
7	8	16	49	30.9645	BD	70	-.15745267E+05	.C00C000E 00	.C000000E 00
7	8	16	49	34.7245	MH	70	-.15485680E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	34.7245	BD	70	-.15570657E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	34.7245	BD	70	-.15655694E+05	.C000000E 00	.0000000E 00
7	8	16	49	37.9204	MH	70	-.15404131E+05	.C00C000E 00	.C000000E 00
7	8	16	49	37.9204	BD	70	-.1557519E+05	.C000000E 00	.C0C0000E 00
7	8	16	49	38.8477	MH	70	-.6773553E+07	.C000000E 00	.0000000E 00
7	8	16	49	42.5963	MH	70	-.15281319E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	42.5963	BD	70	-.15372063E+05	.C000000E 00	.0000000E 00
7	8	16	49	42.5963	BD	70	-.15459887E+05	.C000000E 00	.0000000E 00
7	8	16	49	47.0783	MH	70	-.15159574E+05	.C000000E 00	.0000000E 00
7	8	16	49	47.0783	BD	70	-.15254576E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	49.4822	MH	70	-.15092622E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	49.4822	BD	70	-.15188788E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	50.1275	MH	70	-.66055733E+07	.C000000E 00	.0000000E 00
7	8	16	49	53.8062	MH	70	-.14949175E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	53.8062	BD	70	-.15086604E+05	.C000000E 00	.0000000E 00
7	8	16	49	57.2841	MH	70	-.15160727E+05	.C00C000E 00	.C0C0000E 00
7	8	16	49	57.2841	BD	70	-.14866995E+05	.C000000E 00	.0000000E 00
7	8	16	49	57.2841	BD	70	-.14969642E+05	.C000000E 00	.0000000E 00
7	8	16	49	57.2841	BD	70	-.15062846E+05	.C000000E 00	.0000000E 00
7	8	16	50	.8960	MH	70	-.14758099E+05	.C0C0000E 00	.C0C0000E 00
7	8	16	50	.8960	BD	70	-.14863678E+05	.C000000E 00	.0000000E 00
7	8	16	50	.8960	BD	70	-.14958410E+05	.C000000E 00	.0000000E 00
7	8	16	50	1.4074	MH	70	-.64373836E+07	.C000000E 00	.0000000E 00
7	8	16	50	4.8040	MH	70	-.14636991E+05	.C000000E 00	.0000000E 00

PARAMETERS TO BE CORRECTED (4)

ALPHA DELTA BETA A R V CDAYN GM JZ J3 J5

1 ITERATIONS (MAXIMUM), (6) IC PARAMETERS (7)

(8) 554 OBSERVATION TIMES, 1668 OBSERVATIONS, (9) 3 STATIONS, 3336 CELLS IN COMPACTED DATA LIST (11)

4 FLOCKS (IF BCD INPUT)

OLD FUNCTION IS	1	NEW FUNCTION IS	2
CAME FROM SEGMENT	11	ARE IN SEGMENT	1
OLD FUNCTION IS	1	NEW FUNCTION IS	2
CAME FROM SEGMENT	1	ARE IN SEGMENT	62
OLD FUNCTION IS	1	NEW FUNCTION IS	2

14-09-48 BEGIN EXECUTION

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

CAME FROM SEGMENT 62 ARE IN SEGMENT 2 FUNCTION IS 2

Figure 27. Initial Information

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END
BASIC INPUT CARD 1

BOUNDS
.150000E+01 .150000E+01 .300000E-00 .750000E+00 .492000E+04 .492000E+03 .150000E-00 .100000E-07 .100000E-07 (14)
.100000E-07

101 --2296000E+02119 --6056000E-01201 --2296000E+02219 --6056000E-01301 --2296000E+02319 --6056000E-01 (15)

SIGMA TABLE
INITIAL CONDITIONS
X = .20394186E+08 ALPHA= .23114540E+02 A= .24639581E+08
Y = .87049750E+07 DELTA= .26515160E+02 E= .60470640E-02
Z = .11063023E+08 BETA = .89889776E+02 I= .50150392E+02
XDOT= -.13454234E+05 AZ = .45733120E+02 O= .35850639E+03
YDOT= .12760866E+05 R = .24780837E+08 U= .23399700E+03
ZDOT= .14863762E+05 V = .23765259E+05 T= .83661594E+03

ATMOSPHERE - LOCKHEED CDA/M = .28496000E-00 W/CDA = .35100035E+01
D1 = .68308000E+01 D2 = -.15684000E+02

GM= .55304203E-02 J2= .10826450E-02 J3= -.25460000E-05 J4= -.16490000E-05 J5= -.21000000E-06
J6= .54600000E-06 J7= -.33300000E-06 J8= -.27000000E-06 J9= -.53000000E-07 J10= -.54000000E-07
J21= .90000000E 00 J52= .58460000E-07 L52= -.28190000E+02
J22= .15664000E-05 L22= -.15500000E+02 J53= .22190000E-07 L53= .58580000E+02
J31= .17287000E-05 L31= -.14300000E+01 J54= .16050000E-08 L54= .32270000E+02
J32= .30250000E-06 L32= -.32300000E+02 J55= .10290000E-08 L55= -.15790000E+02
J33= .19660000E-06 L33= .32310000E+02 J61= .95420000E-07 L61= .99460000E+02
J41= .52340000E-06 L41= -.13353000E+03 J62= .29280000E-07 L62= -.38870000E+02
J42= .13720000E-06 L42= .35750000E+02 J63= .10370000E-08 L63= .60000000E 00
J43= .41660000E-07 L43= -.27500000E+01 J64= .15000000E-08 L64= -.15960000E+02
J44= .93780000E-08 L44= .26090000E+02 J65= .38100000E-09 L65= -.28280000E+02
J51= .12470000E-06 L51= -.16413000E+03 J66= .14000000E-09 L66= -.16920000E+02

EARTH MODEL
THE FOLLOWING BODIES ARE USED FOR PLANETARY PERTURBATIONS
NONE

FORMULATION COWELL (EQU.S OF MOTION)

DIFFERENTIAL EQUATION SUBROUTINE E BAR= .1000E-09 A= 1.000 RATIO OF COWELL STEP TO RUNGE KUTTA 4
STEP SIZE - INITIAL= .1000E+01 - MINIMUM= .1562E-01 MAXIMUM= .6400E+02
DO NOT RECOMPUTE PERTURBATIONS FOR CORRECTOR

EQUATIONS OF MOTION USE N1 -10 N2= 6

VARIATIONAL EQUATIONS USE N1 -10 N2= 6 FOR V MATRIX
NO I MATRIX

CONSTANTS
DECIMAL OCIAL
OMEGA E .43752890E-02 32340203260 GM
ALPHA G .49787546E+01 75221125620
C/M M .13808590E+04 3603533376A EARTH MASS - FT .20924777E+24 MASS OF EARTH

DECIMAL OCIAL
.55304203E-02 416244532400
.20924777E+24 MASS OF EARTH

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E-R./A.U.	.23454865E+05	565605075320	N.M./E.R.	.34439335E+04	737510377420
I-O, DISTANCE	.20925738E+08	452000000000	I-O, VELOCITY	.34876230E+06	223146314620
G	.32174060E+02	13201260100	FT/SEC./E.R./MIN.	.24876230E+06	223146314620
DEG/SEC./RAD/MIN	.10471976E+01	44250718340	1/EPS.	.29830000E+03	314631463140
RELATIVE MASS(SUN)	.32295130E+06	723146314620	(MCON)	.1229530E-01	614043432460
EVENUST	.81497900E+00	955337552028	(MARS)	.10782100E-00	25322233700
(JUPITER)	.31788700E+03	422335136140	(SATURN)	.95129000E+02	30446722720

CAME FROM SEGMENT 2 ARE IN SEGMENT 62 FUNCTION IS 2
 OLD FUNCTION IS 2 NEW FUNCTION IS 2

14.09.51 BEGIN EXECUTION
 CAME FROM SEGMENT 62 ARE IN SEGMENT 1 FUNCTION IS
 OLD FUNCTION IS 2 NEW FUNCTION IS 2

14.09.54 BEGIN EXECUTION
 CAME FROM SEGMENT 1 ARE IN SEGMENT 12 FUNCTION IS 2

Figure 27 (cont.)

COMPUTED VALUES FOR ITERATION 1 7/ 8/67 885.000 MIN. Figure 28. Computed Values

A.E.I.D.U.T MEAN ANM= 161.33899 APECEE= 4075.67530
 .24639581E+08 TRUE ANM= 161.55913 HT = 640.21816
 .60470640E+02 0001= -3.60450 PERIGEE= 4030.63175
 .50150392E+02 UDOT= 2.96157 HT = 591.17461 (16)
 .35850639E+03 PERIOD(K)= 107.95173 PERIOD(K)= 107.95173
 .83661994E+03 PERIOD(J)= 107.83470 PERIOD(J)= 107.83470
 CAME FROM SEGMENT 12 ARE IN SEGMENT 1 FUNCTION IS 2
 OLD FUNCTION IS 2 NEW FUNCTION IS 2
 CAME FROM SEGMENT 1 ARE IN SEGMENT 62 FUNCTION IS 2
 OLD FUNCTION IS 2 NEW FUNCTION IS 2

14.09.38 BEGIN EXECUTION
 14.10.02 BEGIN EXECUTION
 CAME FROM SEGMENT 62 ARE IN SEGMENT 13 FUNCTION IS 2

14.10.03 BEGIN EXECUTION
 CAME FROM SEGMENT 13 ARE IN SEGMENT 21 FUNCTION IS 2

ECI COORDINATES OF POSITION AND VELOCITY AT ALL NCAL CROSSINGS WITHIN THE DATA SPAN IN EARTH RADII UNITS

7/ 8/67 928.51826 MM
 -.11723811230828E+01 .33186605308784E-C1 -.44360801643162E-07 -.88733583935479E-03 -.44075741531771E-01 -.52843125252297E-C1
 7/ 8/67 982.07495 MM
 .11809264324098E+01 -.36221085592795E-01 .26694674803984E-07 .17022679758151E-02 .4373275194869E-01 .52457384687182E-C1
 CAME FROM SEGMENT 21 ARE IN SEGMENT 13 FUNCTION IS 2
 OLD FUNCTION IS 0 NEW FUNCTION IS 2
 CAME FROM SEGMENT 13 ARE IN SEGMENT 62 FUNCTION IS 2
 OLD FUNCTION IS 2 NEW FUNCTION IS 2
 (17)

14.11.30 BEGIN EXECUTION
 14.11.40 BEGIN EXECUTION
 CAME FROM SEGMENT 62 ARE IN SEGMENT 15 FUNCTION IS 2

STAT	N	RMS RMS/SIG	TYPE	N	RMS RMS/SIG	TYPE	N	RMS RMS/SIG	TYPE
MH	206	.161216E+01 .266209E+02	(RD)	63	.393518E+03 .171393E+02	(R)			
BD	116	.196791E+01 .324953E+02	(RC)	26	.268186E+03 .116806E+02	(R)			(21)
BH	119	.202287E+01 .394027E+02	(RD)	26	.268888E+03 .117103E+02	(R)			

Figure 30. RMS Summary

Figure 31. Results of Iterations

ITERATION 1 (22)
 564 DATA POINTS WERE USED IN THE SOLUTION (23)
 CURRENT SOLUTION IS BEST SO FAR (24)
 CURRENT SOLUTION IS

ALPHA	DELTA	BETA	A	R	V
-23114540E+02	-26515166E+02	-89889770E+02	-45733120E+02	-24780837E+08	-23765259E+05
GM/M	GM	J2	J3		
-28490000E-00	-55304203E-02	-10826450E-02	-25460000E-05		

CURRENT SOLUTION (LOCAL MACHINE UNITS)

7472154573221420	544320637766672260
146126822171017100	1705615702466762520
710736323265026060	4706747423362016360
113253337465322010	

RMS = 27708193E+02 FOR THIS SOLUTION (27)

CORRECTIONS

.25207767E-02	-.48463704E-04	-.85928347E-04	.49035265E-03	.60568054E+02	.21986359E-01 (28)
-.99368143E-01	.66223787E-08	-.47399442E-09	-.47709546E-09		

BOUNDS

.15000000E+01	.15000000E+01	.30000000E-00	.75000000E+00	.49200000E+04	.49200000E+03 (29)
.15000000E-00	.10000000E-07	.10000000E-07	.10000000E-07		

HITTING BOUNDS (30)

NEXT SOLUTION IS

12317061E+02	-.26515166E+02	.89889684E+02	.4573310E+02	.24780897E+08	.23765261E+05 (31)
-18998180E-00	-59904289E-02	-10826450E-02	-.25460000E-05		

NEXT SOLUTION (LOCAL MACHINE UNITS)

74723354341216200	766360763404357700	544320606644204360
14612676131645460	51362462757153540	1705615723417225540
1326774040257223140	3732470452607342040	4706747413250565300 (32)
1132534411322167510		

PREDICTED RMS = 30560428E+00 FOR NEXT SOLUTION (33)

CURRENT SOLUTION IS (NORMALIZED DATA)

ALPHA	DELTA	BETA	A	R	V
-10446309E-02	-10657239E-02	-75775633E-03	.16072872E-02	.2399429E+03	.16096322E-00 (34)
GM/M	GM	J2	J3		
-64817230E+02	.12757472E-06	.24780837E-04	.27950552E-04		

CORRELATION MATRIX

1.091271E-06
 -1.002007E-06 1.135765E-06
 1.425805E-07 1.474110E-07 5.741945E-07
 4.203503E-07 9.346497E-07 8.069704E-07 2.583372E-06
 1.690322E-01 7.402335E-02 2.600643E-02 1.265453E-01 5.759726E+04
 8.433955E-03 3.555130E-05 4.874953E-05 1.493846E-04 2.963530E+01 2.590916E-02
 6.788504E-03 1.003945E-02 3.786042E-02 3.967345E-02 1.793855E+03 1.355247E+00 4.1822627E+03
 6.947884E-11 1.849656E-11 3.954538E-12 9.345449E-11 2.894611E-05 1.791861E-08 1.926069E-06 1.6322C9E-14
 9.141134E-09 7.329911E-09 2.514224E-08 3.183901E-08 2.461613E-03 8.703271E-07 1.986675E-03 1.163892E-12
 -1.659117E-10 1.983325E-09 2.018024E-08 2.046730E-08 1.300181E-03 1.326400E-06 1.612694E-03 6.072769E-13

(37)

1.210931E-09
 -9.307211E-10 7.812334E-10

ATA INVERSE (OCTAL OUTPUT UNITS)

7627324041360
 6544636257330 63402605700
 156771211000 0244261375702261253516500
 44003652217501407437724700645264324067057745315236C0
 66110541016201433570335230334457127666024132265633205203657525560
 73501225650404723544535170 31747724435407223863346506043103350073436624600120
 20614737647404402202695303416644534710 50359415178603275057096510 5670517052289608522076780
 106756650344024361457125503240313025060215001276032012380033074603342661603040147363453043941261475299C0
 310330115737002450276364570 2736720757007270753717103012571354220 330746625461046660717647506160326127120
 376634002433030123775345302671472757750 04460253532026500C6410670657672651704010277511437406724031762210

5656504342260
 55310146071706322364477460

SQUARE ROOT OF DIAGONAL OF INVERSE

1.0446E-03 1.0657E-03 7.5776E-04 1.6073E-03 2.3999E+02 1.6096E-01 6.4673E+01 1.2776E-07
 3.4798E-05 2.7951E-05
 CAME FROM SEGMENT 15 ARE IN SEGMENT 62 FUNCTION IS 0
 OLD FUNCTION IS 2 NEW FUNCTION IS 0
 CAME FROM SEGMENT 62 ARE IN SEGMENT 63 FUNCTION IS 0

Figure 31 (cont.)

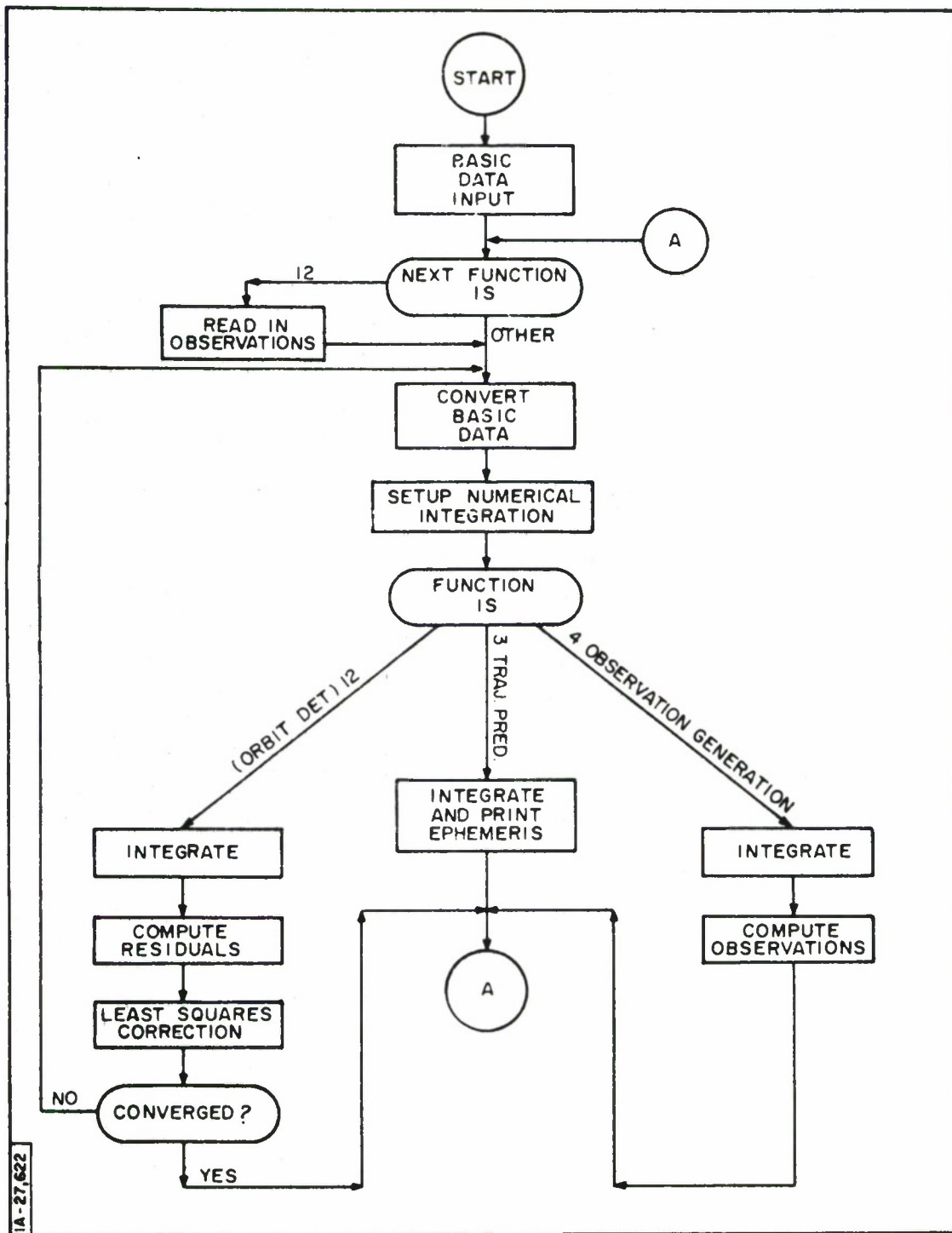


Figure 32. General TRACE-D Flow Chart

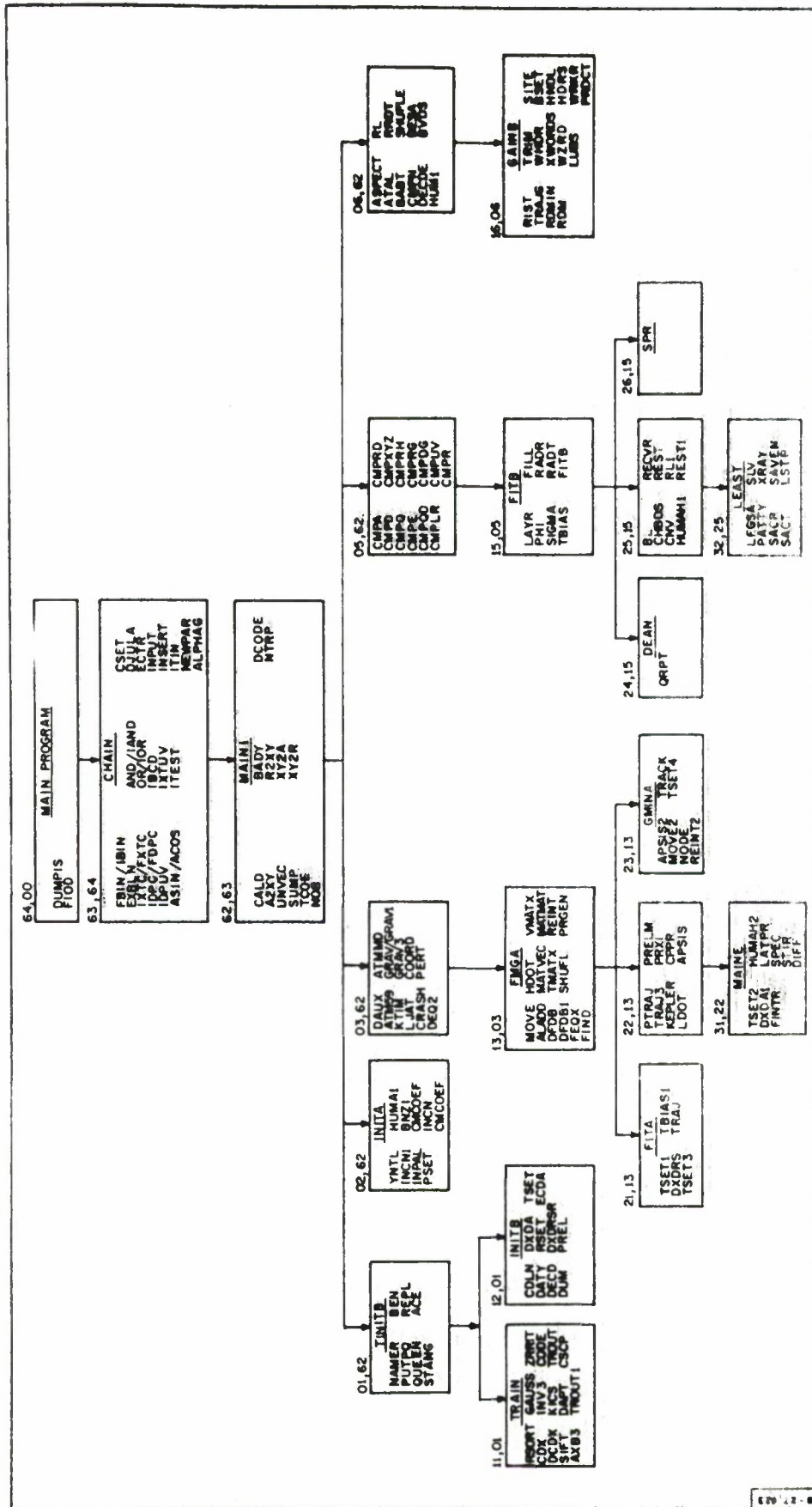


Figure 33. TRACE-D Segmentation Flow Chart

Section 5.

Programming Information

5.1 Structures and Flowcharts

Figures 32 and 33 are both flowcharts of the TRACE-D program; however, each is geared to a different level of description. Figure 32 depicts program paths determined by the function to be performed with only basic operations considered, while Figure 33 presents pertinent programming details also.

Since the TRACE-D program is extremely large (approximately 22,000 source language cards) and can not be fully contained in core, the segmentation mode of operation is employed whereby the program becomes several coreloads. Figure 33 shows the levels of segmentation employed and the makeup of each and every segment. The fact that only the segments along a single vertical path are in core at any one point in time solves the storage program.

The number appearing outside each segment block in Figure 33 serves to identify its level and position in the structure. Those subroutine names underlined are the control programs, which among other things, transfer control to the proper segments for each major function.

5.2 Tape Usage

The TRACE-D program employs many tapes to handle input-output data as well as intermediate calculations. The tape requirements for each option consists of a basic set common to all functions (listed in Table 11) plus a unique option-dependent set. All of the possible option-dependent tapes are listed in Tables 12, 13, 14 and those that are mandatory are appropriately marked. Please note that no more than five tapes from Table 14 may be used in one run (in addition to the basic set, of course).

The above description has been included for completeness; however, as previously mentioned, the user may obtain a running deck

for any option he wishes to choose which will set up all appropriate tapes for him.

Table 11.
Basic Set of Tapes

TAPE NUMBER	NAME	FUNCTION
	LIB1	Program tape #1
	LIB2	Program tape #2
2		System Input Tape
3		System Output Tape
4	PTAPE*	Necessary Scratch Tape
3		Necessary Scratch Tape

* This is a necessary input quantity for all runs.

Table 12.
Trajectory Prediction Tapes

TAPE NUMBER	NAME	FUNCTION
7	CTAPE	Planetary Coordinate Tape
17	NTAPE	Binary trajectory tape (nominal) for trajectory differencing (program generated).
19	DTAPE	Binary difference tape for trajectory differencing.
15		A binary trajectory tape generated by the program and saved.

Table 13.

Observation Generation Tapes

TAPE NUMBER	NAME	FUNCTION
11	ETAPE	BCD tape of observations program generated.
7	CTAPE	Planetary tape
10	IFLAG(16)*	Scratch tape (for trajectory)

* Necessary tape for this option.

Table 14.

Orbit Determination Tapes

TAPE NUMBER	NAME	FUNCTION
11	IBCDI	BCD tape of observations
12	IBINI	Binary tape of compacted observations
7	CTAPE	Planetary coordinate tape
9*		Scratch tape (for normal matrix)
5*		Necessary scratch tape
10*		Scratch tape (trajectory)

* Necessary tapes for this option

5.3 Subroutines

This section is devoted to a complete listing of every subroutine in TRACE-D with a functional description and other pertinent facts also given. In some cases two or more routines are identical in function and differ only slightly in name. This is due to the segmentation rule that the same routine name cannot appear in more than one logical path (i.e., one complete coreload). Therefore, since some routines were needed in more than one path only the names were changed not the content. The routines are listed alphabetically in Table 15 and the information given is self-explanatory.

Table 15.
Subroutine Listing

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE			
		O	R	B	D	E	T	A	J	A	G				
A2XY	62	x	x											312	Converts orbital elements to cartesian coordinates Sets up the code lists for all radar parameters
ACE	01	x												1212	Adds longitude independent terms to the variation- al equations for alpha
ALADD	13	x	x											141	Computes right ascension at Greenwich at 0 hours of given Julian date
ALPHAG	63	x	x											133	Logical "AND" function for two variables
AND	63	x	x											14	Interpolates for and prints latitude, longitude and altitude when BETA = 90°
APSYS	22	x	x											503	

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE				
		O	T	D	R	A	A	T	A	J	G		E	N		
APSYS2	23			x												422
ASIN/ ACOS	63		x													141
ASPECT	05			x												471
ATAL	05			x												116
ATM59	03		x													543
ATMMD	03		x	x												115
AXB3	11	x														205
BABT	06															241
BADY	62															1000
BLN	01	x														401
BL	25	x														111

FUNCTION	CALLS SUBROUTINES	CALLED BY SUBROUTINES
Same as APSIS	NTRP	TRACK
Computes arcsine and arccosine		PTRAJ
Computes aspect angles	XY2R	SITE
Finds I, J elements of matrix		BABT
Computes atmospheric density		ATMMD, LJAT
Channels density evaluation to appropriate routine	ATM59, LJAT	PERT
Solves the system AX=B using Cramer's Rule		INV3
Computes BABT where B and A appropriate matrices		SITE
Computes solution of two-body problem		A2XY
Performs data coding		NAMLR
Finds I, J element of matrix in special format		REST, RESTI

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN								ROUTINE SIZE		
		O	R	B	D	E	T	A	N			
BNZI	02	x									Converts and prints bounds and sigmas	251
BSET	16				x						Sets up headings and labels	341
BVDS	06				x					IDPC, AND	Builds variable data formats	203
CALD	62									INITB, HNDL, PTRAJ, ORPT, RADT, TRAJ, WZRD	Computes complete date from Julian date	216
CDLN	12	x			x					IXTUV, ITIN	Computes data location from BCD name	210
CDX	11	x							RSORT	IDPUV	Packs data into one word	100
CHAIN	63	x			x				MAIN1	INPUT, CSET, DJULA, ALPHAG, NEWPAR, ITIN	Control program for segment 63	607
CHBDS	25	x							LEAST		Modifies bounds for orbit determination	120
CMCOEF	02	x							INITA		Computes coefficients for dynamic station location constraints	1031

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										CALLED BY SUBROUTINES	CALLS SUBROUTINES	FUNCTION	ROUTINE SIZE	
		O	T	D	R	A	A	T	A	G	E					N
CMPA	05	x											RADR	PHI	Computes azimuth partials and residual	456
CMPA	05	x											RADR		Computes topocentric declination partials and residual	623
CMPDG	05	x											RADR		Computes geocentric declination partials and residuals	364
CMPE	05	x											RADR	PHI, CMPR	Computes elevation partials and residuals	626
CMPLR	05	x											RADR		Computes little residuals and partials	451
CMPN	06										x		SITE		Computes noise	136
CMPQ	05	x											SITE	CMPR, FILL	Computes P and O partials and residuals	476
CMPQD	05	x											SITE	CMPRD, FILL	Computes P and O partials and residuals	500
CMPR	05	x											SITE		Computes range partials and residuals	530

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE							
		O	T	R	A	D	R	A	T	A	G		E	N					
CMPRD	05	x													734	Computes range rate partials and residuals			
CMPRG	05	x													340	Computes right ascension partials and residuals			
CMPRH	05	x													636	Computes topocentric RA, HA partials and residuals			
CMPUV	05	x													606	Computes U, V partials and residuals			
CMPXYZ	05	x													514	Computes X, Y, Z partials and residuals			
CNV	25	x													144	Checks for convergence in orbit determination mode			
CODE	11	x													142	Packs data into one word			
COORD	03	x									x				606	Reads JPL tape and performs interpolation			
CPPR	22										x				143	Controls output during trajectory prediction	DIFF, PRXI, PRELM, PTRAJ		

Table 15 (cont.)

NAME	SEGMENT NU NUMBER	USED IN							FUNCTIONS	ROUTINE SIZE	
		O	T	A	T	A	G	E			
CRASH	03	x	x						NTRP, HDOT	Tests for vehi- hicle below critical alti- tude	447
CSCP	11	x							TCDE, DCDX, REPL, IDPC	Compacts and codes data	1174
CSET	63	x	x						TCDE	Sets up some constants	135
DAPT	11	x							DECD	Prints deleted observations	217
DATY	12	x	x					DUM		Prints data types used in partial genera- tion	276
DAUX	03	x	x						MOVE, PERT, MATVEC, GRAV2	Computes deriva- tives for equa- tions of motion and variational equations	270
DCDX	11							CSCP, RSORT, TROUT	IXTUV	Decodes a data word coded by CDX	107
DCODE	62	x	x					KICS, SUMF	IXTUV	Decodes words coded by CODE	141
DECDE	06							DATY	IXTUV	Decodes packet data word	133

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE				
		O	T	D	A	T	A	J	A	G	E		N			
DECD	12	x	x												Same as DECADE	133
DESA	06														Keeps simulation list current	273
DEQ2	03	x													Performs integration	1472
DFDB	13	x	x												Computes non-homogeneous terms for variational equations	376
DFDB1	13	x													Same as DFDB	723
DIFF	31	x	x													750
DJULA	63	x	x												Computes Julian date	177
DUM	12	x	x												Reads station data and stores it	1045
DXDA1	31														Computes partials of pos and vel wrt orbital elements	355
DXDA	12	x													Same as DXDA1	355
DXDRSR	12	x													Computes partials of pos and vel wrt spherical coordinates	342

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE				
		O	T	D	A	T	A	J	P	R	E		N			
DXDRS	21	x														342
ECDA	12	x	x													155
ECTR	63	x	x													253
EXBLN	63	x	x													123
FBIN	63	x	x													305
FDPC	63	x	x													35
FEQX	13	x														183
FILL	15	x														533
FIND	13	x	x													242
FINTR	31	x	x													360
FIOD	64	x	x													14000
FITA	21	x														1472
FITB	15	x														663
FMGA	13	x	x													202

NAME	SEGMENT NUMBER	CALLS SUBROUTINES	FUNCTION	ROUTINE SIZE
		TSET3	Same as DXDRSR	342
		DUM	Codes an array	155
		CHAIN,	Codes an array	253
		INCNI	Extract routine	123
		INPUT	Conversion routine	305
		INPUT	Deposit routine	35
		INPUT	Generates a matrix	183
		RADR, CMPQ	Fills a list for partials computation	533
		CMPQD	Performs linear interpolation	242
		PERT	Used to end a trajectory run	360
		MAINE	Sets up appropriate magnetic tapes	14000
		FMGA	Control routine for segment 21	1472
		MAIN1	Control routine for segment 15	663
		MAIN1	Control routine for segment 13	202

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE					
		O	R	T	D	R	A	A	T	A	G		E	N			
FXTC	63	x	x			x									35	Extract character routine	
GAINA	23					x									1266	Control routine for segment 23	
GAINB	06					x									320	Control routine for segment 06	
GAUSS	11														652	Determines elliptic elements given 2 points	
GRAV	13														470	Computes acceleration components due to geopotential	
GRAV1														301			Computes \dot{h} and \ddot{h} for minimum and maximum altitude
GRAV3																	
HDOT	13	x	x			x									301	Computes \dot{h} and \ddot{h} for minimum and maximum altitude interpolation	
HDRS	16														410	Sets up page headers for observations	
HNDL	16					x									1351	Controls observation output	

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE		
		O	T	D	A	T	A	G	E	N				
HUM1	06								x				Input-output conversion	474
HUM1	02	x						x					Input-output conversion	474
HUM1	25	x											Input-output conversion	474
HUM2	31												Input-output conversion	327
LAND	63	x						x					Logical and function	
IBCD	63	x						x					Conversion routine	
IBIN	63	x						x					Conversion routine	
IDPC	63	x						x					Conversion routine	
IDPUV	63	x						x					Deposit routines	
INC1	02	x						x					Initializes input	766
INC1	02	x						x					Initializes input	1245

BNZ1, R2XY,
 XY2R, NOB,
 INPUT,
 A2XY,
 ALPHAG
 NEWPAR,
 NOB, ECTR,
 INPAL,
 XY2R, YNTL,
 DJULA

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN								ROUTINE SIZE			
		O	T	R	A	D	A	T	A				
		R	B	D	E	T	R	E	N	CALLLED BY SUBROUTINES	CALLS SUBROUTINES	FUNCTION	
INITA	02	x	x	x	x	x	x	x	x	MAIN1	INCN	Control routine for segment 02	525
INITB	12	x	x	x	x	x	x	x	x	INITB	DUM, TCDE, CALD, PREL, REST, NAMER	Control routine for segment 12	360
INPAL	02	x	x	x	x	x	x	x	x	INITA		Checks for incorrect input	261
INPUT	63	x	x	x	x	x	x	x	x	CHAIN	IXTC, IBIN, FBIN	Reads in and stores all input	1662
INSERT	63	x	x	x	x	x	x	x	x	INPUT	INPUV	Inserts character information	102
INV3	11	x	x	x	x	x	x	x	x	TROUT1	AXB3	Computes noise	108
IOR	63	x	x	x	x	x	x	x	x	INPUT		Logical function	
ITEST	63	x	x	x	x	x	x	x	x	INPUT		Tests for certain character configurations	117
ITIN	63	x	x	x	x	x	x	x	x	CHAIN		Checks the next function code in list and sets indicator	106
IXTC	63	x	x	x	x	x	x	x	x	INPUT		Extract routine for characters	
IXTUV	63	x	x	x	x	x	x	x	x	INPUT		Extract routine	
KEPLER	22	x	x	x	x	x	x	x	x	TRAJ3		Solves Keplers equation	160

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN							ROUTINE SIZE
		O	T	F	A	T	A	N	
		R	R	A	J	P	R	E	
		B	A	D	E	G			
		D	A	E					
		T	A	T					
KICS	11	x							505
KTIM	03	x	x						
LATPR	31		x						
LAYR	15	x							
LDOT	22			x					163
LEAST	32	x							578
LEGSA	32	x							1355
LJAT	03	x	x						564

FUNCTION	CALLS SUBROUTINES	CALLED BY SUBROUTINES
Computes initial conditions from 2 R, A, E sets	SUMP, AZXY, DCODE, GAUSS, STRANG	TRAIN
Tests for orbit adjusts times Latitude print routine		TRACK, TRAJ TRAJ3
Accumulates ATA matrix and residuals	NTRP, LDOT	STIR
Computes longitude and rate of longitude		RADR
Control routine for segment 32	SAVEN, SLV, LSTP, RECVR, TCDE, ITIN, SIGMA, SACR, SACT, PATTY, CNV	LATPR
Solves AX=B in least squares sense		FITB
Compute density for Lockheed Jacchia	ATM59	SLV
		ATMMD

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE						
		O	T	D	R	A	T	A	J	P	E		N					
LSTP	32	x													1125	Controls output for least squares	HUMAH1	LEAST
LUBS	16				x										155	Checks data generation indicators		SITE
MAIN1	62	x			x										516	Control routine for segment 62	INITA, FITB, TINITB, FMGA, GAINB	MAIN Prog
MAINE	31					x									1322	Control routine for segment 32	ITIN, FINTR, SPEC, TSET2, TRAJ3	FMGA
MATMAT	13	x			x										114	Computes AB+C		DAUX, DFDB, DFDB1
MATVEC	13	x			x										111	Computes matrix times vector product		REINT, REINT2
MOVE	13	x			x										267	Moves data from one array to another		DAUX, TRAJ, TRAJ3, TSET2
MOVE2	23						x								236	Same as MOVE		TRACK, TSET4
NAMER	01	x			x										230	Finds list of names for output		TRAIN, INITB, CHAIN, INCN1
NEWPAR	63	x			x										561	Decodes parameter list	INSERT	

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE		
		O	T	R	A	D	R	A	T	A	N			
NOB	62	x	x	x	x	x	x	x	x	x	x		Finds correct geopotential coefficient	141
NODE	23												Interpolates for nodal crossings	252
NTRP	62	x	x	x	x	x	x	x	x	x	x		Interpolation routine	371
OR	63	x	x	x	x	x	x	x	x	x	x		Logical or function	1231
PATY	32	x	x	x	x	x	x	x	x	x	x		Prints ATA and inverse	641
PERT	03	x	x	x	x	x	x	x	x	x	x		Computes perturbative accelerations	
PHI	15	x											Computes station coordinate quantities	126
PRDCT	16												Predicts rise and set times	571
PREL	12	x	x	x	x	x	x	x	x	x	x		Computes and prints elements	427
PRELM	22	x	x	x	x	x	x	x	x	x	x		Generates print times	345
PRGEN	13	x	x	x	x	x	x	x	x	x	x			

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN								ROUTINE SIZE	
		O	T	D	R	A	T	A	D		
PRXI	22	x									262
PSET	03	x	x								50
PTRAT	22	x									1216
PUTPQ	01	x									115
QUEEN	01	x	x								140
R2XY	62	x	x								257
RADR	15	x									1233
RADT	15	x									741
RDM	16										10
RDMIN	16										10
RECVR	25	x									135
REINT	13	x	x								456

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										CALLED BY SUBROUTINES	CALLS SUBROUTINES	FUNCTION	ROUTINE SIZE	
		O	T	R	A	D	R	A	T	A	G					E
SAVEN	32	x											LEAST		Saves old matrix on tape	135
SHUFLE	06								x				TRAJG		Shuffles two data list	116
SHUFL	13	x							x				TSET2			117
SIFT	11	x											TRAIN	IXTUV, DAPT	Second difference editing routine	522
SIGMA	15	x											A2XY, BADDY, ASPECT		Finds correct sigma for station L	157
SITE	16										x		GAINB	BABT, LUBS, RRDT, WZRD, CMPN, HUML, ASPECT, DECDE, WRKR REST1, REST LEGSA	Decodes parameter words for data generation	2443
SLV	32	x											LEAST		Solves normal equations	204
SPEC	31												MAINE, CPPR		Write special trajectory tape	340
STANG	01	x											KICS, PSET, TRAIN		Computes station data	137
STIR	31										x		TRAJ3		Interpolates for special trajectory print times	266
SUMP	62	x									x		KICS, RADR	DCODE	Codes data words	237
TBIAS	15	x									x		FITB	SUMP, IXTUV	Computes time bias for each station	217

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN							CALLED BY SUBROUTINES	CALLS SUBROUTINES	FUNCTION	ROUTINE SIZE
		O	T	D	R	A	T	A				
		x	x	x	x	x	x					
TBIAS1	21							FITA	SUMP, LXTUV	Same as TBIAS	217	
TCDE	62	x	x					FILL, NAMED	INITB,	Decodes date	101	
TINITB	01	x						MAIN1	TRAIN	Control routine for segment 01	227	
TMATX	13	x	x					PERT		Calculates T matrix for variational equations	236	
TRAIN	11	x						TINTB	KICS, SIFT, ACE, PUTPQ, REPL, TROUT, RSORT, INPUT, STANG, ZRRIT	Control routine for segment 11	1330	
TRACK	23	x						GAINA		Generates trajectory tape for data generation	453	
TRAJ3	31		x					MAINE	MOVE, NRP, APSIS, KTIM, CPPR, SHUFL, STIR, DEQ2, PRGEN, CRASH, TSET2, DXDA1	Controls integration in trajectory prediction mode	1010	

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN							ROUTINE SIZE
		O	T	A	T	A	G	E	
		R	R	D	J	P	R	N	
		B	A	A	A	R	E		
		D	T	T	T	E			
		E							
		T							
TRAJ	21	x							1033
TRAJG	16				x				267
TRIM	16				x				152
TROUT	11	x							1047
TROUT1	11	x							313
TSET	12	x					x		514

CALLS SUBROUTINES	FUNCTION
NTRP, MOVE CALL, REINT KTIM, TSET1 CRASH, ALADD, PRGEN, TRIM, NTRP, SHUFLE	Controls integration in orbit determination mode
GAINB, PRDCT TRAJG	Reads trajectory from tape for data generation
TCDE, EXIT, DCDX, IXTUV TROUT1, DJULA, ALPHAG, INV3	Computes yaw, roll and pitch corrections Tracking data output routine
CSET, DXDA, A2XY, XY2A, DXDRSR, R2XY	Tracking covariance matrix setup and output routine Initializes integration

CALLLED BY SUBROUTINES
FITA
GAINB, PRDCT TRAJG
TRAIN
TROUT
INITB

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE					
		O	T	A	T	D	R	A	J	A	G		E	N			
TSET1	21	x														403	Initializes inter- gration for orbit determination
TSET2	31		x													344	Initializes inter- gration for tra- jectory prediction
TSET3	21	x														262	Initializes inter- gration for mul- tiple vehicles
TSET4	23						x									331	Initializes inter- gration for data generation
UNVEC	62	x	x														Computes unit vector
VMATX	03	x														263	Calculates matrix for variational equations
WHDR	16						x									255	Writes header page
WRKR	16						x									172	Controlled output routine
WZRD	16						x										Data generation routine
XRAY	32	x														172	Converts units of ATA

Table 15 (cont.)

NAME	SEGMENT NUMBER	USED IN										ROUTINE SIZE				
		O	T	R	A	D	R	A	T	A	G		E	N		
XY2A	62	x	x	x	x	x									412	Converts rectangular coordinates to elliptical
XY2R	62	x	x	x	x	x									225	Converts rectangular coordinates to spherical
YNTL	02	x	x	x	x	x									3713	Output initial conditions and constants
ZRRIT	11	x													240	Sets up sigmas for zero residuals

5.4 Variable Lists

In this section are listed several variable arrays used in the TRACE-D program. These particular variables were chosen because they are the most important and critical storage areas of TRACE-D. They contain all of the indicators and input that dictate the logical program flow.

Table 16. NUMB ARRAY

NUMB	NUMBER OF	SET IN INPUT NAME
1	RADAR STATIONS	TRAIN
2	OBSERVATION TIMES OR STATIONS REQUIRING SIGHTING EPHEMERIS DATA OR STATIONS REQUIRING SIMULATION DATA	TRAIN DUM DUM
3	WORDS IN COMPACTED RADAR OBSERVATION LIST - TOTAL	TRAIN
4	WORDS OF COMPACTED RADAR OBSERVATIONS IN CORE NOW	TRAIN
5	DIFFERENTIAL EQUATION PARAMETERS TO BE SOLVED FOR	CHAIN
6	INITIAL CONDITION PARAMETERS TO BE SOLVED FOR	CHAIN
7	RADAR STATION PARAMETERS TO BE SOLVED FOR	KING
8	RADAR OBSERVATION PARAMETERS TO BE SOLVED FOR	KING
9	PROGRAM TAPE UNIT	CHAIN - PTAPE
10	MAXIMUM ITERATIONS ALLOWED	CHAIN - MAXIT
11	TOTAL PARAMETERS (SUM OF 5,6,7 AND 8)	TRAIN
12	TRAJECTORY PARAMETERS (SUM OF 5 AND 6)	TRAIN
13	OBSERVATIONS (TOTAL NUMBER OF MEASUREMENTS)	TRAIN
14	PRESENT ITERATION	
15	BASIC TYPES OF OBSERVATIONS	CHAIN
16	SIZE OF BUFFERS IN DEAN (Q DATA) - IF = 0, SET TO 5000	DEAN
17	TOTAL RADAR PARAMETERS (SUM OF 7 AND 8)	TRAIN
18	TAPE UNIT FOR PLANETARY COORDINATE TAPE	CHAIN - CTAPE
19	SECOND ORDER DIFFERENTIAL EQUATIONS BEING INTEGRATED (3*(1+NUMB(12)*IFLAG(8)))	INCN
20	POSSIBLE KINDS OF RADAR PARAMETERS (LAT, LONG, HEIGHT, AND BIASES)	CHAIN
21	WORDS IN CORE FOR SIGHTING EPHEMERIS BUCKET	CHAIN
22	POSSIBLE KINDS OF SIGHTING DATA	CHAIN
23	DATA NOISE CONTROL (ZERO FOR NO NOISE, NON-ZERO STARTS RANDOM NUMBER GENERATORS FOR DATA NOISE)	CHAIN - NOISE
24	POSITION IN ITIN LIST OF FUNCTION BEING EXECUTED	ITIN
25	EFFECTIVE PARAMETERS BEING SOLVED FOR (NUMB(11)-(NO. OF CONSTRAINTS))	CHAIN - KNST
26	TAPE UNIT FOR GENERATING BCD STATION AND OBSERVATION TAPE (IF ZERO, NO TAPE GENERATED)	CHAIN - ETAPE

Table 16 (cont.)

27	FLOCKS OF DATA	TRAIN
28	TAPE UNIT FOR ECLIPSE COORD TAPE	CHAIN
29	CURRENT PASS THRU DUM - 0 FOR 1ST PASS, 1 FOR REST	CHAIN
30	ELEMENTS IN ATA	MAIN
31	TAPE UNIT FOR NOMINAL TRAJ. FOR DIFFERENCING RUN	INPAL - NTAPE
32	TAPE UNIT FOR DIFFERENCED TRAJ. FOR DIFFERENCING RUN (LOGICAL NO.)	INPAL - DTAPE
33	MAXIMUM NUMBER OF 2ND DIFFERENCE EDITOR ITERATIONS	
34	NUMBER OF 3 COLUMN PARAMETERS	
35	}	
36		
37		
38		
39	NOT USED	
40		
41		
42		
43	CONVERSION CONSTANT FOR DISTANCES GENERATED IN GAIN. MUST BE INPUT = 3443.9336 NM/ER OR 6975.246 KYD/ER	
44	LOGICAL TAPE NUMBER FOR ANOTHER COMPACTED DATA TAPE TO BE GENERATED IN TRAIN	
	INDICATOR FOR FIXED BASELINE STATION LOCATION CONSTRAINTS - 1 IF OPTION BEING USED	
45	NOT USED	
46	NON-ZERO INDICATES SPECIAL TRAJECTORY TAPE GENERATION	TTAPE
47-50	NOT USED	

Table 17. IFLAG ARRAY

IFLAG - OPTION INDICATORS	INPUT NAME
1 CURRENT FUNCTION BEING EXECUTED = 1, } ORBIT DETERMINATION = 2, } = 3, TRAJECTORY = 4, GAIN	
2 RESTORE (1) LAST GOOD SOLUTION OR CORRECT (0) PRESENT SOLUTION 3 CURRENT LINK BEING EXECUTED	
4 REASON FOR EXIT FROM MAIN (1-MAXIMUM NUMBER OF ITERATIONS. 2-CONVERGED, 3-TRAJECTORY COMPLETED)	
5 CORRECTIONS ARE HITTING BOUNDS (1) OR NOT (0) 6 = 0, COMPLETE SIGHTING EPHEMERIS PRINTED = 1, ONLY RISE, SET, MAXIMUM ELEVATION TIMES PRINTED = 2, ALL DATA, EXCEPT THAT AT RISE, SET, ETC., SAVED ON TAPE ZERO, REGULAR RESIDUAL PRINTING	
7 NEGATIVE, AT ITERATION = MAXIT, SORTED RESIDUALS ARE PRINTED AFTER THE REGULAR RESIDUAL PRINTING POSITIVE, AT ITERATION = MAXIT, ONLY SORTED RESIDUALS ARE PRINTED. NO RESIDUALS ARE PRINTED PRIOR TO THIS.	
8 USED ONLY WHEN RESIDUAL PRINTING INDICATED IN THE PRCDE. (PRCDE(2)) ANALYTIC TRAJECTORY PARTIALS (0) OR VARIATIONAL EQUATIONS (1)	PARTL
9 BOUNDS PROVIDED FOR LEAST SQUARES SOLUTION (1) OR NO BOUNDS (0) 10 NOT USED	
11 T-MATRIX OPTION IF=0, NO T-MATRIX =1, INPUT DRHODH*/H/RHO, NO EARTH FLATTENING =2, INPUT DRHODH*/H/RHO, USE EARTH FLATTENING =3, CALC. DRHODH*/H/RHO, NO EARTH FLATTENING =4, CALC. DRHODH*/H/RHO, USE EARTH FLATTENING	TMATX
12 PARAMETER SPECIFYING SEQUENCE OF FUNCTIONS TO BE 13 PERFORMED	ITIN
14 USED IN GAIN. IF = 0, SORT OUTPUT -- NON-ZERO, DO NOT SORT USED IN SUBROUTINE FINTR IN MAIN	
15 TRAJECTORY COMPARISON OPTION IF IDIFF = 0, REGULAR TRAJECTORY = 1, WRITE PRESENT TRAJECTORY AS REFERENCE ON NTAPE = 2, 1ST COMPARISON, DIFFERENCES WRITTEN ON DTAPE	IDIFF

Table 17 (cont.)

	= 3, OTHER THAN FIRST OR LAST COMPARISON CASES
	= 4, FOR ONE AND ONLY COMPARISON CASE
	= 5, LAST COMPARISON
16	FORTRAN LOGICAL UNIT FOR TRAJECTORY TAPE WRITTEN BY FIT A AND GAIN A.
17	SET NON-ZERO IN TSET IF TO IS A PARAMETER
18	NON-ZERO, ACCUMULATE ATA IN DOUBLE PRECISION (FOR ATA LESS THAN 2746)
19	IF SET NON-ZERO SIGMA TABLE WEIGHTING VALUES WILL BE USED EVEN IF VARIANCE/COVARIANCE MATRICES ARE INCLUDED IN DATA DECK
20	IF NON-ZERO, OPERATE IN 3 PTS./PASS MODE
21	OPTION INDICATOR FOR 2ND DIFFERENCE EDITOR, CONTROLS EDITING OF FIRST 2 AND LAST 2 POINTS
22	} NOT USED
23	
24	
25	SET IN TSET IF ALPHA PARTIALS ARE TO BE COMPUTED.
26	AFTER COMPLETING FIT A CALL FIT B (0) OR DO NEXT FUNCTION (1).
27	NOT USED
28	INDICATOR FOR RESPECIFICATION OF GEOPOTENTIAL COEFFICIENTS \emptyset = RESPECIFICATION
29	NUMBER OF ORBIT ADJUSTS IN SPECIAL TABLE (DELV)

IDLV

Table 18. CNDT ARRAY

CNDT - PARAMETER LIST. CODES ARE IN ITRCD	
1-6	INITIAL CONDITIONS
7	T-ZERO
8	CDA/W
9	GM
10-18	J2-J10
19-38	J21-J66
39-58	LAMBDA21-LAMBDA66
59	ASUBE ' EARTH RADIUS
60	OMEGASUBA - ATMOSPHERE ROTATION RATE
61	T1 THRUST (T1*EXPF(-T2*T))
62	T2
68-75	ICS, TO, AND DRAG FOR SATELLITE NO. 2
80-87	ICS, TO, AND DRAG FOR SATELLITE NO. 3
92-99	ICS, TO, AND DRAG FOR SATELLITE NO. 4
104-111	ICS, TO, AND DRAG FOR SATELLITE NO. 5
116-123	ICS, TO, AND DRAG FOR SATELLITE NO. 6
124-129	} NOT USED
130-135	
136-153	
154	K-ZERO -- TELEMETRY DATA
155	K-ONE -- TELEMETRY DATA

Table 19. KIND ARRAY

KIND	MISCELLANEOUS FIXED POINT INPUT	INPUT NAME
1	UNIT FOR INPUT BCD RADAR DATA TAPE	IBCDI
2	UNIT FOR INPUT BINARY COMPACTED RADAR DATA TAPE	IBINI
3	USED INTERNALLY	
4	EPOCH DATE - YEAR	YEAR
5	- MONTH	MONTH
6	- DAY	DAY
7	PRCDE - OUTPUT CONTROL	PRCDE
8	PARAMETER	
9	FLOCK FLAG	

Table 20. TREG ARRAY

USE OF TREG FOR INTEGRATION (COW)

TREG	CELL	CONTENTS
(K+3)		NEQ (SET IN COW AT B = 35)
(K+2)		CURRENT TIME IN MINUTES FROM MIDNIGHT OF EPOCH
(K+1)		CURRENT INTEGRATION STEP SIZE
(K)-(K-2)		X
(K-3I)-(K-3I-2)		X(PI)
(K-NEQ)-(K-NEQ-2)		X-DOT
(K-NEQ-3I)-(K-NEQ-3I-2)		X-DOT(PI)
(K-2NEQ)-(K-2NEQ-2)		X-DBL. DOT
(K-2NEQ-3I)-(K-2NEQ-3I-2)		X-DBL. DOT(PI)

WHERE ---- NEQ = 3(N+1)

N = TOTAL NUMBER OF I.C. AND D. E. PARAMETERS FOR THE CURRENT RUN

K = L-3 (CURRENTLY = 5490)

L = DIMENSION OF TREG = 90(M+1)+3

M = MAXIMUM NUMBER OF I.C. AND D.E. PARAMETERS (CURRENTLY = 60)

Table 21 (cont.)

(658-677)	SIN(M(LAMBDA-LAMBDA(MN)))	GRAV CALLING SEQUENCE
(678-697)	COS(M(LAMBDA-LAMBDA(MN)))	GRAV CALLING SEQUENCE
(698-706)	DFDX(1) V-MATRIX	
(707-715)	DFDX(2) T-MATRIX	
(716-724)	DFDXD U-MATRIX	
(725-727)	DF/DX*(PSI(PK))	
(728-730)	DF/DXDOT*(PSI-DOT(PK))	
(731-910)	DF/DB	
(916)	RHO (DENSITY)	
(917)	A (VEL OF SOUND)	
(918)	H (ALTITUDE)	
(919)		
(920)	M (MACH NUMBER)	
(921-923)	X-DOT(A)	
(924)	D/V(A) = RHO/2*V(A)*CDA/W	
(925-927)	F(3)	
(928)	ABSF(X-DOT) = V(A)	
(935-937)	F(4) THRUST FORCE	
(938-943)	ABSF(X(J))**3	
(944-949)	ABSF(X-X(J))	
(950-955)	ABSF(X-X(J))**3	
(956-961)	ABSF(X-X(J))**5	
(962-964)	X-X(1)	
(965-967)	X-X(2)	
(968-970)	X-X(3)	
(971-973)	X-X(4)	
(974-976)	X-X(5)	
(977-979)	X-X(6)	
(980-982)	F(2)	
(983-1000)	INTERPOLATED VELOCITIES OF OTHER BODIES	

Table 22. STAT ARRAY

STAT--PROPERTIES RELATED TO THE LTH STATION

CELL	DESCRIPTION	UNITS
(1,L) ---	GEODETIC LATITUDE	(RADIAN)
(2,L) ---	EAST LONGITUDE	(RADIAN)
(3,1) ---	ALTITUDE	(EARTH RADII)
(4,L) ---	COS (LAT)	
(5,L) ---	SIN (LAT)	
(6,L) ---	W1	(EARTH RADII)
(7,L) ---	W3	(EARTH RADII)
(8,L) ---	SIGMA SET	
(9,L) ---	REFRACTIVITY TYPE	
(10,L) ---	STATION NAME	
	Q STATION NUMBER	
	P STATION NUMBER	
(11,L) ---	(NOT USED)	

Table 23. COMMON LAYOUT

COMMON A - BLOCKS NEEDED FOR ALL LINKS - 8722 CELLS

ALPH	1	ITEMP	45
AUS	1	ITRCD	62
C	100	KIND	10
CC	3,6	NUMB	50
CO	56	PARINT	50
CI	56	PKICK	50
CNDT	160	PRTIM	21
CPRAM	2	PUSH	200
DAVE	100	REFR	15
DPRAM	40	SIS	1
DRAG	120	SUSP	1
ELL	20	TRAJX	367
FIC	10	TRJN1	552
FLEE	100	TUMP	100
HEAD	24	XTRA	50
IDTAPE	17	TEMP	1000
IFLAG	30	TREG	5493

COMMON B - BLOCKS NEEDED FOR FIT AND DATA GENERATION LINKS - 4300 CELLS

GOK	1800	PBIAS	100
BIAS	100	RPRAM	200
DPAR	100	SIGGY	100
ICDLC	100	SIGMY	100
IPRCD	500	STAT	11,100
ISIG	100		

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DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) The MITRE Corporation, Bedford, Massachusetts		2a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED	
		2b. GROUP	
3. REPORT TITLE TRACE-D USERS' MANUAL			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) N/A			
5. AUTHOR(S) (First name, middle initial, last name) S. G. Santarelli			
6. REPORT DATE July 1969		7a. TOTAL NO. OF PAGES 192	7b. NO. OF REFS 5
8a. CONTRACT OR GRANT NO. F19628-68-C-0365		9a. ORIGINATOR'S REPORT NUMBER(S) ESD-TR-69-273	
b. PROJECT NO. 7070		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) MTR-839	
c.			
d.			
10. DISTRIBUTION STATEMENT This document has been approved for public release and sale; its distribution is unlimited.			
11. SUPPLEMENTARY NOTES N/A		12. SPONSORING MILITARY ACTIVITY Directorate of Planning and Technology, Electronic Systems Division, Air Force Systems Command, L. G. Hanscom Fld., Bedford, Mass	
13. ABSTRACT This report describes the MITRE version of the TRACE-D program now in operation. While the primary function of TRACE-D is orbit determination, options are also available in the program for trajectory prediction and observational data generation. A functional description of these features is contained in this report along with a complete user's manual and a brief program description.			

14.

KEY WORDS

LINK A

LINK B

LINK C

ROLE

WT

ROLE

WT

ROLE

WT

PROGRAMMING
 ORBIT DETERMINATION
 TRAJECTORY PREDICTION
 OBSERVATIONAL DATA GENERATION
 SATELLITE TRACKING